

Job No. 12-242-306 Sheet No. Cover  
By DTN/PGS Date Sept 2012



CARUSO  
TURLEY  
SCOTT  
consulting  
structural  
engineers

CLIENT:

**Panel Claw**  
1600 Osgood Street  
Building 200, Suite 2-23  
North Andover, MA 01845

PROJECT:

**Madonna Road**  
1550 Madonna Road  
San Luis Obispo, CA

YOUR VISION IS OUR MISSION

PARTNERS

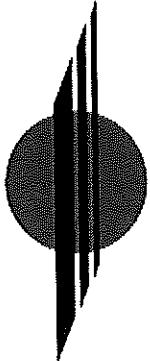
Richard D. Turley, PE  
Paul G. Scott, PE, SE  
Sandra J. Herd, PE, SE  
Chris J. Atkinson, PE, SE  
Thomas R. Morris, PE  
Richard A. Dahlmann, PE

GENERAL INFORMATION:

**BUILDING CODE:** 2009 IBC, 2010 CBC, ASCE 7-05

INDEX OF SHEETS:

<b>MEMO</b>	Summary of Documentation and results
<b>1.0 – 1.3</b>	Wind Tunnel Testing
<b>2.0 – 2.26</b>	Array/Ballast Layouts
<b>3.0</b>	Ballast Loads Calculator
<b>4.0 – 4.111</b>	Mechanical Attachment Calculator
<b>A1 – A10</b>	Mechanical Attachment Capacities



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Richard A. Dahlmann, PE

Date: September 11, 2012

**Mr. Robert Clough**  
Panel Claw  
1600 Osgood Street, Bldg 20, Ste 2-23  
North Andover, MA 01845

**RE: Evaluation of Panel Claw system**

Project Name: Madonna Road  
CTS Job No.: 12-242-306

Per the request of Robert Clough at Panel Claw, CTS was asked to review the Panel Claw system and its resistance to wind and seismic loads.

**Wind Evaluation:**

Panel Claw provided CTS with wind tunnel testing performed by I.F.I (Institute for Industrial Aerodynamics) at the Aachen University of Applied Science (reference pgs). The system tested was the "Polar Bear Gen II 10deg" system. This system consists of photovoltaic panels installed at a 10 degree tilt onto support assemblies. The support assemblies consist of a support frame for the PV panels, wind deflectors and areas for additional mass/weight as required for the ballast loads.

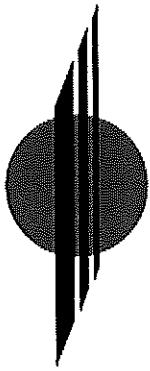
The wind tunnel testing was performed per Method 3 in Chapter 6 of ASCE 7-05. The parameters of the testing were a flat roof system in both Exposure B and C on a building with and without parapets. The testing resulted in pressure and/or force coefficients that were applied to the velocity pressure  $q_z$  in order to obtain the wind loads on the PV system (reference pgs 1.0 – 1.3). From the wind load results it is then possible to calculate the ballast loads required to resist the uplift and sliding forces. CTS agrees with the methodologies used to develop the required ballast loads for the "Polar Bear Gen II 10 deg" system per the wind tunnel testing results.

Panel Claw also provided CTS with the excel tool that was developed to express the equations used to obtain the ballast loads on roofs (reference pgs 3.0). CTS has reviewed this tool and the required ballast loads to find that the loads provided are not within the values required. Therefore, Panel Claw calculated the amount of mechanical attachments that would be required to resist the wind force that is not accommodated by the applied ballast loads (reference pg 4.0 - 4.1).

**Seismic Evaluation:**

CTS was asked to review the Panel Claw system to determine attachments required to resist seismic loading of the ballasted solar support system on the roof of the existing building. Please note the following support:

- The ballasted solar support system has a certain capacity to resist wind loads. If additional attachments are required, the attachments can be used for seismic and wind. There are no load combinations in the code that required the application of seismic and wind forces together.
- The building parapets provide a physical barrier that will prevent the system from sliding off the roof and becoming a life safety issue.



As this is not a life safety issue we have calculated the required attachments. Utilizing CBC Load Combination 16-15 we have reduced the 0.6 Dead Load value further, by subtracting the vertical component of the seismic forces (0.7E).

Panel Claw has provided a calculation for the number of mechanical attachments that are required to resist any seismic forces that are applied to the system (reference pg 4.0 – 4.111). The total number of mechanical attachments is dependant on the capacity of each attachment (reference pg A1 – A10). The attachment provided is the Eco-Fasten - Universal Roof Attachment System. Each base plate of this system attaches through to the roof deck using 8 # 14 screws.

Therefore, it has been determined that the system that has been provided by Panel Claw is sufficient to resist both wind and seismic loads at Madonna Road.

Please contact CTS with any questions regarding this letter or attachments.

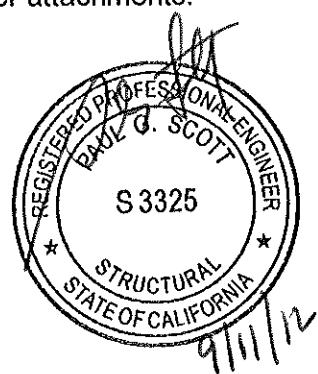
Respectfully,

Dean Noel  
Structural Designer

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PARTNERS

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Notifizierte Prüf-, Überwachungs- und  
Zertifizierungsstelle Nr. 1388  
nach dem Bauproduktengesetz

Client: PanelClaw Inc., North Andover, MA 01845, USA  
Project No.: PCM02  
Report No.: PCM02-2

## **Wind loads on the photovoltaic roofing system „Polar Bear Gen II 10deg“ of Panel Claw Inc.**

**Determining the characteristic values for uplift and sliding  
according to the American Standard ASCE/SEI 7-05**

Aachen, 12/13/2011

*Thorsten Kray*

Dr.-Ing. Th. Kray

*F. Hunke*

Dipl.-Ing. (FH) F. Hunke

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BLZ 390 500 00

Commerzbank AG Aachen  
Kto.-Nr. 3 006 848  
BLZ 390 400 13

Amtsgericht Aachen  
HRB 4518

Wind tunnel tests were conducted on the PV flat roof system „Polar Bear Gen II 10deg“ of Panel Claw Inc. in accordance with chapter 6.6 of ASCE/SEI 7-05. The tests were performed at I.F.I. Institut für Industrieaerodynamik GmbH (Institute for Industrial Aerodynamics), Institute at the Aachen University of Applied Sciences. The system consists of PV-modules angled at 10°, which are fixed on support assemblies. The support assemblies create a rigid connection of the PV solar module and the wind deflector of two rows behind one another. The rear side of a row of panels is fully covered by a wind shield, see Fig. 1.1. Fig. 1.2 shows a wind tunnel model.

Testing was carried out with surface roughnesses in the approach section of the boundary layer wind tunnel equivalent to open country (Exposure C according to ASCE/SEI 7-05) and suburban terrain (Exposure B). Pressure and/or force coefficients were derived from the measurements. These coefficients may be multiplied by the design velocity pressure  $q_z$ , determined depending on the wind zone, the exposure category and the building height in accordance with the American standard ASCE/SEI 7-05 to determine the wind loads on the PV system. From these results it is possible to calculate the necessary ballast for uplift and sliding safety - sliding of PV elements occurs if the aerodynamic lift has decreased the down force due to deadweight sufficiently so that the drag forces are larger than the frictional forces - on flat roofs with pitch angles up to 7°.

For the present analysis, I.F.I. created a calculation tool in Excel which can be used not only for further programming or the dimensioning in a project, but also for purposes of documenting the ballast calculation. The tool presents a summary of the values calculated on the safe side from the tests for all wind directions and the roof zones 1, 2 and 3. In addition, it contains correction formulae taking into account the positive effect of a parapet on the wind loads in the edge and corner regions. The correction coefficient is calculated from the results of the wind tunnel tests.

The results are given as quasi-static characteristic values. As stated in ASCE/SEI 7-05 where local load coefficients for an area of 1 m<sup>2</sup> to 100 m<sup>2</sup> are given, the force coefficients do not apply to modules placed individually, but only to arrays with at least 10 m<sup>2</sup> module's surface where at least two rows are statically joint to one another. This is important as the simultaneity of smaller turbulences on the analysed

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Report No.: PCM02-2

Wind loads on the photovoltaic roofing system

„Polar Bear Gen II 10deg“ of Panel Claw Inc.

Determining the characteristic values for uplift and sliding according to the American Standard  
ASCE/SEI 7-05

field of 10 m<sup>2</sup> has to be excluded and only bigger turbulence effects have to be taken into consideration. Thus, smaller arrays may have to carry more ballast depending on their situation on the roof.

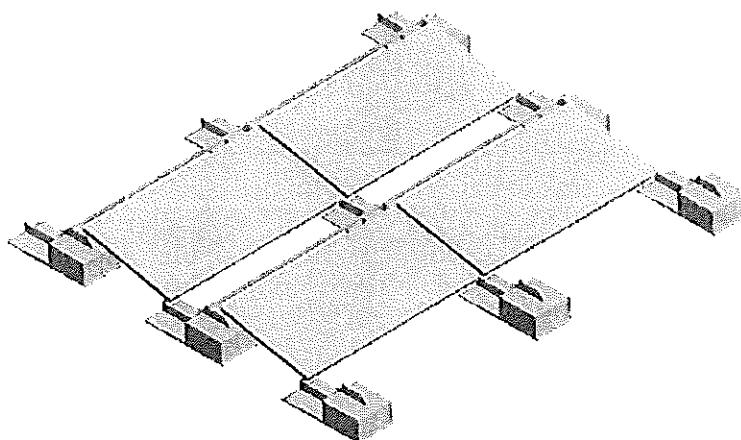


Bild 1.1: PV-system "Polar Bear II 10deg" for flat roofs

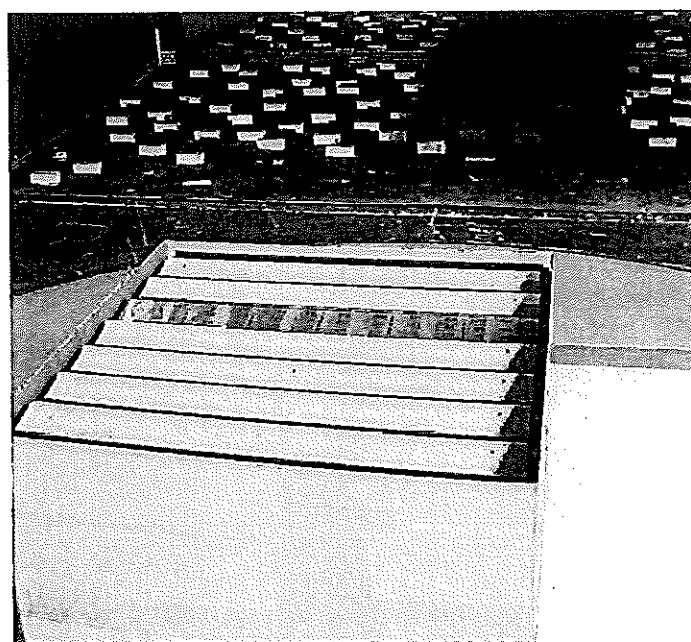


Bild 1.2: Wind tunnel model of the PV-system "Polar Bear II 10deg" with covered edge zones and with parapet; suburban terrain exposure

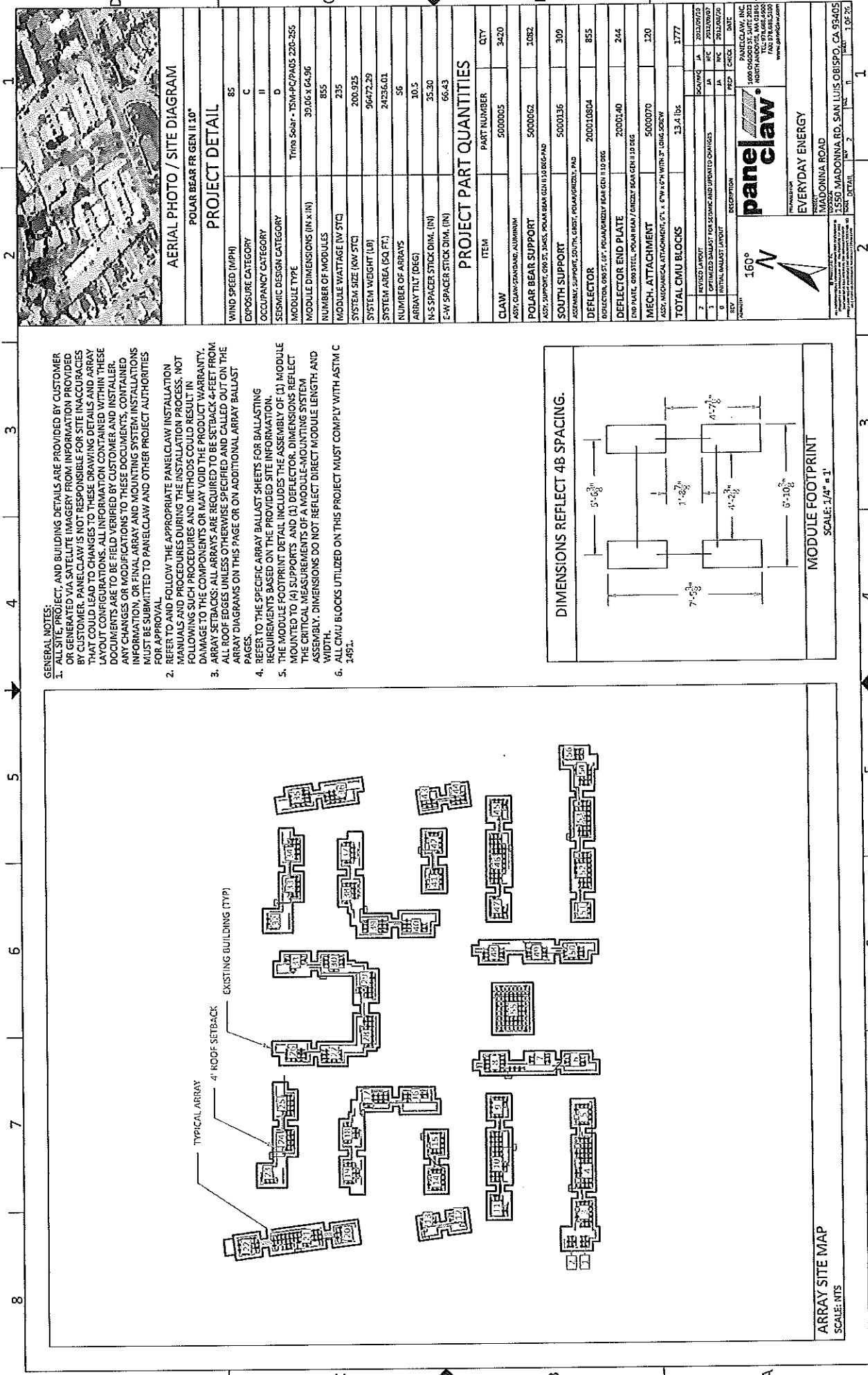
The results were determined for a set-up where the rows were aligned from east to west. However, the results are applicable for any row alignment with the points of the compass. As wind tunnel testing was carried out for a low-rise building with height of 30 ft (9.1 m) in a single exposure site as permitted in ASCE/SEI 7-05 section 6.6, the given force coefficients are only valid for PV systems installed on buildings lower than 60 ft (18.3 m).

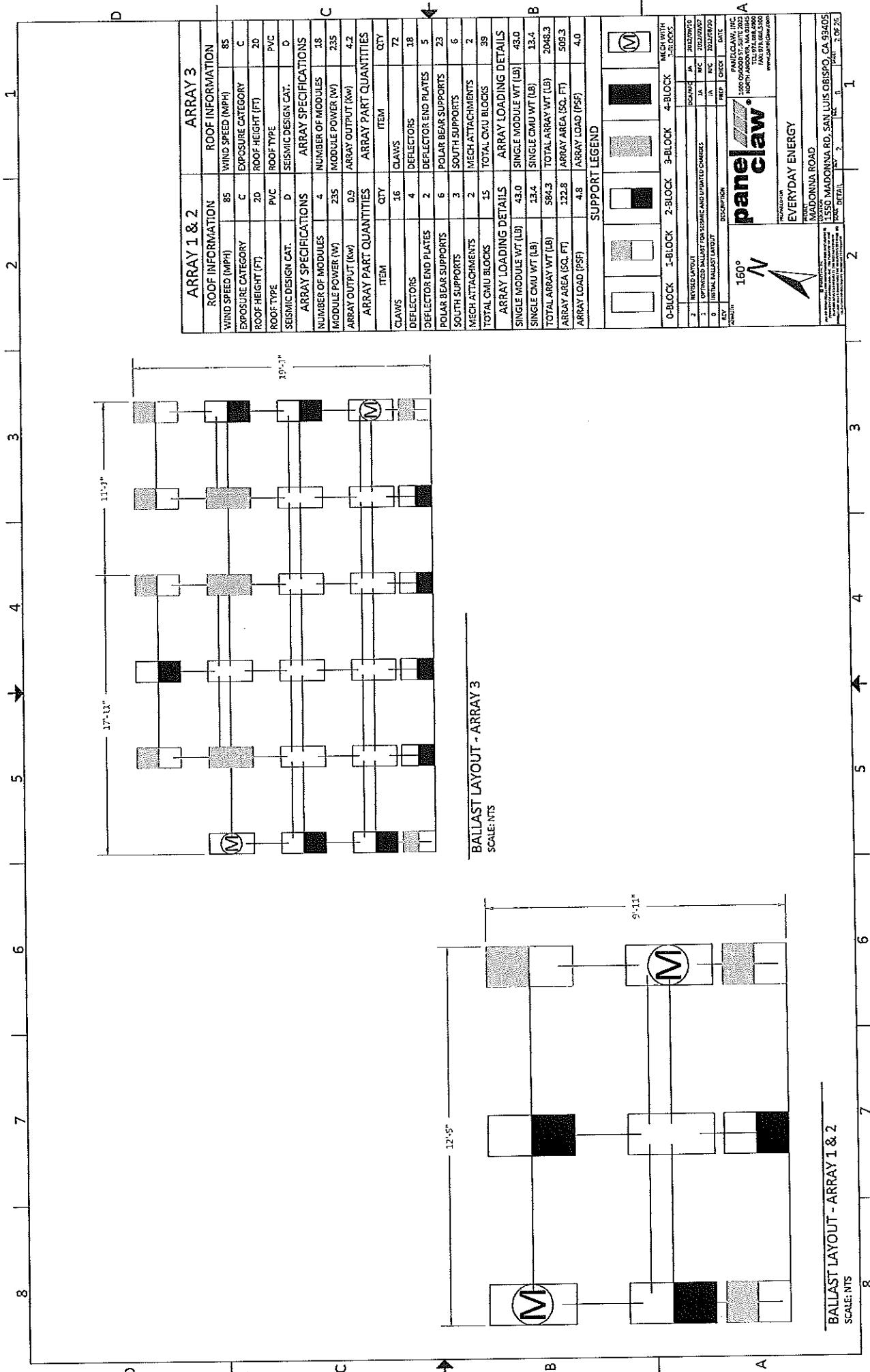
The coefficients extracted from the wind tunnel tests may also be used in accordance with the information given in ASCE/SEI 7-05. The values show that the system in question needs very little ballasting in the centre of a field. The sliding and uplift loads exerted by the wind on the modules are very small due to the arrangement in rows. Higher loads were only observed in corners and in exposed edges of the field, and these have to be taken into account. On the basis of the measurements carried out, this may be done directly by increasing the ballast locally on the edge or corner elements as well as – in the arrangement of rows and space between the rows – by distributing the loads under consideration of areas less submitted to them and the dead load of the modules. However, in the latter case, higher structural demands are required for the load transfer by the supporting assemblies since, theoretically, a suspended corner module has to be held in place by the adjacent modules.

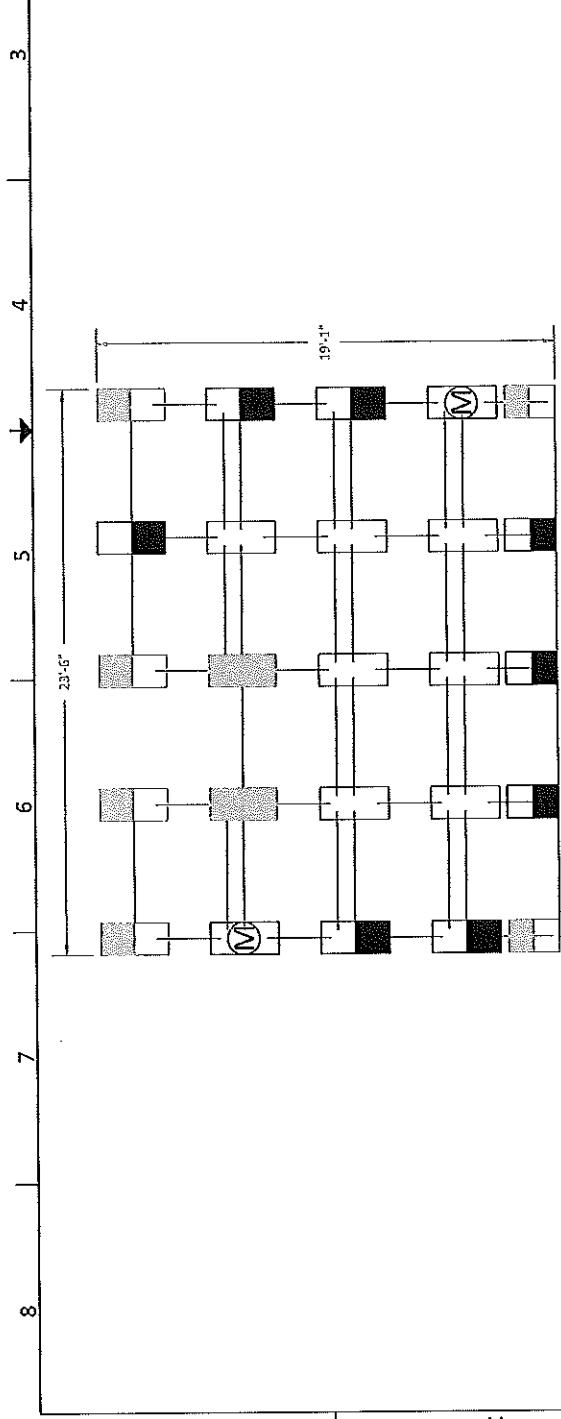
As stated in the ASCE/SEI 7-05 section C6.5.2, for some projects with irregular or unusual site locations or buildings or structures differing from the provisions given under ASCE/SEI 7-05 section 6.5.2, a wind engineer must be consulted to evaluate the upwind situation and the applicability of the wind tunnel results. For example unusual building shapes, neighboring tall buildings and irregular topographic features such as mountain gorges require a statement of a wind expert.

The analysis of the maximum loads in the different roof zones for the inclination angle of 10° resulted in a maximum lift coefficient of  $c_{lz} = 0.09$  in the inner area of the roof and  $c_{lz} = 0.12$  in the corner zone of the roof, these results being based on the module's surface area. At the same time, sliding forces appear, their coefficients reaching  $c_{fx,y} = 0.07$  in the centre of the field and  $c_{fx,y} = 0.13$  in the corner zones.

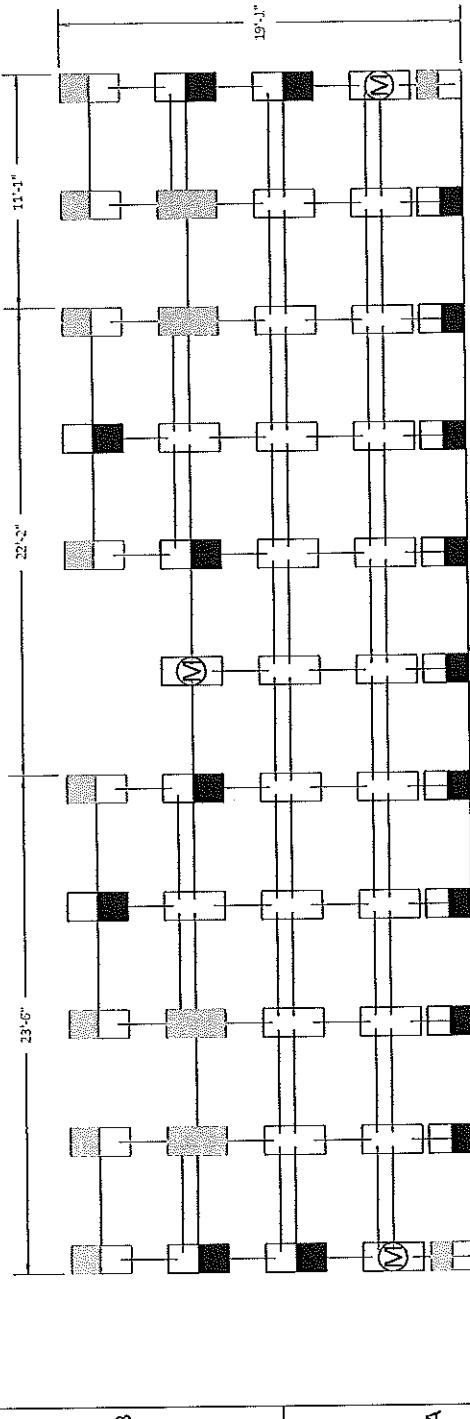
Details of the tests and of the analysis can be found in the long version of the report PCM02-1.





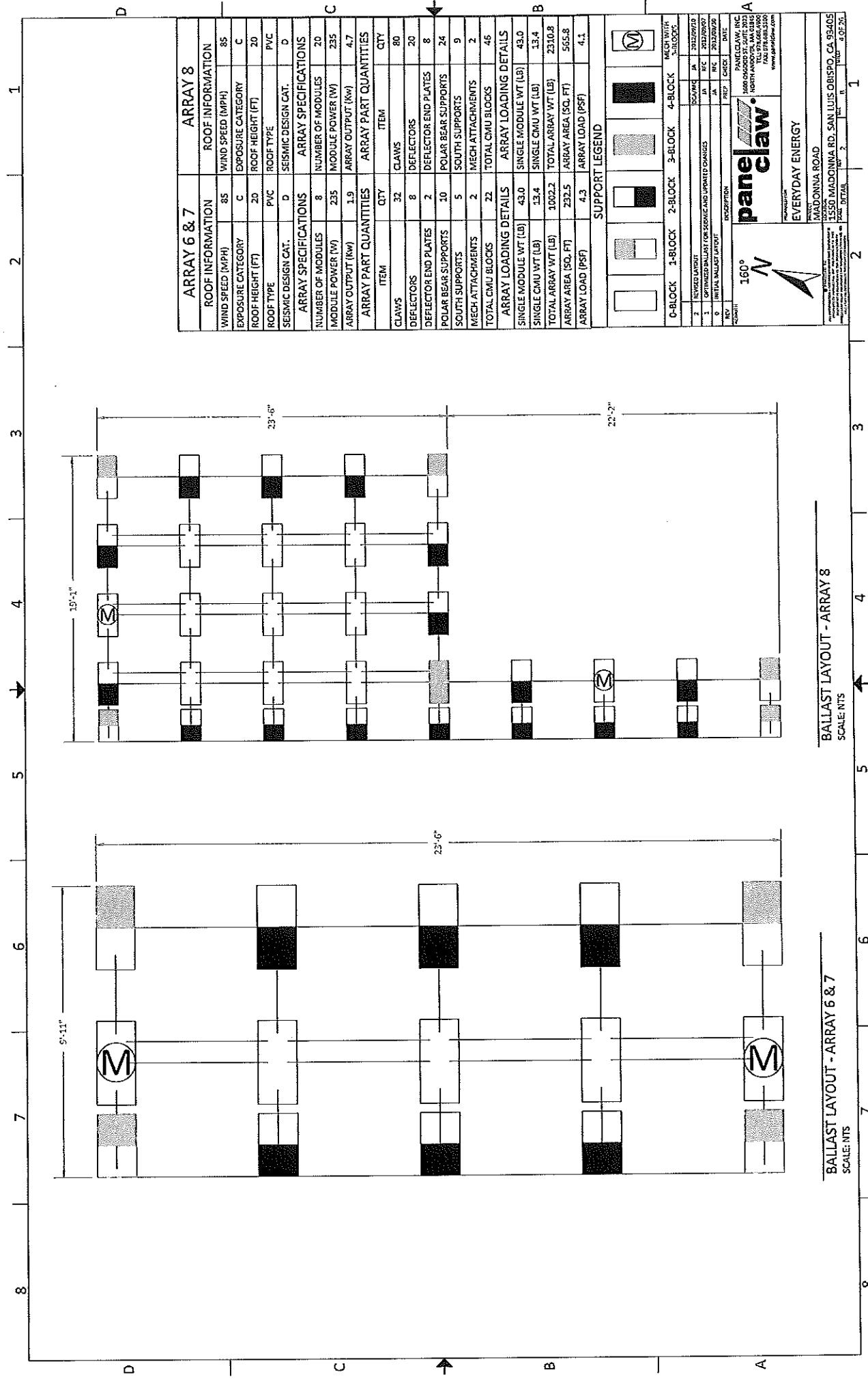


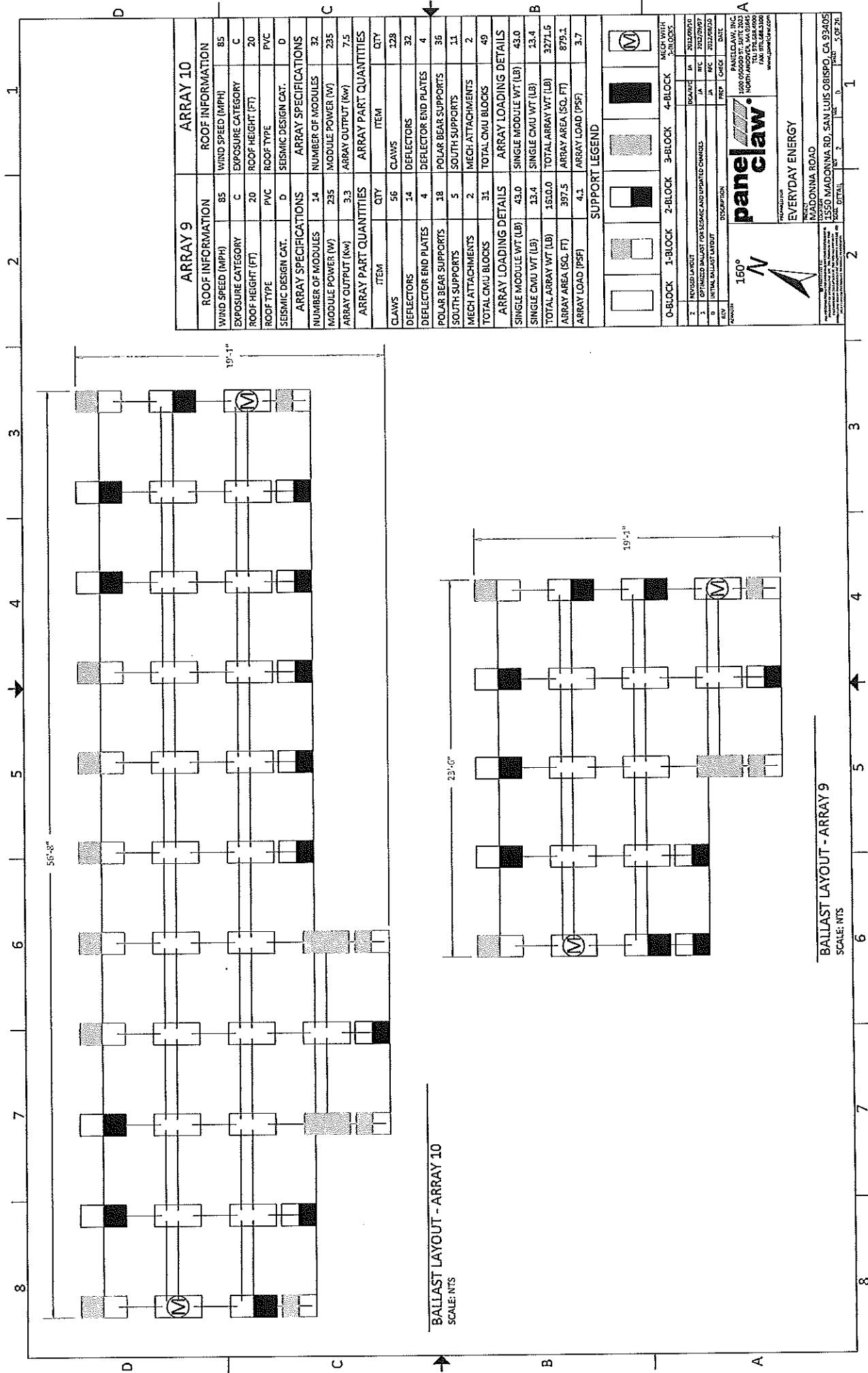
BALLAST LAYOUT - ARRAY 5 & 15  
SCALE: NTS

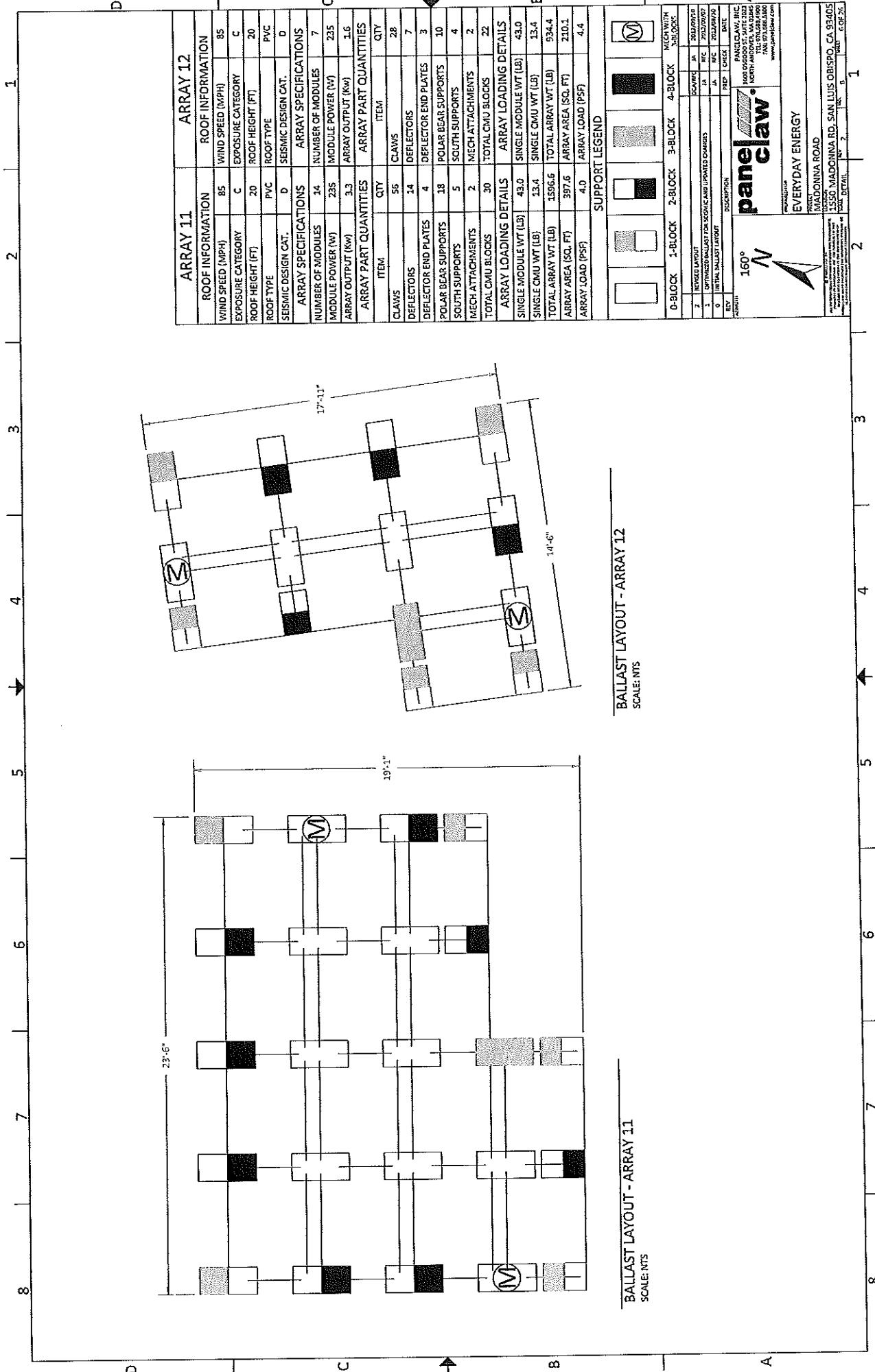


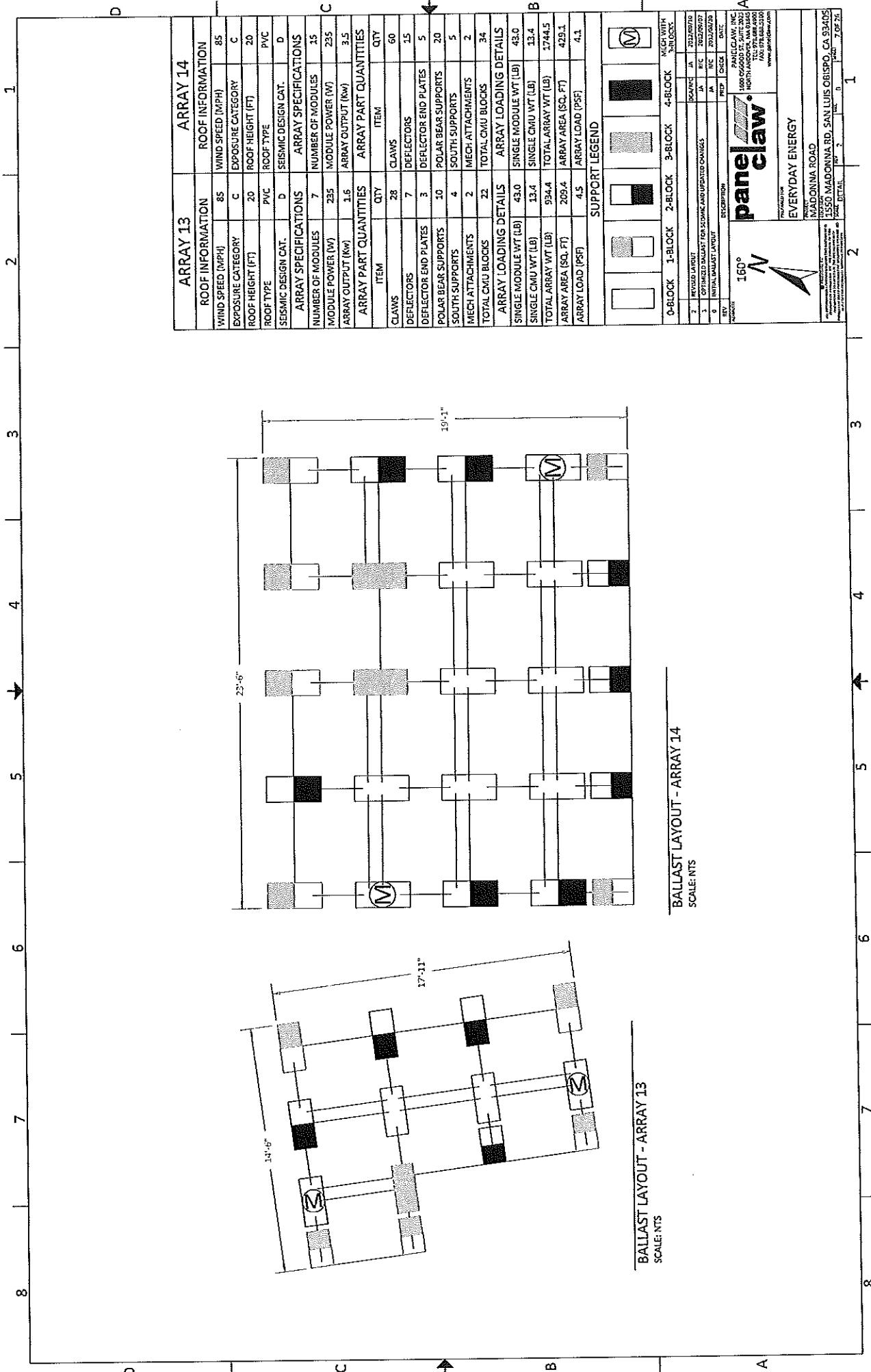
BALLAST LAYOUT - ARRAY 4  
SCALE: NTS

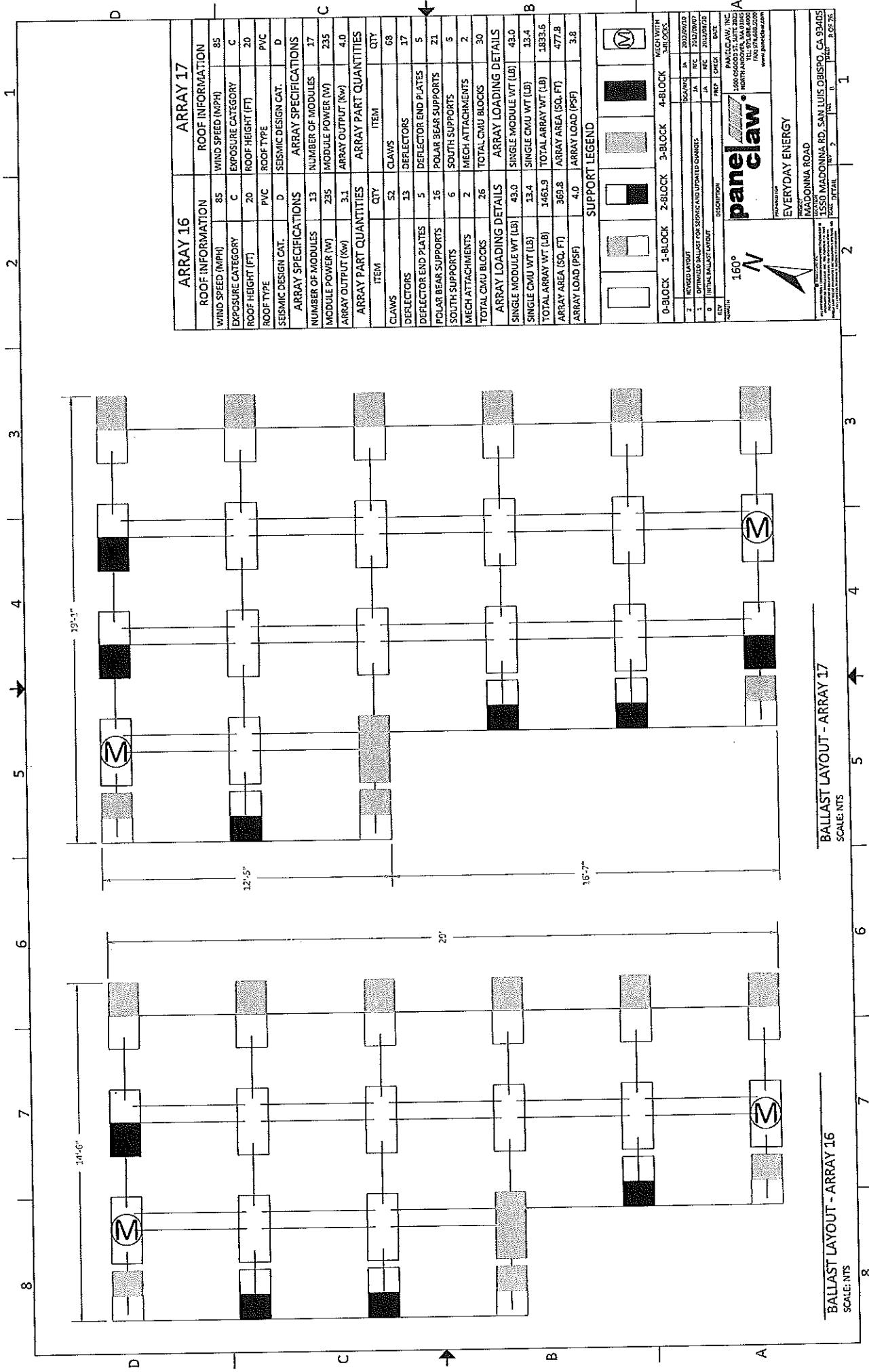
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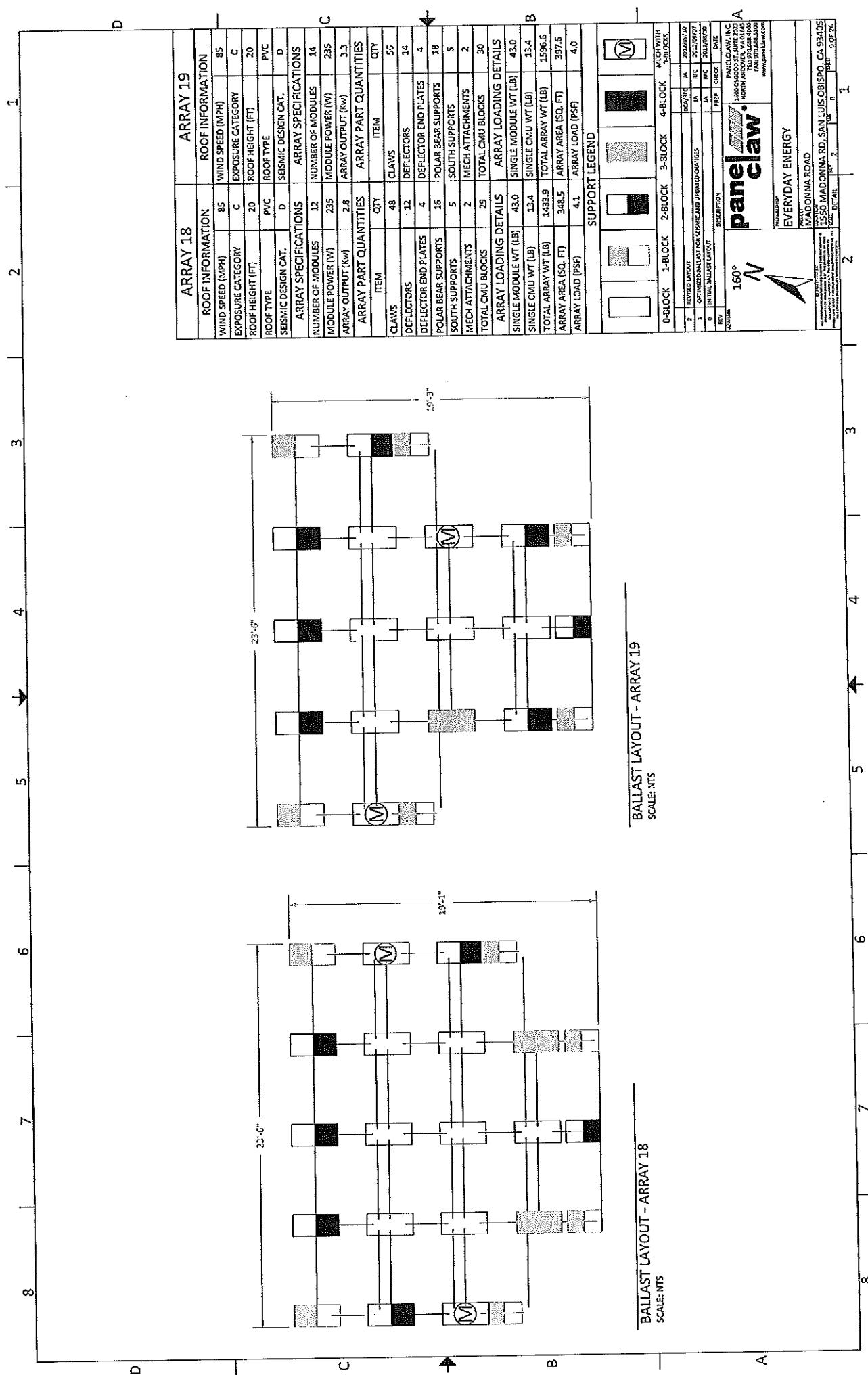


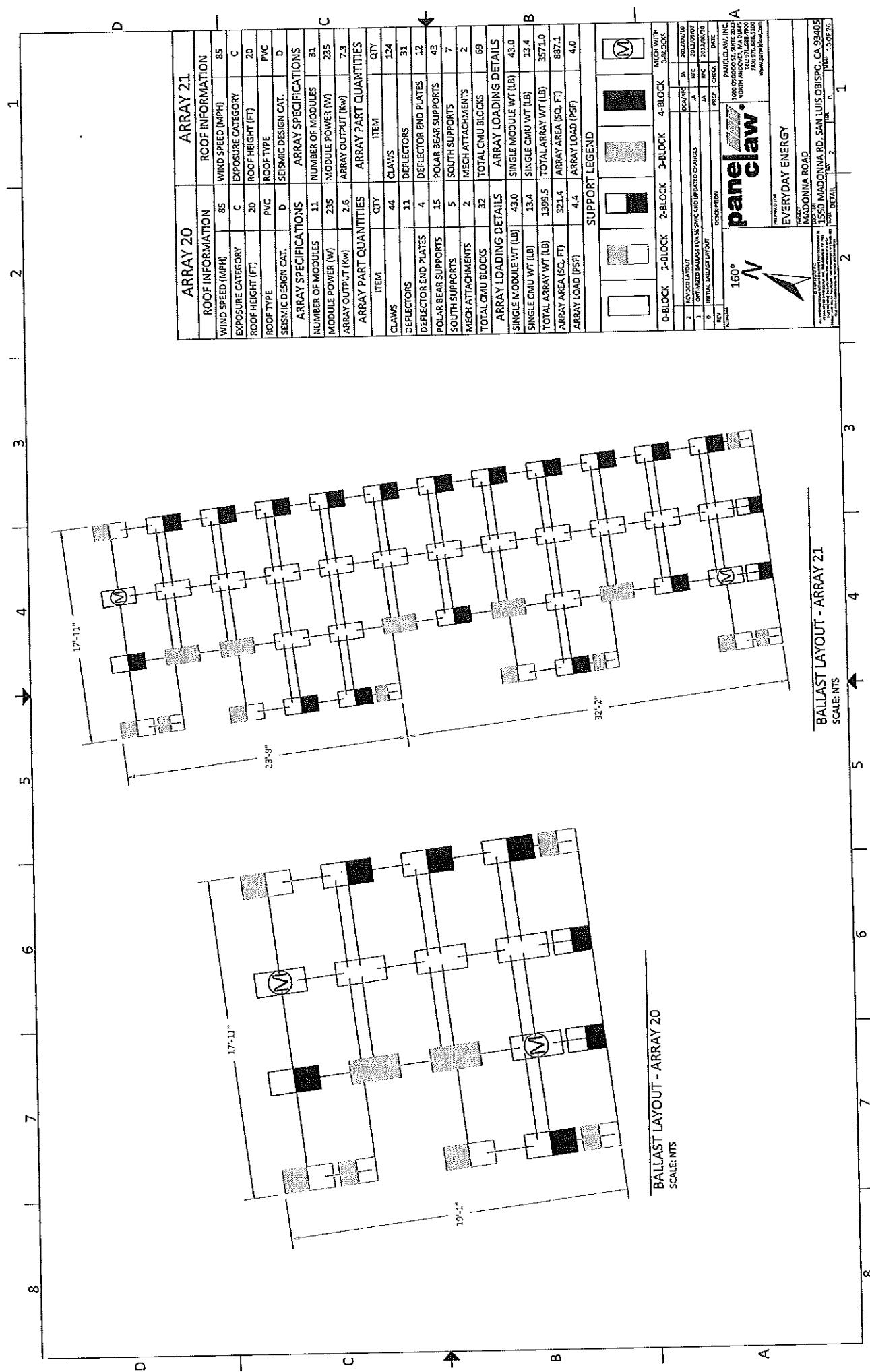


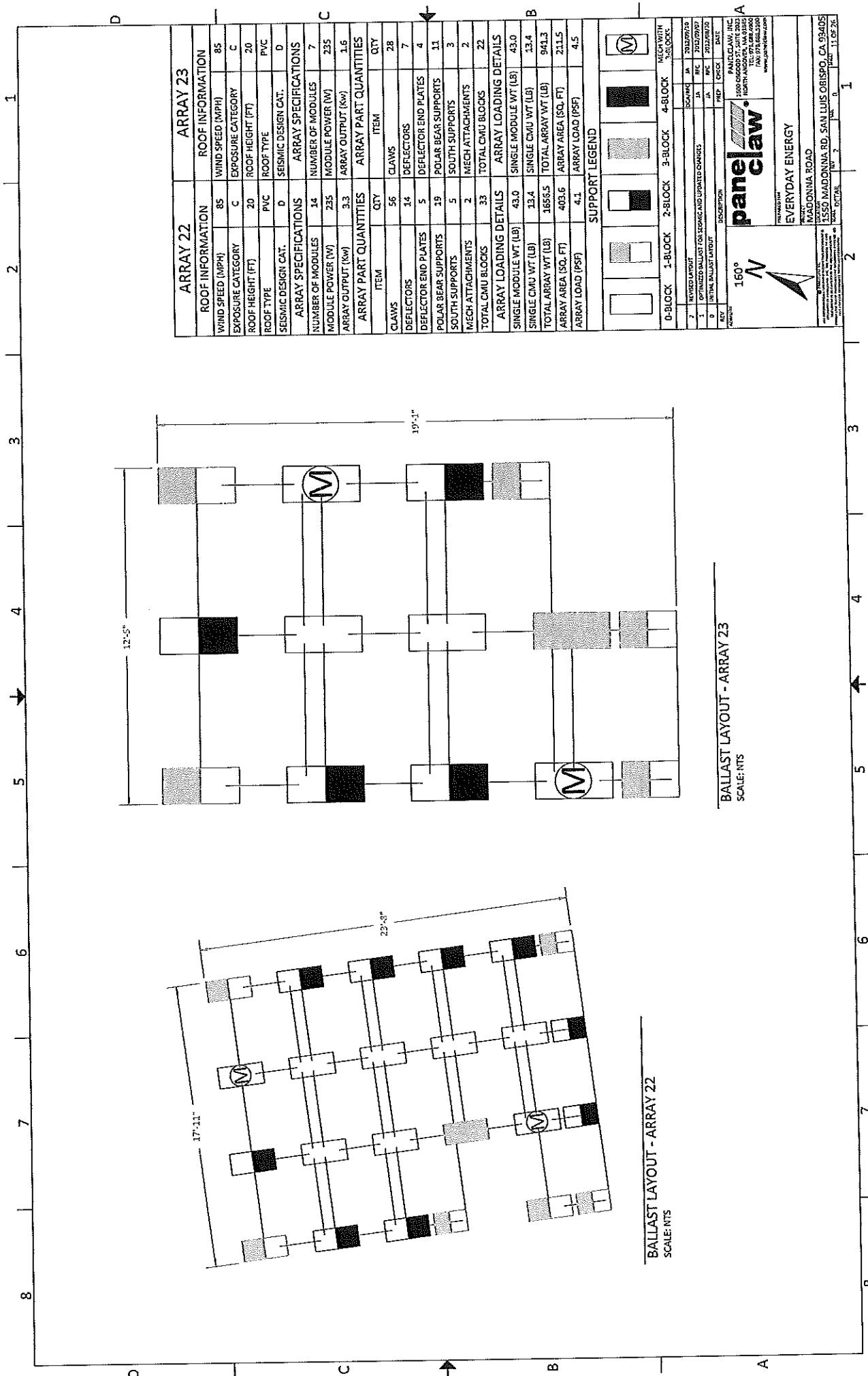


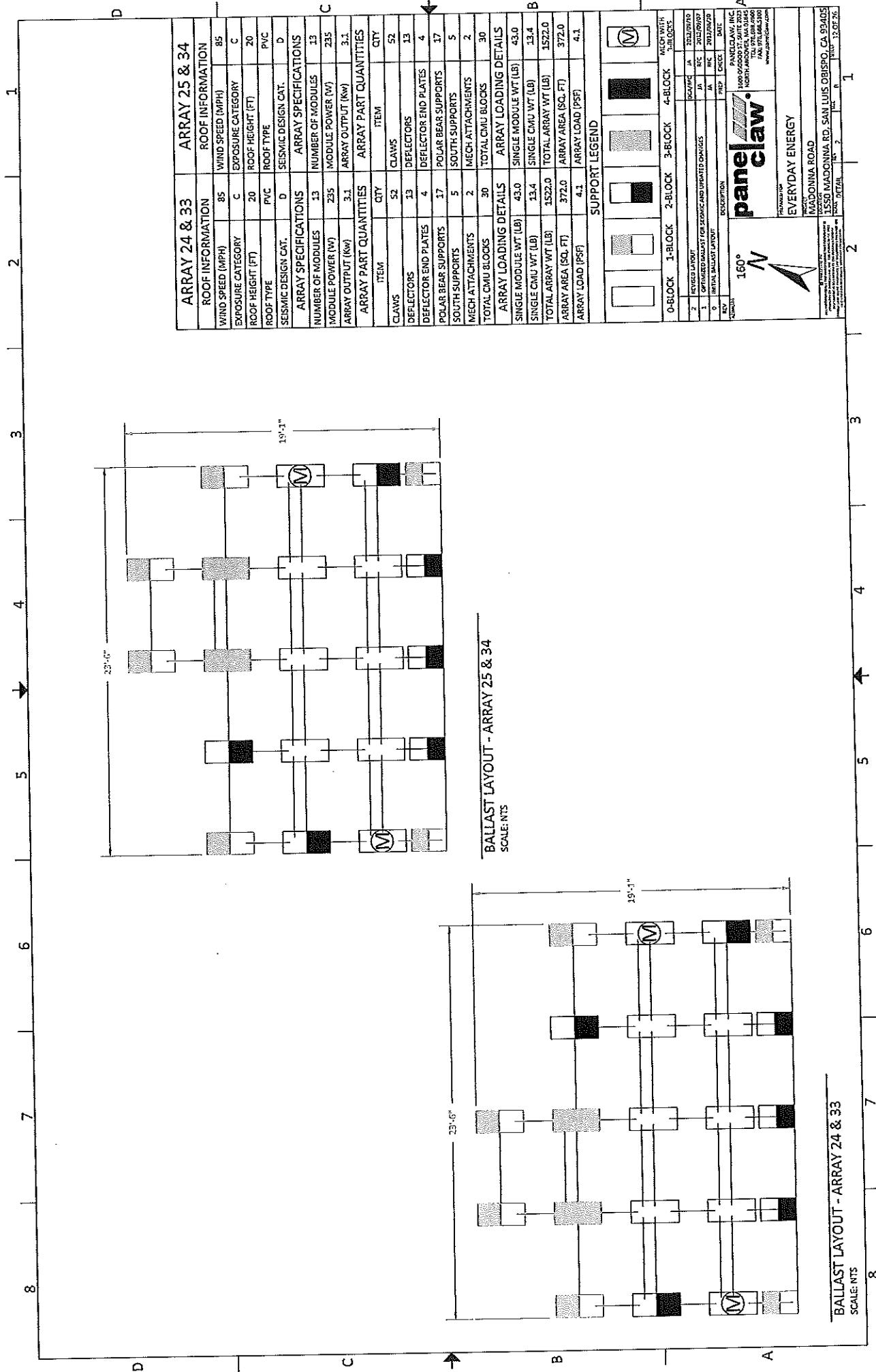


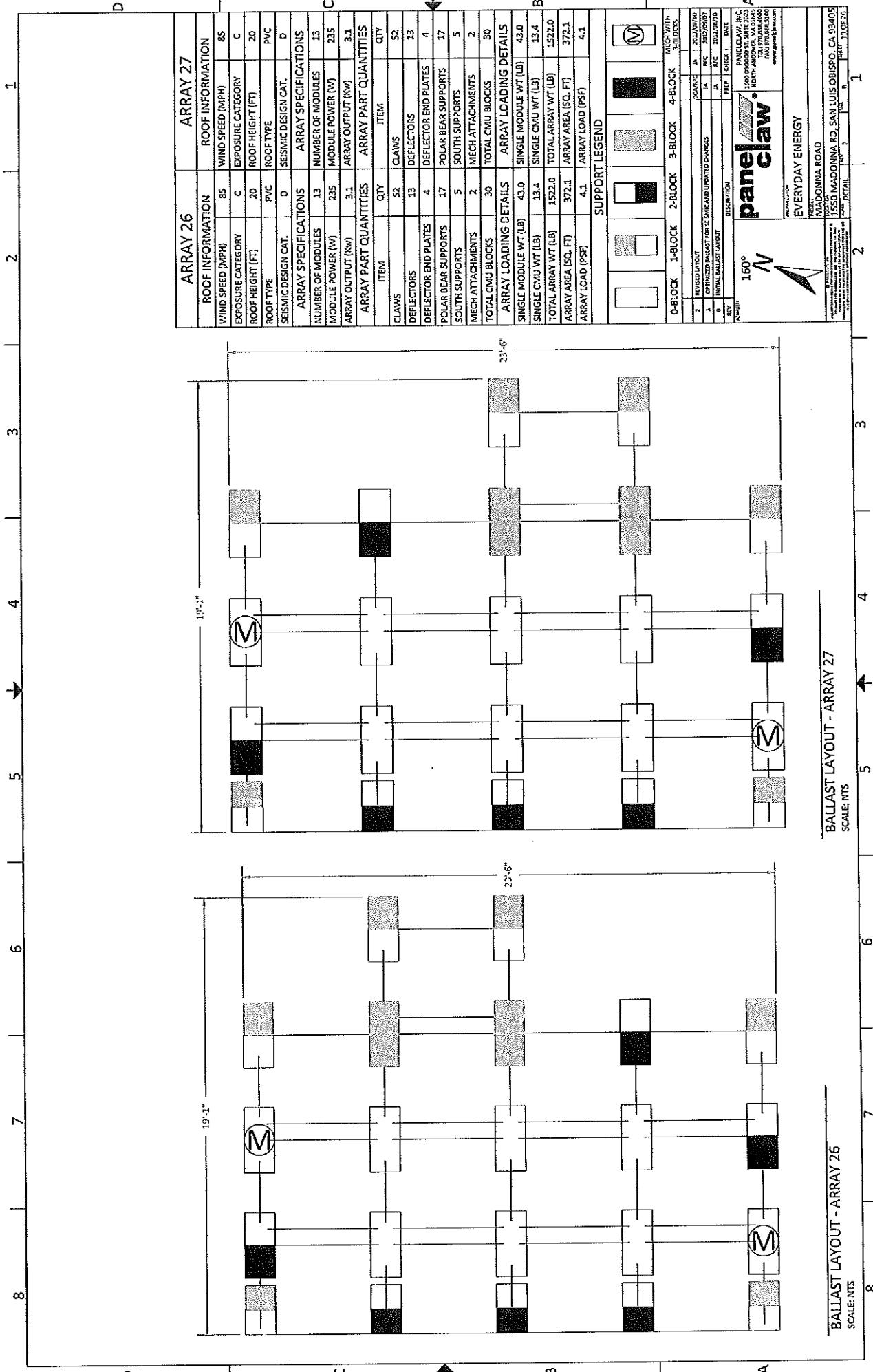


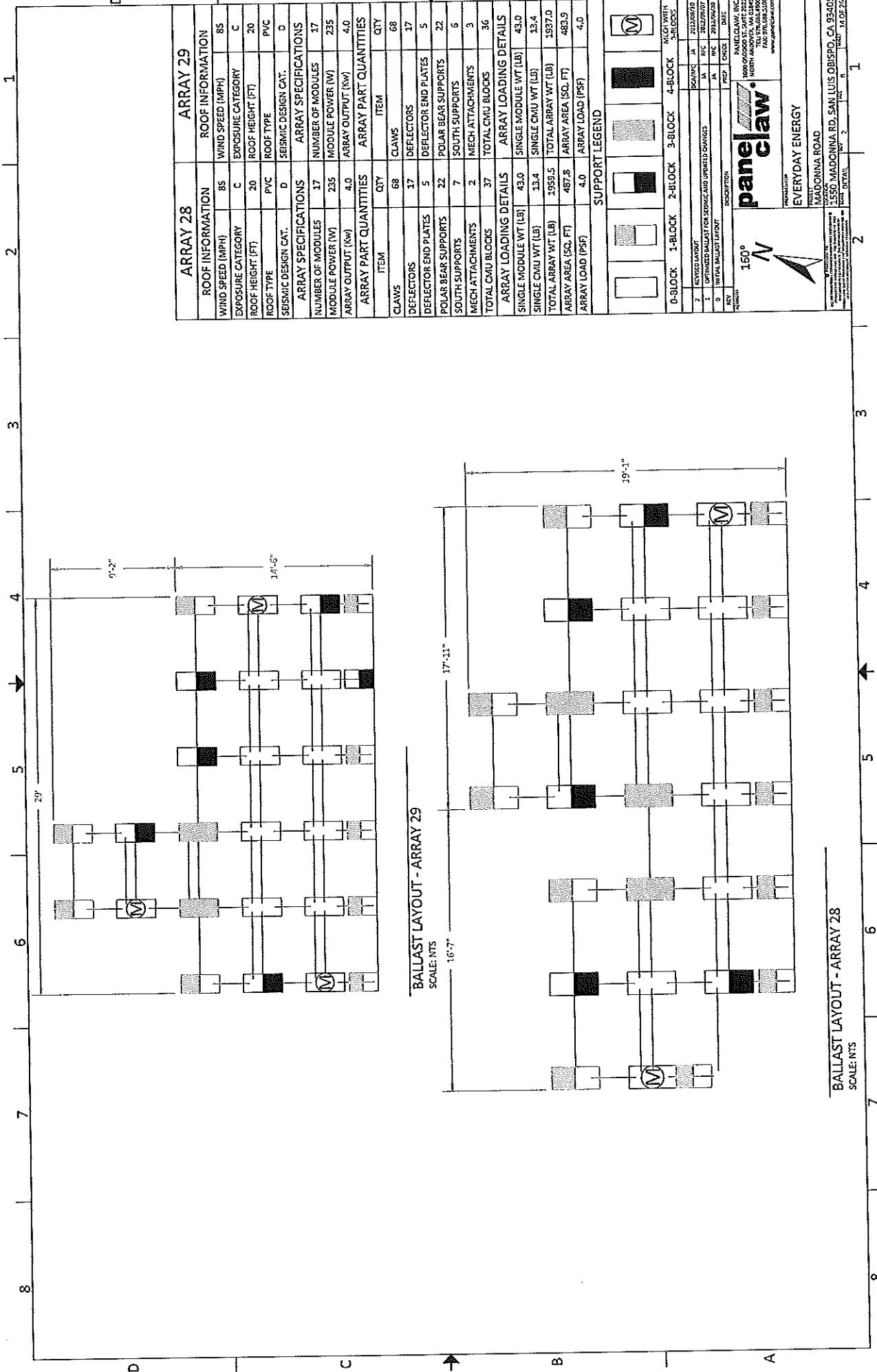


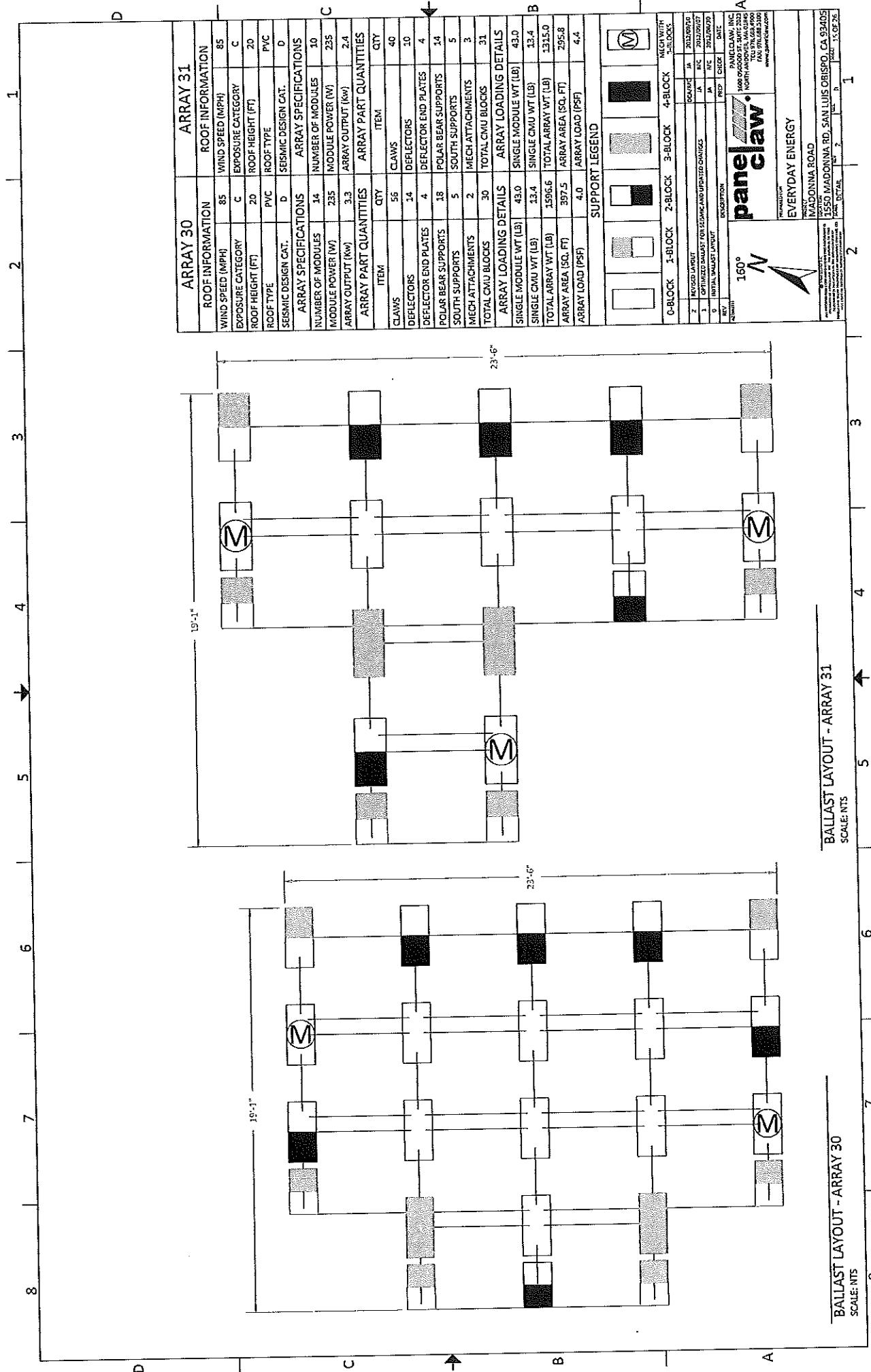


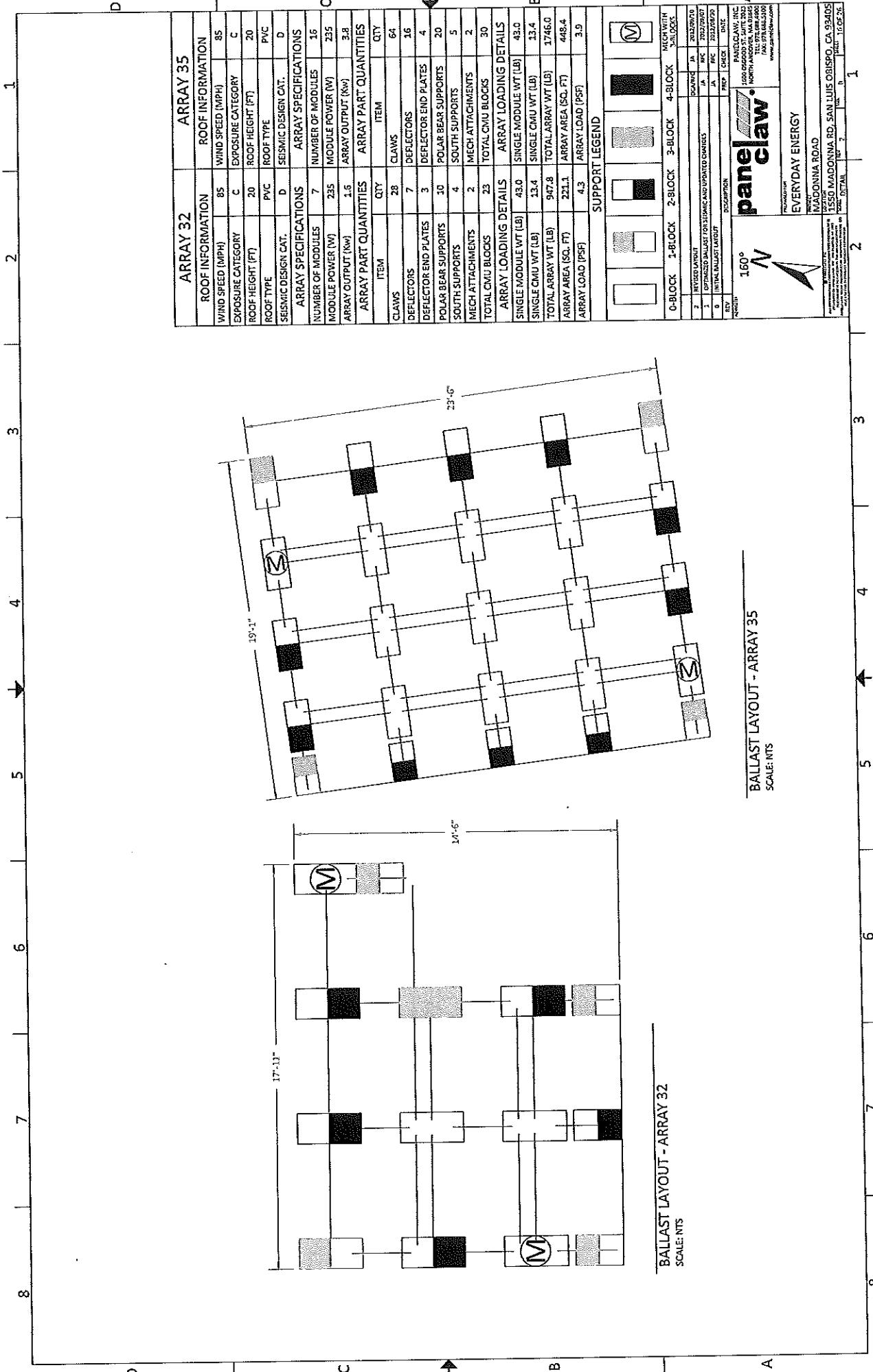


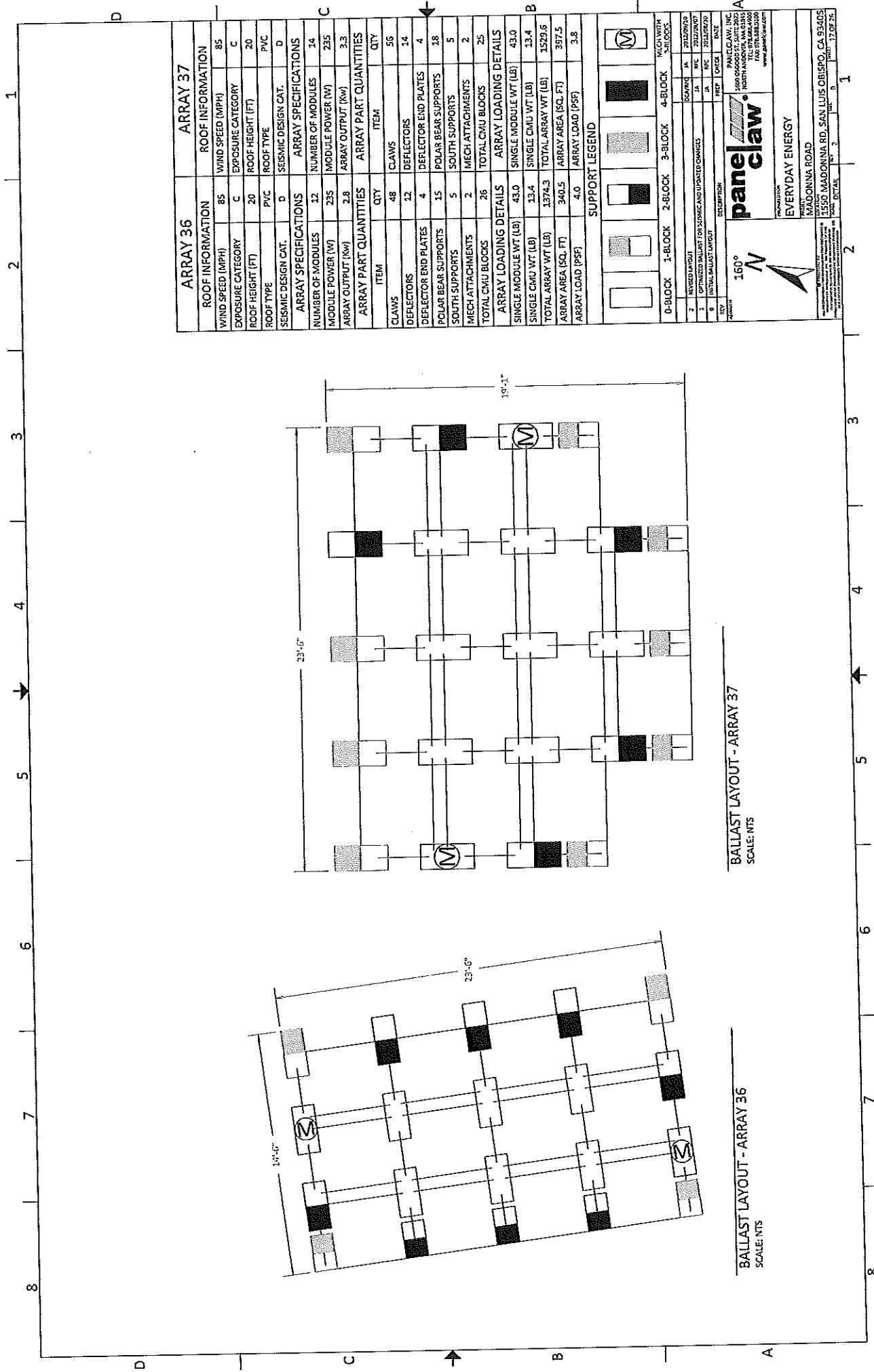


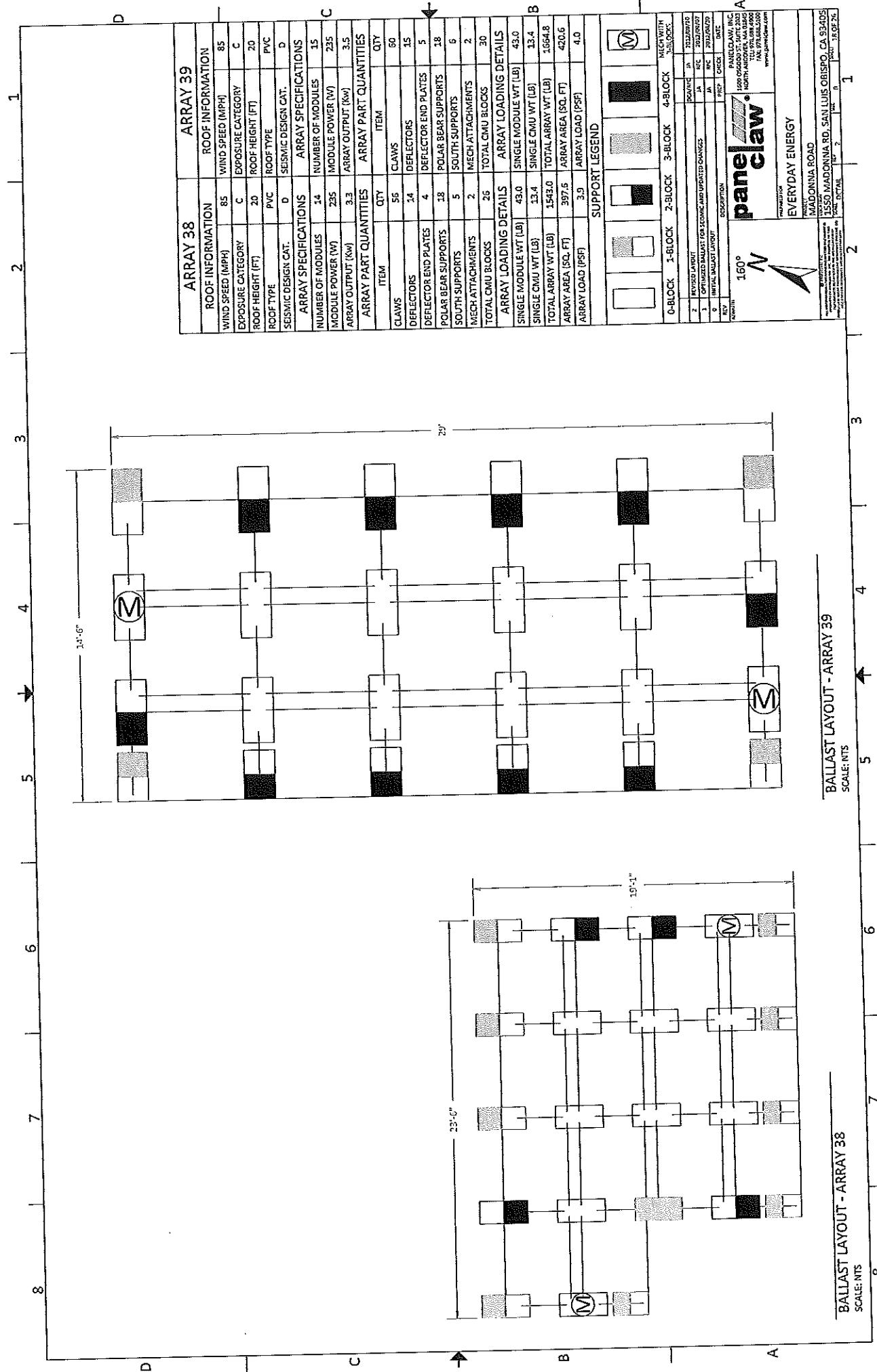
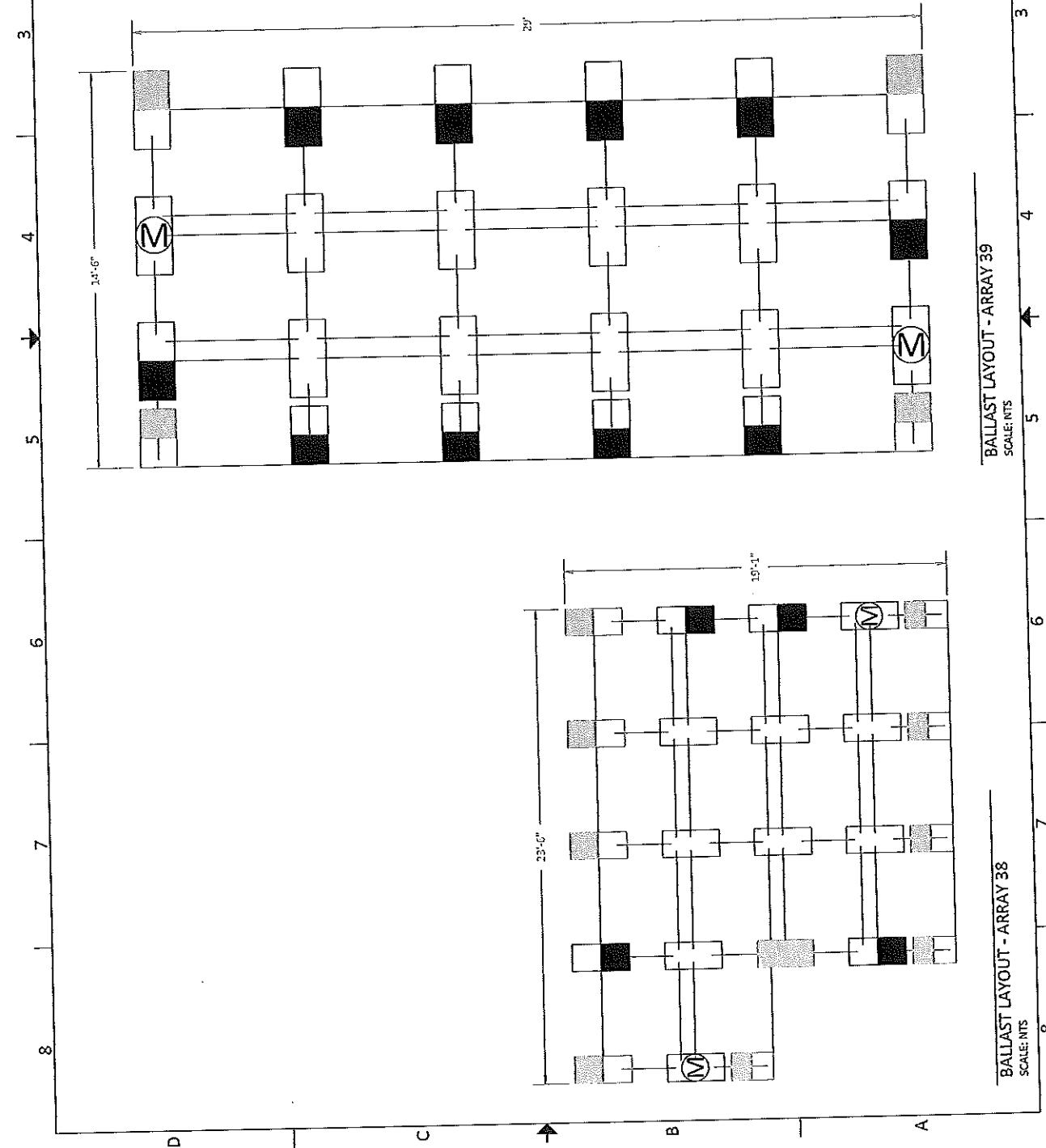




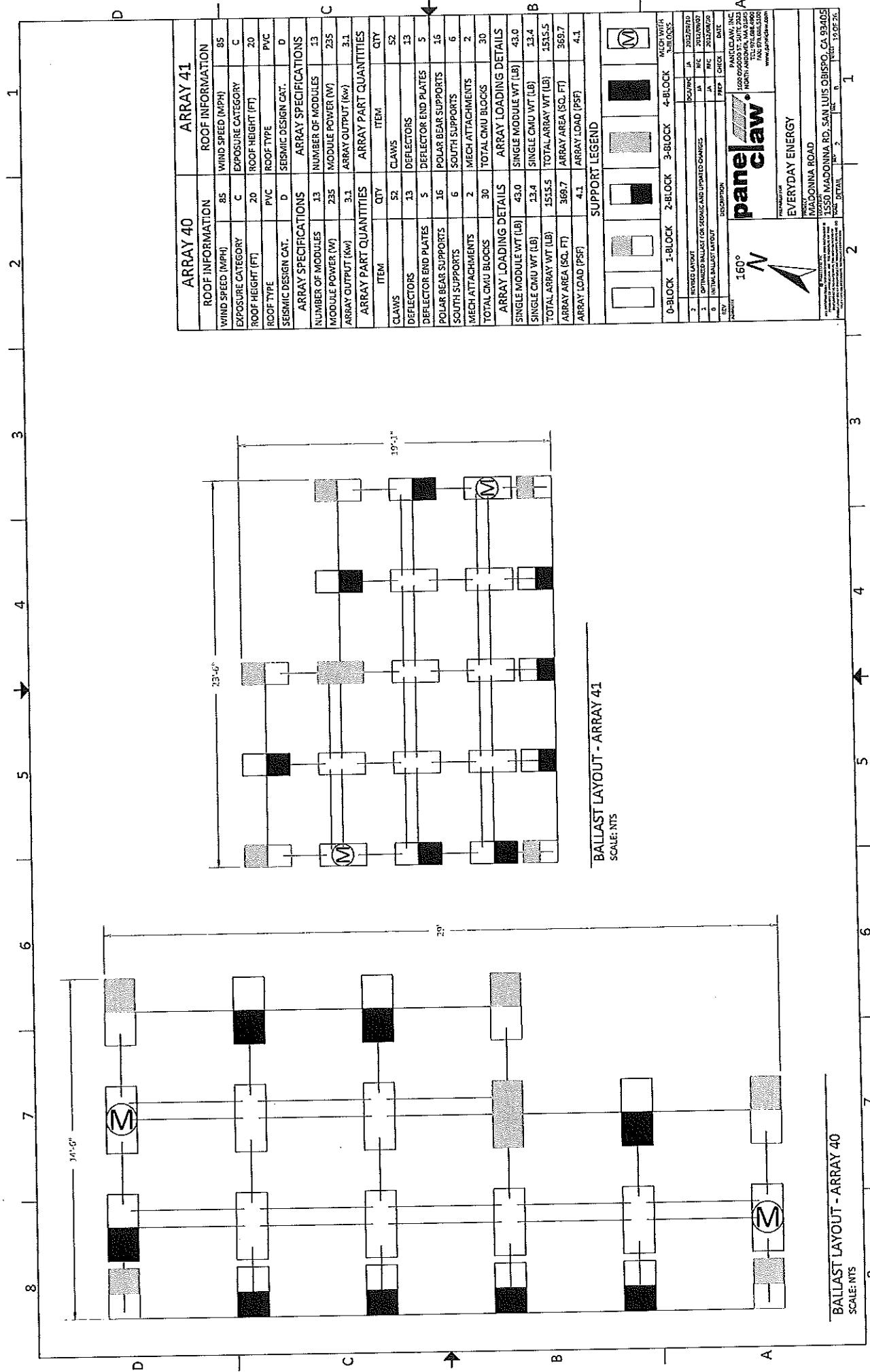


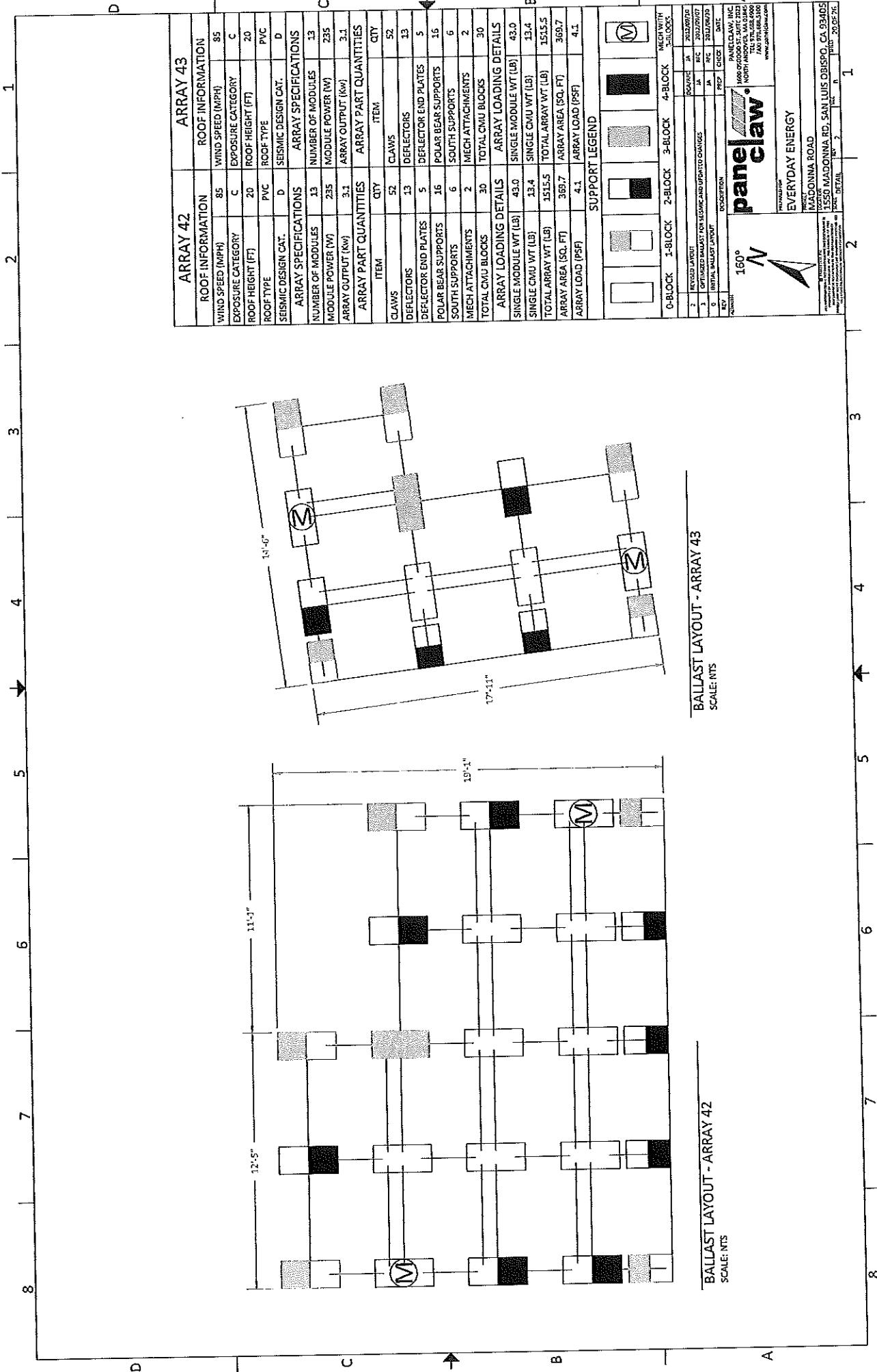


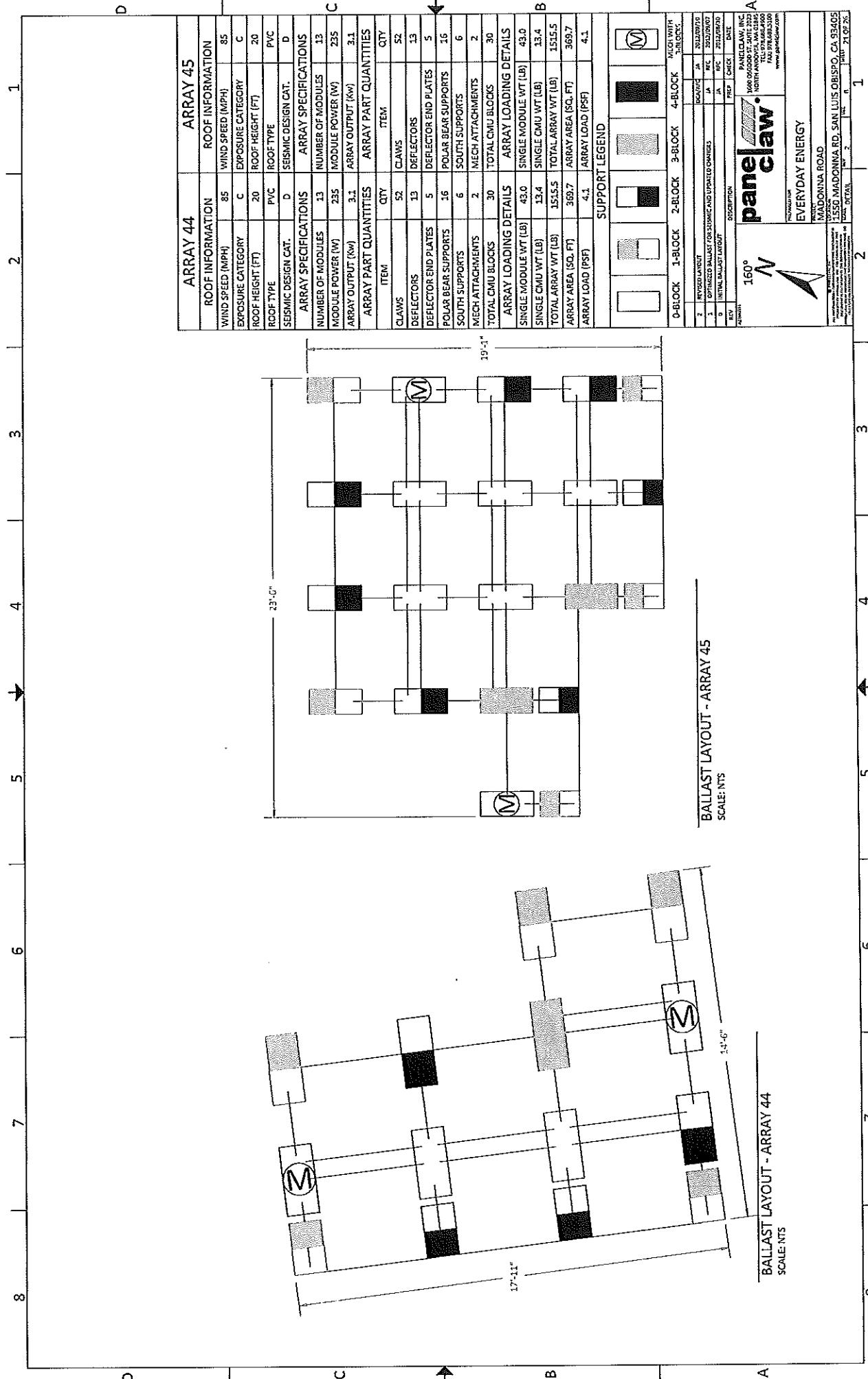


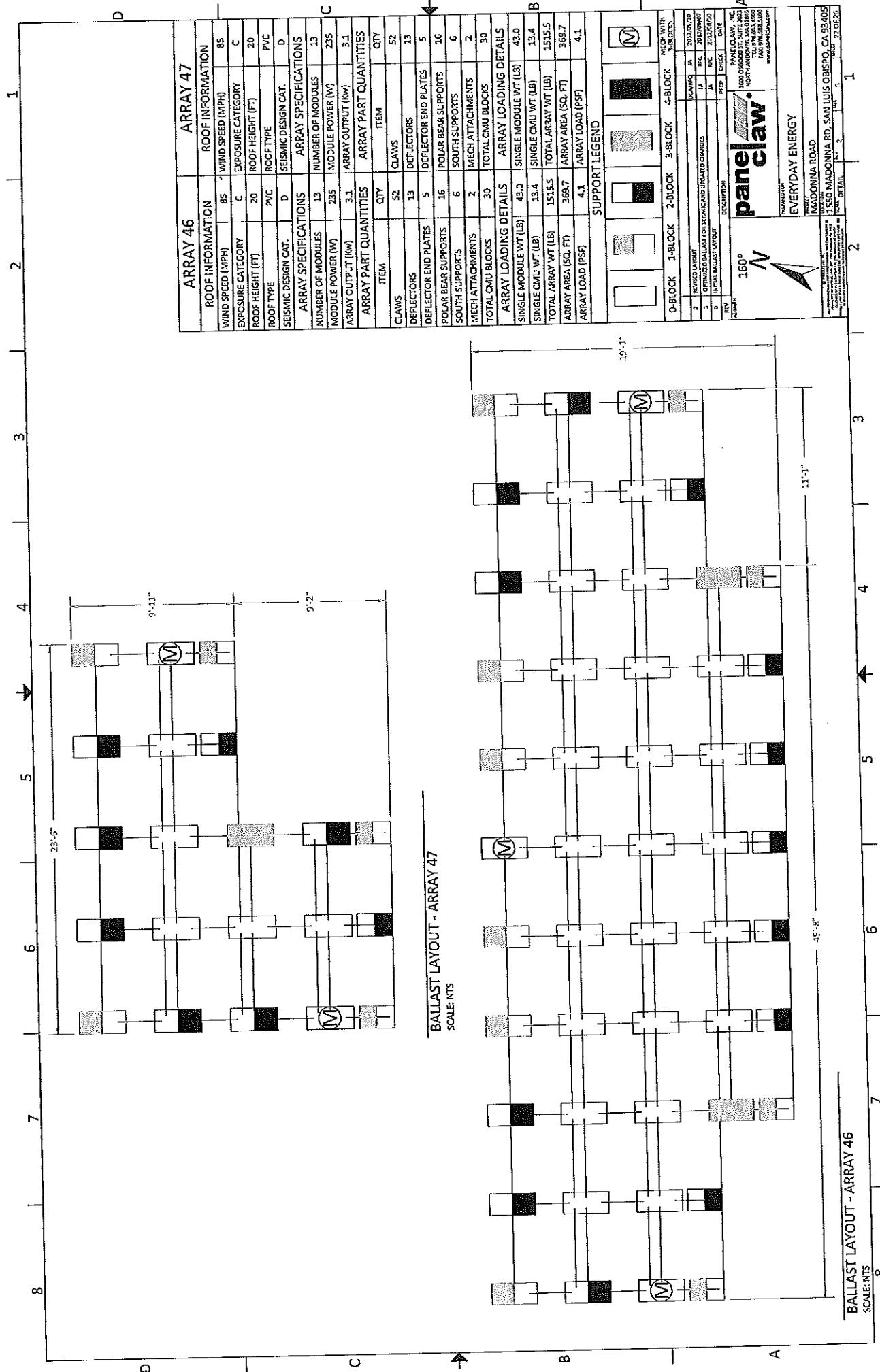


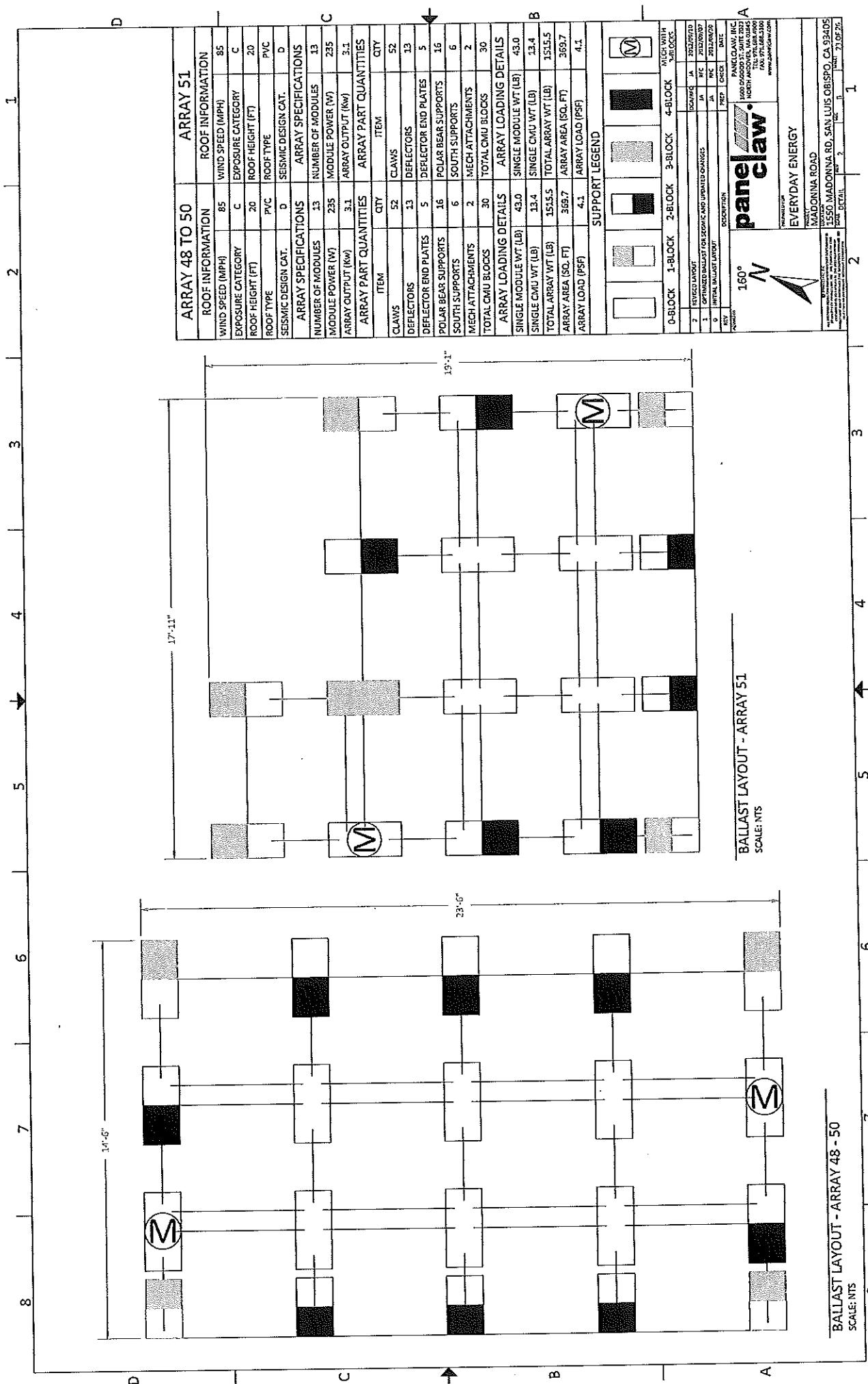
2-18

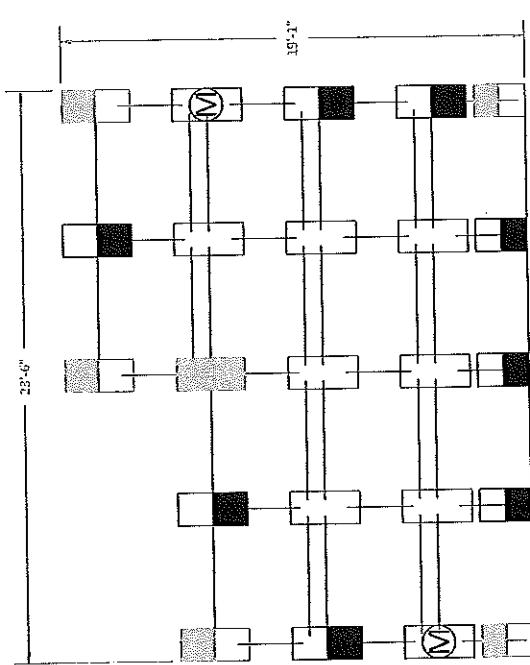




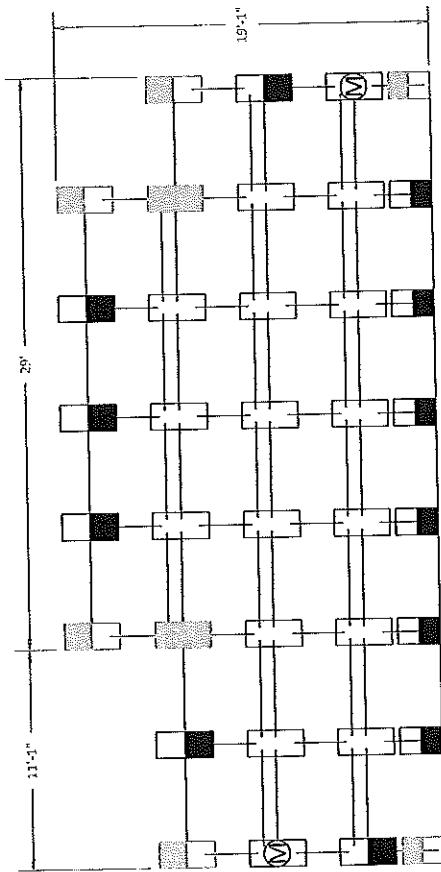








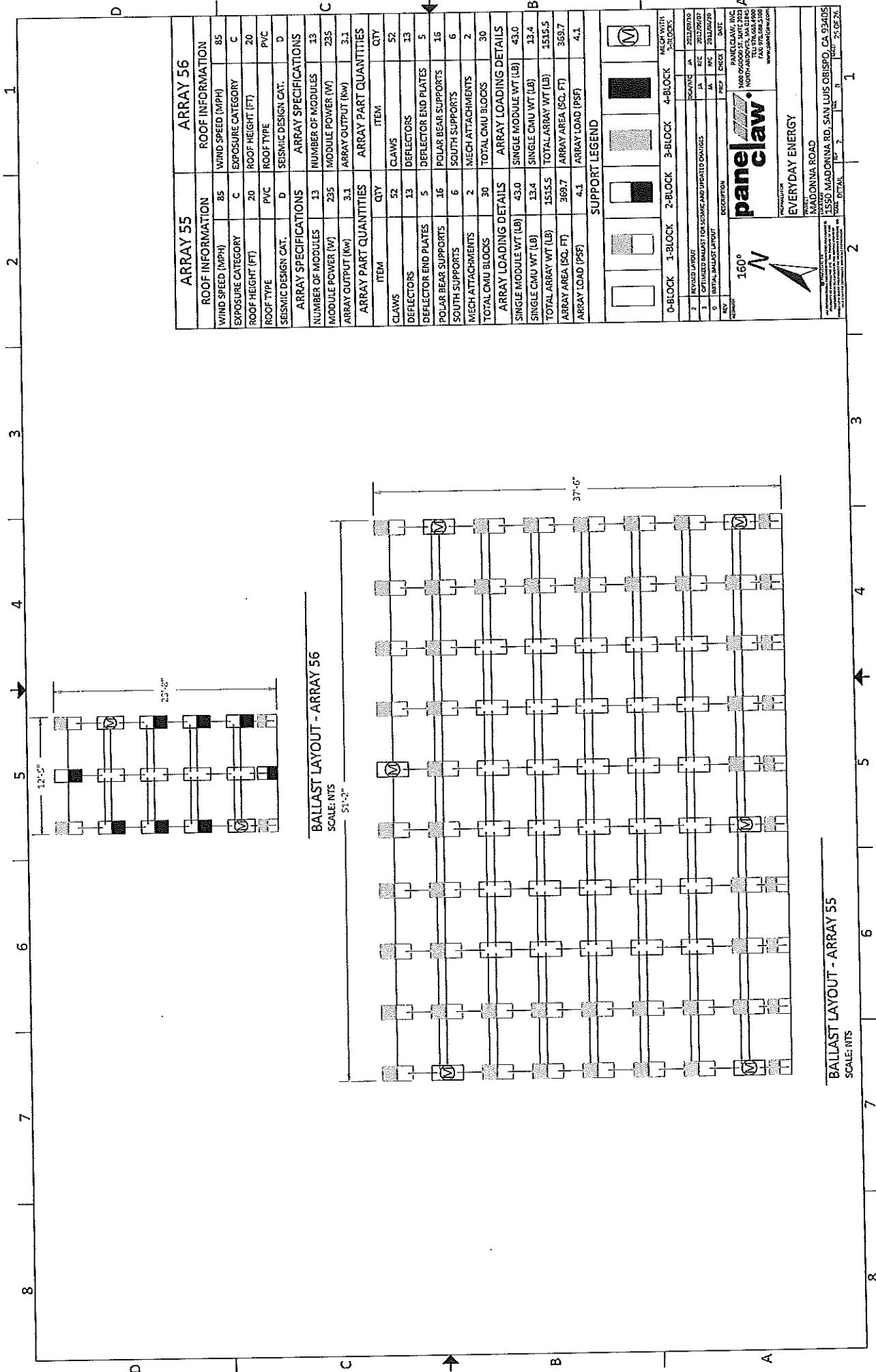
**BALLAST LAYOUT - ARRAY 54**

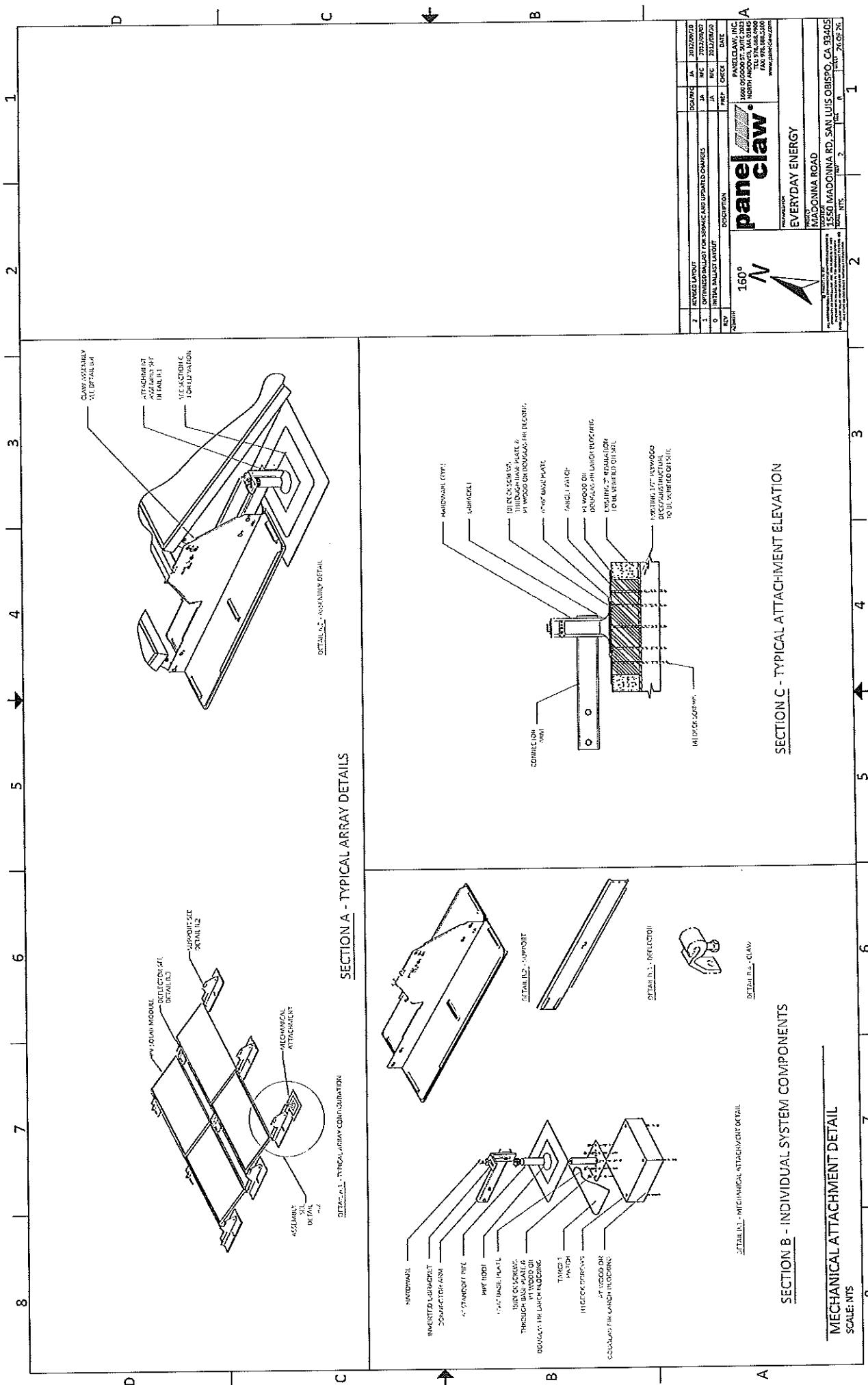


BALLAST LAYOUT - ARRAY 52 & 53

ARRAY 52 & 53							ARRAY 54	
ROOF INFORMATION				ROOF INFORMATION				
WIND SPEED (MPH)	35	WIND SPEED (MPH)	85					
EXPOSURE CATEGORY	C	EXPOSURE CATEGORY	C					
ROOF HEIGHT (FT)	20	ROOF HEIGHT (FT)	20					
ROOF TYPE	PVC	ROOF TYPE	PVC					
SEISMIC DESIGN CAT.	D	SEISMIC DESIGN CAT.	D					
ARRAY SPECIFICATIONS		ARRAY SPECIFICATIONS						
NUMBER OF MODULES	13	NUMBER OF MODULES	13					
MODULE POWER (W)	235	MODULE POWER (W)	235					
ARRAY OUTPUT (kW)	3.1	ARRAY OUTPUT (kW)	3.1					
ARRAY PART QUANTITIES			ARRAY PART QUANTITIES					
ITEM	QTY	ITEM	QTY	ITEM	QTY	ITEM	QTY	
CLAWS	52	CLAWS	52	DEFLECTORS	13	DEFLECTORS	13	
DEFLECTOR END PLATES	5	DEFLECTOR END PLATES	5	POLAR BEAR SUPPORTS	16	POLAR BEAR SUPPORTS	16	
SOUTH SUPPORTS	6	SOUTH SUPPORTS	6	MECH ATTACHMENTS	2	MECH ATTACHMENTS	2	
TOTAL CMU BLOCKS	30	TOTAL CMU BLOCKS	30					
ARRAY LOADING DETAILS								
ARRAY MODULE WT (LB)		SINGLE MODULE WT (LB)		SINGLE CMU WT (LB)		4-BLOCK		
43.0		43.0		43.0		WITH WITH 3-BLOCKS		
SINGLE CMU WT (LB)		13.4		13.4				
TOTAL ARRAY WT (LB)		1515.5		1515.5				
ARRAY AREA (SQ. FT)		369.7		ARRAY AREA (SQ. FT)		369.7		
ARRAY LOAD (PSF)		4.1		ARRAY LOAD (PSF)		4.1		
SUPPORT LEGEND								
0-BLOCK	1-BLOCK	2-BLOCK	3-BLOCK	4-BLOCK				
160°	N							
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0	1	2	3	4				
SUPPORT LEGEND								
0	1	2	3	4				
SUPPORT LEGEND								
0	1	2	3	4				
SUPPORT LEGEND								
0	1	2	3	4				
SUPPORT LEGEND								
0	1	2	3	4				
SUPPORT LEGEND								
0	1	2	3	4				
SUPPORT LEGEND								
0	1	2	3	4				
SUPPORT LEGEND								
0	1	2	3	4				
<img alt="0 icon								

SCALE: NTS





Rooftop Ballast Map in Unit Blocks																									
Weight of (1) Ballast		13.4	lbs	Ballast Per Additional Column		6	units	80.4	lbs	Tot. # of Cols:		20	Dim A	66.43	inch	Ballast Load		0.69	psf	Total Ballast Weight		6994.8	lbs		
Zero Ballast Threshold		1	lbs	Ballast Per Additional Row		22	units	294.8	lbs	Tot. # of Rows:		20	Dim B	55.15	inch	Dead Load		3.03	psf	Total Dead Load Weight		30797.12	lbs		
Total Ballast Required		1791	lbs	Total Ballast Calculated		2439	lbs	Over Ballast Amount		648	lbs	Edge Zone Columns:		0	Rep. Area (A'B)	25.4418	sf	Total Platform Load		3.71	psf	Total Platform Weight		37791.92	lbs
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0						
Req: 0.00	lbs	Used: 0.00	lbs	Req: 0.00	lbs	Used: 0.00	lbs	Req: 0.00	lbs	Used: 0.00	lbs	Req: 0.00	lbs	Used: 0.00	lbs	Req: 0.00	lbs	Used: 0.00	lbs						
Over: 0.00	lbs	Over: 0.00	lbs	Over: 0.00	lbs	Over: 0.00	lbs	Over: 0.00	lbs	Over: 0.00	lbs	Over: 0.00	lbs	Over: 0.00	lbs	Over: 0.00	lbs	Over: 0.00	lbs						
0	1	2	1	2	1	2	1	2	1	2	1	2	1	2	1	2	1	2	0						
Req: 0.00	lbs	Used: 0.00	lbs	Req: 42.61	lbs	Used: 53.60	lbs	Req: 2.83	lbs	Used: 23.45	lbs	Req: 2.83	lbs	Used: 20.10	lbs	Req: 2.83	lbs	Used: 23.45	lbs	Req: 42.61	lbs				
Over: 0.00	lbs	Over: 10.99	lbs	Over: -2.41	lbs	Over: 20.62	lbs	Over: 17.27	lbs	Over: 17.27	lbs	Over: 17.27	lbs	Over: 17.27	lbs	Over: 17.27	lbs	Over: 20.62	lbs	Over: 4.29	lbs				
0	2	4	2	4	2	4	2	4	2	4	2	4	2	4	2	4	2	4	0						
Req: 0.00	lbs	Used: 0.00	lbs	Req: 42.61	lbs	Used: 53.60	lbs	Req: 2.83	lbs	Used: 20.10	lbs	Req: 2.83	lbs	Used: 13.40	lbs	Req: 2.83	lbs	Used: 20.10	lbs	Req: 42.61	lbs				
Over: 0.00	lbs	Over: 10.99	lbs	Over: -2.41	lbs	Over: 17.27	lbs	Over: 10.57	lbs	Over: 10.57	lbs	Over: 10.57	lbs	Over: 10.57	lbs	Over: 17.27	lbs	Over: 40.20	lbs	Over: 10.99	lbs				
0	2	4	2	4	2	4	2	4	2	4	2	4	2	4	2	4	2	4	0						
Req: 0.00	lbs	Used: 0.00	lbs	Req: 48.12	lbs	Used: 53.60	lbs	Req: 9.12	lbs	Used: 23.45	lbs	Req: 9.12	lbs	Used: 13.40	lbs	Req: 9.12	lbs	Used: 23.45	lbs	Req: 48.12	lbs				
Over: 0.00	lbs	Over: 5.48	lbs	Over: -4.57	lbs	Over: 14.33	lbs	Over: 4.28	lbs	Over: 10.05	lbs	Over: 10.05	lbs	Over: 10.05	lbs	Over: 4.28	lbs	Over: 14.33	lbs	Over: 5.48	lbs				
0	2	4	2	4	2	4	2	4	2	4	2	4	2	4	2	4	2	4	0						
Req: 0.00	lbs	Used: 0.00	lbs	Req: 48.12	lbs	Used: 53.60	lbs	Req: 9.12	lbs	Used: 26.80	lbs	Req: 9.12	lbs	Used: 13.40	lbs	Req: 9.12	lbs	Used: 26.80	lbs	Req: 48.12	lbs				
Over: 0.00	lbs	Over: 5.48	lbs	Over: -1.22	lbs	Over: 17.68	lbs	Over: 4.28	lbs	Over: 6.70	lbs	Over: 6.70	lbs	Over: 6.70	lbs	Over: 4.28	lbs	Over: 17.68	lbs	Over: 5.48	lbs				
0	2	4	2	4	2	4	2	4	2	4	2	4	2	4	2	4	2	4	0						
Req: 0.00	lbs	Used: 0.00	lbs	Req: 48.12	lbs	Used: 53.60	lbs	Req: 9.12	lbs	Used: 30.15	lbs	Req: 9.12	lbs	Used: 20.10	lbs	Req: 9.12	lbs	Used: 30.15	lbs	Req: 48.12	lbs				
Over: 0.00	lbs	Over: 5.48	lbs	Over: -1.22	lbs	Over: 21.03	lbs	Over: 10.98	lbs	Over: 13.40	lbs	Over: 13.40	lbs	Over: 13.40	lbs	Over: 10.98	lbs	Over: 21.03	lbs	Over: 5.48	lbs				
0	2	4	2	4	2	4	2	4	2	4	2	4	2	4	2	4	2	4	0						
Req: 0.00	lbs	Used: 0.00	lbs	Req: 41.24	lbs	Used: 53.60	lbs	Req: 41.24	lbs	Used: 46.90	lbs	Req: 41.24	lbs	Used: 46.90	lbs	Req: 41.24	lbs	Used: 46.90	lbs	Req: 41.24	lbs				
Over: 0.00	lbs	Over: 12.35	lbs	Over: 9.01	lbs	Over: 2.31	lbs	Over: 9.50	lbs	Over: 7.74	lbs	Over: 9.50	lbs	Over: 2.31	lbs	Over: 9.50	lbs	Over: 7.74	lbs	Over: 12.35	lbs				
0	2	4	2	4	2	4	2	4	2	4	2	4	2	4	2	4	2	4	0						
Req: 0.00	lbs	Used: 0.00	lbs	Req: 41.24	lbs	Used: 53.60	lbs	Req: 41.24	lbs	Used: 53.60	lbs	Req: 41.24	lbs	Used: 40.20	lbs	Req: 41.24	lbs	Used: 53.60	lbs	Req: 41.24	lbs				
Over: 0.00	lbs	Over: 12.35	lbs	Over: 12.35	lbs	Over: 12.35	lbs	Over: 12.35	lbs	Over: 1.04	lbs	Over: 12.85	lbs	Over: 9.50	lbs	Over: 12.85	lbs	Over: -1.04	lbs	Over: 12.35	lbs				
0	1	2	1	2	1	2	1	2	1	2	1	2	1	2	1	2	1	2	0						
Req: 0.00	lbs	Used: 0.00	lbs	Req: 0.00	lbs	Used: 0.00	lbs	Req: 0.00	lbs	Used: 0.00	lbs	Req: 0.00	lbs	Used: 0.00	lbs	Req: 0.00	lbs	Used: 0.00	lbs	Req: 0.00	lbs				
Over: 0.00	lbs	Over: 0.00	lbs	Over: 0.00	lbs	Over: 0.00	lbs	Over: 0.00	lbs	Over: 0.00	lbs	Over: 0.00	lbs	Over: 0.00	lbs	Over: 0.00	lbs	Over: 0.00	lbs	Over: 0.00	lbs				
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0						
Repeatable Column																									

Total Ballast 182

Drop Down Inputs	
Direct Inputs	
Calculated Field	
DO NOT OVERRIDE ANY CALCULATED FIELDS	
Company Name	EVERYDAY ENERGY
Project Name	MADONNA ROAD
Project Address (City,State)	1550 MADONNA RD, SAN LUIS OBISPO, CA
ZIPCODE	93405

DO NOT OVERRIDE ANY CALCULATED FIELDS

Site Specific Seismic Conditions						
S1	1.516	Fa	1.00	Site Class	D	Mech. Attach. Vertical Strength (lb)
S1	0.555	Fv	1.50			Mech. Attach. Lateral Strength (lb)

PRODUCT				
PRODUCT	TILT ANGLE	MATERIAL	SUPPORT OPTIONS	ROW SPACING/SHADE CONFIGURATION
<input checked="" type="checkbox"/> BEAR GEN II <input checked="" type="checkbox"/> BEAR GEN II <input checked="" type="checkbox"/> END BEAR <input checked="" type="checkbox"/> END (TBD) <input checked="" type="checkbox"/> END BEAR	0°	STEEL	0° <input checked="" type="checkbox"/> SOUTH SUPPORT	0°
Total Number of Arrays	56			
SITE INFORMATION				
WIND SPEED (MPH)	85	CALCULATED SDC		
EXPOSURE CATEGORY	C	0		
SEISMIC DESIGN CATEGORY	D			
OCCUPANCY CATEGORY	B			
GROUND SNOW LOAD (PSF)	0			
BUILDING INFORMATION				
ROOF HEIGHT	20	Width of the building (N/S) (feet):	120	
ROOF TYPE	FLAT	Length of the building (E/W) (feet):	128	
ROOF TILT	0	Parapet Height (ft) (feet):		
NOTE: MODIFY INDIVIDUAL ARRAY DETAILS IN "ACAD TABLES" TAB				

ENTER PROJECT SPECIFIC NOTES BELOW THAT MAY/MAY NOT BE ON THE ARRAY INTAKE FORM		REVISION NUMBER
Using 13.44 # blocks. Ex2x16. Half the size of a normal CMU block.		2
		Request Type
		PULLLIST
COPY NAMING CONVENTION BELOW TO FILE NAME		
PanelClaw_PolarBear10_Drawing_EVERYDAY ENERGY_MADONNA ROAD_RevZ_INT		

PROJECT SUMMARY										MODULE SPECIFIC INFORMATION				
PART	TYPE/PART#	DESCRIPTION/WATT	WEIGHT (LBS)	QTY	Claws Per Module	Standard Claw	Max Allowable Load (psf)	COMBINED WIND/SNOW LOAD (COMBO #S OF 2.4)	UL APPROVED MODULE	Module "A" Dimension (in.)	Module "B" Dimension (in.)	MODULE WIDTH (inches) If Not Approved Manually enter below the Calculated Field	MODULE LENGTH (inches) If Not Approved Manually enter below the Calculated Field	
MODULE	Trina Solar - ISMA PV-PAD02-205	235	43	855	4	Standard Claw	50	10.82	Y	66.43	55.15	0.99	1.65	
COMBINED LOAD CANNOT EXCEED THE MAX ALLOWABLE LOAD. IF SO DETERMINE BEST POSSIBLE SOLUTION. (SPEAK WITH SALES)														
CLAW	500005	ASSY, CLAW-STANDARD, ALUMINUM	0.25	3420										
[NORTH] SUPPORT	500062	SUPPORT, G90 ST, 304SS, POLAR BEAR GEN II 10 DEG	19.44	1062										
[MIDDLE] SUPPORT	N/A	N/A	0	0										
SOUTH SUPPORT	500036	EMBLY, SUPPORT, SOUTH, G90ST, POLAR/GRIZZLY, 10 DEG	12.75	309										
DEFLECTOR	200016804	DEFLECTOR, G90 ST, 69°, POLAR/GRIZZLY BEAR GEN II 10 DEG	11.22	855										
MECHANICAL ATTACHMENT	5000070	MACHICAL ATTACHMENT, 6' x 6' x 6'1" WITH 3" LO	3.56	120										
END PLATE	2000140	ATE, G90 STEEL, POLAR BEAR / GRIZZLY BEAR GEN II	0.19	244										
X-BRACE	N/A	N/A	0	0										
CMU BLOCK	IF Only Grizzly Bear layout, Put "0" as the CMU block weight ==>				13.4	1777								

5/10 DEGREE COUNTS TABLE														
BLOCK COUNT FOR SUPPORT MECHANICAL ATTACHMENT BLOCK COUNT MAX X SIZE MAX COUNT TOWARDS THE OVERALL BLOCKSIZE DO NOT COUNT REPEATS														
Array #	Module Count	End Plates	0/Grizzly	1	2	3	4	5	6	7	8	9	10	11
1	4	2	1	1	2	0			2	1				3
2	4	2	1	1	2	0			2	4				6
3	18	5	9	4	5	3			23	9				11
4	20	7	20	8	4	3			43	2				5
5	15	5	7	4	5	2			20	3				5
6	8	2	3	2	3	0			10	0				5
7	8	4	3	2	3	0			10	2				9
8	20	8	9	3	1				24	0				5
9	14	4	13	7	6	2			0	2	3			30
10	32	4	13	7	6	1			18	0	4			11
11	14	4	7	2	2	1			18	0	3	1		4
12	7	3	2	2	2	1			10	0	3	1		4
13	7	3	2	2	2	1			10	0	2	3		5
14	15	5	7	4	5	2			20	0	2	3		6
15	15	6	6	1	1				16	0	3	3		6
16	13	5	9	6	3	1			21	0	3	3		6
17	17	5	2	6	1				16	0	4	1		5
18	12	4	5	2	6	1			18	0	4	1		5
19	14	4	7	2	5	2			15	0	3	2		32
20	11	4	3	3	5	2			43	0	5	2		7
21	31	12	14	5	17	5			19	0	3	2		5
22	14	5	6	3	7	1			2	0	3	0		3
23	7	4	2	2	4	1			11	0	2	3		5
24	13	4	6	4	3	2			17	0	2	3		5
25	13	4	6	4	3	2			17	0	2	3		5
26	13	4	6	4	3	2			17	0	2	3		5
27	13	4	6	4	3	2			22	0	7	0		7
28	17	5	7	5	3	2			3	0	5	1		6
29	17	5	8	4	5	2			18	0	4	1		5
30	14	4	7	4	5	2			14	0	4	1		5
31	10	3	2	4	2	1			10	0	3	1		4
32	7	3	2	1	2				17	0	2	3		5
33	13	6	4	3	2				17	0	2	3		5
34	13	6	4	3	2				20	0	2	3		5
35	16	9	2	7	0				15	0	2	3		5
36	12	6	2	5	0									

Required Mechanical Attachments For Vertical Uplift			MECH. ATTACH. REQUIRED FOR SEISMIC			RATIO		
Required CMU Weight (\$)	CMU Block Wt. (lb.)	Actual vs. Required CMU wt. (\$)	REQUIRED MA'S	(Default)W/O FRICTION	WITH FRICTION	Support to Module Ratio	Ratio Check	Variance of MA's (Must be 0 or Higher)
184.3	201	-17	1	1	1	2.25	Too High!	1
184.3	201	-17	1	1	1	2.25	Too High!	1
840	522.6	317	1	2	1	1.61	OK	0
1521.3	871	650	1	3	1	1.50	OK	0
700.5	455.6	245	1	1	1	1.67	OK	1
371.2	294.8	76	1	1	1	1.88	OK	1
328.8	294.8	34	1	1	1	1.88	OK	1
832.8	616.4	216	1	2	1	1.65	OK	0
626	415.4	211	1	1	1	1.64	OK	1
1133	656.6	476	1	2	1	1.47	OK	0
583.5	402	182	1	1	1	1.64	OK	1
289	294.8	-6	1	1	1	2.00	OK	1
289	294.8	-6	1	1	1	2.00	OK	1
626	455.6	170	1	1	1	1.67	OK	1
626	455.6	170	1	1	1	1.67	OK	1
662.7	348.4	114	1	1	1	1.69	OK	1
629.8	402	228	1	1	1	1.59	OK	1
498.6	338.6	110	1	1	1	1.75	OK	1
583.5	402	182	1	1	1	1.64	OK	1
595.9	428.8	167	1	1	1	1.82	OK	1
1390.5	924.6	456	1	2	1	1.61	OK	0
595.9	442.2	154	1	1	1	1.71	OK	1
291.8	294.8	-3	1	1	1	2.00	OK	1
541.1	402	139	1	1	1	1.69	OK	1
541.1	402	139	1	1	1	1.69	OK	1
541.1	402	139	1	1	1	1.69	OK	1
628.4	495.8	133	1	2	1	1.71	OK	0
630.9	482.4	149	1	2	1	1.65	OK	1
583.5	402	182	1	1	1	1.64	OK	1
413.7	415.4	-2	1	1	1	1.90	OK	2
290.4	308.2	-18	1	1	1	2.00	OK	1
541.1	402	139	1	1	1	1.69	OK	1
541.1	402	139	1	1	1	1.69	OK	1
658.4	402	265	1	1	1	1.56	OK	1
498.6	348.4	150	1	1	1	1.67	OK	1
500	335	173	1	1	1	1.64	OK	1
493.7	348.4	145	1	1	1	1.64	OK	1
623.3	402	221	1	1	1	1.60	OK	1
538.3	402	135	1	1	1	1.69	OK	1
583.5	402	182	1	1	1	1.64	OK	1
498.6	402	97	1	1	1	1.75	OK	1
289	294.8	-6	1	1	1	2.00	OK	1
289	294.8	-6	1	1	1	2.00	OK	1
500	415.4	85	1	1	1	1.75	OK	1
1183.8	633.4	500	1	1	1	1.42	OK	2
541.1	402	139	1	1	1	1.75	OK	1
498.6	318.4	150	1	1	1	1.67	OK	1
498.6	348.4	150	1	1	1	1.67	OK	1
498.6	348.4	150	1	1	1	1.67	OK	1
416.4	348.4	68	1	1	1	1.80	OK	1
1002.7	562.8	402	1	1	1	1.48	OK	1
1002.7	562.8	402	1	1	1	1.48	OK	1
583.5	402	182	1	1	1	1.64	OK	1
430.1	830.8	-601	1	1	1	1.25	OK	5
2525.3	348.4	2177	4	1	1	1.80	OK	-2

34649.7 23811.8 10837.9 57 DIV/0! DIV/0! 1.27 OK

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Array Informations		
qty	item	weight
4	Modules + Deflectors	54.22
15	Ballast CMU Block	13.4
6	North Support	19.44
3	South Support	12.75
0	Middle Support	0.0
	% of Mechanical Attachments to Supports Ratio	11%
	area, SQFT	123
	total weight, LBS	573
	total load, PSF	4.7
	total mech attach	1

**ASCE 7-05 Seismic Worksheet for Non-Structural Members****11.4 Seismic Ground Motion Values**

Description	Symbol	Input Values	Sections/Figures / Comments
Zip Code	93405	1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
<b>11.4.1 Mapped acceleration parameters</b>			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F. D is default if site soil properties unknown - See table 20.3.1
<b>11.4.2 Site Class</b>	D		
<b>11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters</b>			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4, Fv*S1
<b>11.4.4 Design Spectral Acceleration Parameters</b>			
Short Periods	Sds	1.01	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

**13.1 Seismic Design Requirements for Nonstructural components**

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

## General Design Requirements

13.2	Description	Symbol	Value/Comment
13.2.1	Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections 13.2, 13.3, 13.4, 13.5
13.2.2	Special Certification Requirements		N/A
13.2.3	Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4	Flexibility		Flexibility as well as strength must be considered
13.2.5	Testing Alternative		components tested to ICC-ES AC 156 are acceptable
13.2.6	Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by table 13.2-1
13.2.7	Construction Documents		

## 13.3 Seismic Demands on Nonstructural Components

13.3.1	Seismic Design Force	Symbol	Equation	Notes
		Fp	$F_p = (0.4 * a_p * SDS^{**}W_p) / (R_p/I_p)^{*}(1+2z/h)/1.4$	Fp values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		Fph	198	
		Fpmax	926	
		Fpmin	174	
	spectral acceleration, short period [g]	SDS	1.011	
	component amplification factor (table 13.6-1)	ap	1.00	
	Component Importance Factor	Ip	1.00	
	Operating Weight (total load of array) [lbs]	Wp	573	
	Response modification Factor (table 13.5-1 or 13.6-1)	Rp	2.50	
	point of component attachment [ft]	z	25	Only ratio z/h is used, which is 1.0
	average roof height [ft]	h	25	Only ratio z/h is used, which is 1.0
	concurrent vertical load [lb]	Fv	$(.2 * SDS^{**}W_p) / 1.4$	Fv values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
			33	
	vertical resisting load	g*D_L	0.9*Wp	
			515	

### 13.3.2 Seismic Relative Displacements

13.4	Nonstructural Component Anchorage		Components shall be bolted, welded or otherwise positively fastened without consideration for frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to Fp and Rp due to anchorage conditions need not be considered
13.4.1	Design Forces		The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2

	roof attach lateral strength	628	[lbs]
	roof attach vertical strength	808	[lbs]
	Seismic Lateral Design Force, Fp	198	[lbs]
	Seismic Vertical Design Force, Fv	33	[lbs]
	total roof attachments req for lateral	1	
	total roof attachments req for vertical	1	

‡ 60% of the vertical resisting load ( $0.6^*W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.

Array Informations			
qty	item	weight	total
4	Modules + Deflectors	54.22	217
15	Ballast CMU Block	13.4	201.0
6	North Support	19.44	116.6
3	South Support	12.75	38.3
0	Middle Support	0.0	0.0
	% of Mechanical Attachments to Supports Ratio	11%	
	area, SQFT	123	
	total weight, LBS	573	
	total load, PSF	4.7	
	total mech attach	1	

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
Zip Code	93405	1520 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, short periods	S1	0.555	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	D		A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class			
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.333	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters	Output Values		
Short Periods	Sds	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
13.2	Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for Architectural, Mechanical and Electrical Components and Supports			Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements			N/A
13.2.3 Consequential Damage			cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4 Flexibility			Flexibility as well as strength must be considered
13.2.5 Testing Alternative			components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data			An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7 Construction Documents			
13.3 Seismic Demands on Nonstructural Components			
13.3.1 Seismic Design Force			$F_p = ((0.4 * a_p * SDS^2 * W_p) / (R_p / I_p)) * (1 + 2z/h) / 1.4$ Fp values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	Ibs	Fph	138
		Fpmx	926
		Fpmin	174
		SDS	1.011
		ap	1.00
		Component Importance Factor	Ip 1.00
		Operating Weight (total load of array) [lbs]	Wp 573
		Rp	2.50
		point of component attachment [ft]	z 25
		average roof height [ft]	h 25
		concurrent vertical load [lb]	Fv = (2 * SDS^2 * Wp) / 14 83
		vertical resisting load	9.9 * Wp 515
13.3.2 Seismic Relative Displacements			1
Components shall be bolted, welded or otherwise fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to Fp and Rp due to anchorage conditions need not be considered			
13.4 Nonstructural Component Anchorage			The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
13.4.1 Design Forces			
	roof attach lateral strength		628 [lbs]
	roof attach vertical strength		808 [lbs]
	Seismic Lateral Design Force, Fp		198 [lbs]
	Seismic Vertical Design Force, Fv		83 [lbs]
	total roof attachments req for lateral		1
	total roof attachments req for vertical		60% of the vertical resisting load (0.6 * Wp) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.

Array Informations			
Qty	Item	weight	total
18	Modules + Deflectors	54.22	976
39	Balast CMU Block	13.4	522.6
23	North Support	19.44	447.1
6	South Support	12.75	76.5
0	Middle Support	0.0	
	% of Mechanical Attachments to Supports Ratio	7%	
	area, SQFT	509	
	total weight, LBS	2022	
	total load, PSF	4.0	
	total mech attach	2	

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Comments
Zip Code	93405	1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
<b>11.4.1 Mapped acceleration parameters</b>			Figures 22-1 to 22-14
mapped MCE spectral response, short period	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1 D
<b>11.4.2 Site Class</b>			
<b>11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters</b>			
Site coefficient, short period	Fa	1.000	Table 11.4-1
Site coefficient, 1 second	Fv	1.500	Table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.333	Sec 11.4, Fv*S1
<b>11.4.4 Design Spectral Acceleration Parameters</b>			
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor		D unknown
13.1.4 Exemptions		Ip 1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements		
13.2	Description	Symbol/Value/Comment
13.2.1 Applicable Requirements for Architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3,13.4,13.6
13.2.2 Special Certification Requirements	N/A	
13.2.3 Consequential Damage		cannot cause failure of other essential architectural, electrical for mechanical components
13.2.4 Flexibility		Flexibility as well as strength must be considered
13.2.5 Testing Alternative		components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7 Construction Documents		

13.3 Seismic Demands on Nonstructural Components		
13.3.1 Seismic Design Force	F <sub>p</sub>	F <sub>p</sub> =(0.4*ap*SDS*W <sub>p</sub> )/(R <sub>p</sub> /I <sub>p</sub> )*(1+2z/h)/1.4 F <sub>p</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	F <sub>p</sub> [lbs]	F <sub>p</sub> =701
	F <sub>pmax</sub> [lbs]	3270
	F <sub>pmin</sub> [lbs]	613
spectral acceleration, short period [g]	SDS	1.011
component amplification factor (table 13.6-1)	ap	1.00
Component Importance Factor	I <sub>p</sub>	1.00
Operating Weight (total load of array) [lbs]	W <sub>p</sub>	2022
Response modification Factor (table 13.5-1 or 13.6-1)	R <sub>p</sub>	2.50
point of component attachment [ft]	z	25
average roof height [ft]	h	25
concurrent vertical load [lb]	F <sub>V</sub>	=(2*SDS*W <sub>p</sub> )/1.4 292
vertical resisting load	g <sub>DL</sub>	0.9*N <sub>p</sub> 320
13.3.2 Seismic Relative Displacements		

13.4 Nonstructural Component Anchorage	Components shall be bolted, welded or otherwise fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3-1 except that modifications to F <sub>p</sub> and Rp due to anchorage conditions need not be considered
13.4.1 Design Forces	The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3-1 and 13.3-2
roof attach lateral strength	628 [lbs]
roof attach vertical strength	808 [lbs]
Seismic Lateral Design Force, F <sub>p</sub>	701 [lbs]
Seismic Vertical Design Force, F <sub>V</sub>	292 [lbs]
total roof attachments req for lateral	2
total roof attachments req for vertical	2
	60% of the vertical resisting load (0.6*W <sub>p</sub> ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.

Array Informations			
qty	item	weight	total
36	Modules + Deflectors	54.22	1952
65	Ballast CMU Block	13.4	871.0
43	North Support	19.44	835.9
11	South Support	12.75	140.3
0	Middle Support	0	0.0
	% of Mechanical Attachments to Supports Ratio	6%	
	area, SQFT	999	
	total weight, LBS	3799	
	total load, PSF	3.8	
	total mech attach	3	

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4 , =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.555	Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor		D unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
13.2	Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports			Table 13-2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements	N/A		
13.2.3 Consequential Damage			cannot cause failure of other essential architectural, electrical for mechanical components
13.2.4 Flexibility			Flexibility as well as strength must be considered
13.2.5 Testing Alternative			Components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data			An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13-2-1
13.2.7 Construction Documents			

Seismic Demands on Nonstructural Components			
13.3	Description	Symbol	Value/Comment
13.3.1 Seismic Design Force			$F_p = (0.4 * a_p * SDS * W_p) / (R_p / I_p) * (1+2z/h) / 1.4$ Fp values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		Fph	1316
		Fpmax	6143
		Fpmin	1152
	spectral acceleration, short period [g]	SDS	1.01.1
	component amplification factor (table 13-6-1)	ap	1.00
	Component Importance Factor	I_p	1.00
	Operating Weight (total load of array) [lbs]	W_p	3799
	Response modification Factor (table 13-5-1 or 13-6-1)	R_p	2.50
	point of component attachment [ft]	z	2.55
	average roof height [ft]	h	25
	concurrent vertical load [lb]	F_v	$(2.5 * SDS * W_p) / 1.4$
			559
	vertical resisting load	9*D_L	$0.9 * W_p$
			3419
13.3.2 Seismic Relative Displacements			
13.4 Nonstructural Component Anchorage			Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13-3-1 except that modifications to Fp and Rp due to anchorage conditions need not be considered
13.4.1 Design Forces			The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13-3-1 and 13-3-2
	roof attach lateral strength	628 [lbs]	
	roof attach vertical strength	808 [lbs]	
	Seismic Lateral Design Force, Fp	1316 [lbs]	
	Seismic Vertical Design Force, Fv	549 [lbs]	
	total roof attachments req for lateral	3	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.
	total roof attachments req for vertical	‡	

Array Informations			
qty	item	weight	total
15	Modules + Deflectors	54.22	813
34	Ballast CMU Block	13.4	455.6
20	North Support	19.44	388.8
5	South Support	12.75	63.8
0	Middle Support	0.0	
	% of Mechanical Attachments to Supports Ratio	4%	
	area, SQFT	429	
	total weight, LBS	1721	
	total load, PSF	4.0	
	total mech attach	1	

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
	Ss	1.516	Figures 22-1 to 22-14
	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
	D		
11.4.2 Site Class			
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
	Fa	1.000	table 11.4-1
	Fv	1.500	table 11.4-2
	Sms	1.916	Sec11.4,-Fa*Ss
	Sm1	0.833	Sec11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
	Short Periods	Sds 1.011	11.4.3, 2/3*Sms
	1 second period	SD1 0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ib	do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
13.2	Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports			Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements			N/A
13.2.3 Consequential Damage			cannot cause failure of other essential architectural, electrical for mechanical components
13.2.4 Flexibility			Flexibility as well as strength must be considered
13.2.5 Testing Alternative			components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data			An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7 Construction Documents			
13.3 Seismic Demands on Nonstructural Components			
13.3.1 Seismic Design Force			$F_p = (0.4 * a_p * SDS * W_p) / (R_p / I_p) * (1 + 2z/h) / 1.4$ Fp values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	[lbs]	Fph	597
		Fpmax	2784
		Fpmin	522
spectral acceleration, short period [g]		SDS	1.011
component amplification factor (Table 13.6-1)		ap	1.00
Component Importance Factor		Io	1.00
Operating Weight (total load of array) [lbs]		Wp	1721
Response modification Factor (Table 13.5-1 or 13.6-1)		Rp	2.50
point of component attachment [ft]		z	25
average roof height [ft]		h	25
concurrent vertical load [lb]		Fv	$(2 * SDS * W_p) / 1.4$
		Dv	269
vertical resisting load		Wp	$0.9 * W_p$
		Wp	1549
13.3.2 Seismic Relative Displacements			
13.4 Nonstructural Component Anchorage			Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to Fp and Rp due to anchorage conditions need not be considered
13.4.1 Design Forces			The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
	roof attach lateral strength		628 [lbs]
	roof attach vertical strength		808 [lbs]
	Seismic Lateral Design Force, Fp		597 [lbs]
	Seismic Vertical Design Force, Fv		249 [lbs]
	total roof attachments req for lateral		1
	total roof attachments req for vertical		4
			60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.

Array Informations			
city	item	weight	total
8 Modules + Deflectors		54,222	134
22 Ballast CMU Block		13.4	294.8
10 North Support		19.44	194.4
5 South Support		12.75	63.8
0 Middle Support		0.0	0.0
% of Mechanical Attachments to Supports Ratio		7%	
area_SQFT		233	
total weight_LBS		987	
total load_PSF		4.2	
total mech attach		1	

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Comments
	Zip Code	93405 1550 MADONNARD RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design Category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20-3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4.1
Site coefficient, 1 second	Fv	1.500	table 11.4.2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.533	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters	Output Values		
Short Periods	Sds	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor		Unknown
13.1.4 Exemptions		1p 1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
13.2	Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for Architectural, Mechanical and Electrical Components and Supports			Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements	N/A		
13.2.3 Consequential Damage			cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4 Flexibility			Flexibility as well as strength must be considered
13.2.5 Testing Alternative			components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data			An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7 Construction Documents			
13.3 Seismic Demands on Nonstructural Components			
13.3.1 Seismic Design Force		F <sub>p</sub>	F <sub>p</sub> = [(0.4 * a <sub>p</sub> * S <sub>D</sub> * W <sub>P</sub> ) / (R <sub>D</sub> / I <sub>D</sub> ) * (1 + 2z/h)] / 1.4 F <sub>p</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	[lbs]	F <sub>p</sub> h 342	
		F <sub>pmax</sub> 1596	
		F <sub>pmin</sub> 299	
spectral acceleration, short period [g]		S <sub>D</sub> 1.01.1	
component amplification factor (Table 13.6-1)		a <sub>p</sub> 1.00	
Component Importance Factor		I <sub>P</sub> 1.00	
Operating Weight (total load of array) [lbs]		W <sub>P</sub> 987	
Response modification Factor (Table 13.5-1 or 13.6-1)		R <sub>P</sub> 2.50	
point of component attachment [ft]		z 25	Only ratio z/h is used, which is 1.0
average roof height [ft]		h 25	Only ratio z/h is used, which is 1.0
concurrent vertical load [lb]		F <sub>V</sub> = (2 * S <sub>D</sub> * W <sub>P</sub> ) / 1.4	F <sub>V</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		112	
vertical resisting load		9 * D <sub>L</sub>	0.9 * W <sub>P</sub>
		888	
13.3.2 Seismic Relative Displacements			
13.4 Nonstructural Component Anchorage			Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to F <sub>P</sub> and R <sub>P</sub> due to anchorage conditions need not be considered
13.4.1 Design Forces			The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
	roof attach lateral strength	628 [lbs]	
	roof attach vertical strength	808 [lbs]	
	Seismic Lateral Design Force, F <sub>P</sub>	342 [lbs]	
	Seismic Vertical Design Force, F <sub>V</sub>	142 [lbs]	
total roof attachments req for lateral		1	60% of the vertical resisting load (0.6 * W <sub>P</sub> ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.
		‡	

Array Informations		
qty	item	weight
8	Modules + Deflectors	54.22 434
22	Ballast CMU Block	13.4 294.8
10	North Support	19.44 194.4
5	South Support	12.75 63.8
0	Middle Support	0 0.0
	% of Mechanical Attachments to Supports Ratio	7%
areas, SQFT		233
total weight, LBS		987
total load, PSF		4.2
total mech attach		1

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	Table 11.4-1
Site coefficient, 1 second	Fv	1.500	Table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.333	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters	Output Values		
Short Periods	Sds	10.11	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

## General Design Requirements

13.2	Description	Symbol	Value/Comment
13.2.1	Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2	Special Certification Requirements		N/A
13.2.3	Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4	Flexibility		Flexibility as well as strength must be considered
13.2.5	Testing Alternative		components tested to ICC-ES AC 156 are acceptable
13.2.6	Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7	Construction Documents		

## 13.3 Seismic Demands on Nonstructural Components

13.3.1	Seismic Design Force		$F_p = [(0.4 * a_p * SDS * W_p) / (R_p / I_p)] * [1 + 2z/h] / 1.4$
		[lbs]	$F_p = 342$
			$F_{ph} = 342$
			$F_{pmax} = 15.96$
			$F_{pmin} = 2.99$
	spectral acceleration, short period [g]		SDS 1.011
	component amplification factor (table 13.6-1)		ap 1.00
	Component Importance Factor		Ip 1.00
	Operating Weight (total load of array) [lbs]		Wp 987
	Response modification Factor (table 13.5-1 or 13.6-1)		Rp 2.50
	point of component attachment [ft]		z 25
	average roof height [ft]		h 25
	concurrent vertical load [lb]		$F_v = (2 * SDS * W_p) / 1.4$
			142
	vertical resisting load		$0.9 * W_p$
			888
13.3.2	Seismic Relative Displacements		1

13.4	Nonstructural Component Anchorage		Components shall be bolted, welded or otherwise positively fastened without consideration for frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to $F_p$ and $R_p$ due to anchorage conditions need not be considered
13.4.1	Design Forces		The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
	root attach lateral strength		628 [lbs]
	root attach vertical strength		808 [lbs]
	Seismic Lateral Design Force, $F_p$		342 [lbs]
	Seismic Vertical Design Force, $F_v$		142 [lbs]
	total roof attachments req for lateral		1
	total roof attachments req for vertical		# 60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.

Array Informations			
qty	item	weight	total
20	Modules + Deflectors	54.22	1084
46	Ballast CMU Block	13.4	616.4
24	North Support	19.44	466.5
9	South Support	12.75	114.8
0	Middle Support	0.0	0.0
	% of Mechanical Attachments to Supports Ratio	6%	
	area, SQFT	565	
	total weight, LBS	2282	
	total load, PSF	4.0	
	total mech attach	2	

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

11.4 Seismic Ground Motion Values			
Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short period	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	Table 11.4-1
Site coefficient, 1 second	Fv	1.500	Table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.533	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	1.01	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

13.1 Seismic Design Requirements for Nonstructural components			
Description	Symbol	Value/Comment	
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions	
13.1.3 Component Importance Factor	D	Unknown	13.1.3 Does not meet conditions requiring a 1.5 importance factor
13.1.4 Exemptions	Ib	1.00 do not meet any exemptions	
13.1.5 Applicability of Nonstructural Component Requirements			the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents			12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design			

General Design Requirements			
13.2	Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports			Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements			N/A
13.2.3 Consequential Damage			cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4 Flexibility			Flexibility as well as strength must be considered
13.2.5 Testing Alternative			components tested to ICC-ES AC156 are acceptable
13.2.6 Use of Experience Data			An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7 Construction Documents			
13.3 Seismic Demands on Nonstructural Components			
13.3.1 Seismic Design Force			$F_p = [(0.4 * a_p * SDS * W_p) / (R_p / I_p)] * [1 + 2z/h] / h / 1.4$
		$F_p$ [lbs]	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		$F_{ph}$ 751	
		$F_{pmax}$ 3690	
		$F_{pmin}$ 692	
	spectral acceleration, short period [g]	SDS 1.011	
	component amplification factor (table 13.6-1)	ap 1.00	
	Component Importance Factor	Ip 1.00	
	Operating Weight (total load of array) [lbs]	Wp 2282	
	Response modification Factor (table 13.5-1 or 13.6-1)	Rq 2.50	Only ratio z/h is used, which is 1.0
	point of component attachment [ft]	z 25	Only ratio z/h is used, which is 1.0
	average roof height [ft]	h 25	
	concurrent vertical load [lb]	$F_v = 1.2 * SDS * W_p / 1.4$	$F_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		329	
	vertical resisting load	$S_{VDL}$	$0.9 * V_p$
		2054	
13.3.2 Seismic Relative Displacements			
Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to $F_p$ and $R_p$ due to anchorage conditions need not be considered			
13.4 Nonstructural Component Anchorage			The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
13.4.1 Design Forces			
	roof attach lateral strength	628 [lbs]	
	roof attach vertical strength	808 [lbs]	
	Seismic Lateral Design Force, $F_p$	791 [lbs]	
	Seismic Vertical Design Force, $F_v$	329 [lbs]	
	total roof attachments req for lateral	2	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.
	total roof attachments req for vertical	#	

Array Informations			
array	item	weight	total
14	Modules + Deflectors	54.22	759
31	Ballast CMU Block	13.4	415.4
18	North Support	19.44	349.9
5	South Support	12.75	63.8
0	Middle Support	0	0.0
	% of Mechanical Attachments to Supports Ratio	4%	
	area, SQFT	3.98	
	total weight, LBS	1588	
	total load, PSF	4.0	
	total mech attach	1	

ASCE 7-05 Seismic Worksheet for Non-Structural Members

**11.4 Seismic Ground Motion Values**

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
		Ss 1.5116	Figures 22-1 to 22-14
		S1 0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1 D
11.4.2 Site Class			
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
	Fa	1.000	Table 11.4-1
	Fv	1.500	Table 11.4-2
	Sms	1.5116	Sec 11.4, =Fa*Ss
	Sm1	0.5553	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters	Output Values		
	Sds	1.011	11.4.3, 2/3*Sms
	SD1	0.5555	11.4.4, 2/3*Sm1
	1 second period		

**13.1 Seismic Design Requirements for Nonstructural components**

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
13.2	Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports			Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements			N/A
13.2.3 Consequential Damage			cannot cause failure of other essential architectural, electrical for mechanical components
13.2.4 Flexibility			Flexibility as well as strength must be considered
13.2.5 Testing Alternative			components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data			An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7 Construction Documents			
13.3 Seismic Demands on Nonstructural Components			
13.3.1 Seismic Design Force			$F_p = [(0.4 * a_p * SDS^2 * W_p) / (R_p / I_p)]^{*} [1 + 2z/h] / 1.4$
	[lbs]	$F_{ph}$	550
		$F_{pm}$	2568
		$F_{pmin}$	482
		SDS	1.011
	spectral acceleration, short period [g]	a <sub>p</sub>	1.00
	component amplification factor (table 13.6-1)	I <sub>p</sub>	1.00
	Component Importance Factor	I <sub>p</sub>	1.00
	Operating Weight (total load of array) [lbs]	W <sub>p</sub>	1588
	Response modification Factor (table 13.5-1 or 13.6-1)	R <sub>p</sub>	2.50
	point of component attachment [ft]	z	2.25
	average roof height [ft]	h	2.25
	concurrent vertical load [lb]	F <sub>v</sub>	$(2 * SDS^2 * W_p) / 1.4$
			229
	vertical resisting load	$g^2 D_L$	$0.9 * W_p$
			1429
13.3.2 Seismic Relative Displacements			1
Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to F <sub>p</sub> and R <sub>p</sub> due to anchorage conditions need not be considered			
13.4 Nonstructural Component Anchorage			The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
13.4.1 Design Forces			
	roof attach lateral strength	623	[lbs]
	roof attach vertical strength	808	[lbs]
	Seismic Lateral Design Force, F <sub>p</sub>	550	[lbs]
	Seismic Vertical Design Force, F <sub>v</sub>	229	[lbs]
	total roof attachments req for lateral	1	
	total roof attachments req for vertical	#	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.

Array Informations		
qty	item	weight
32	Modules + Deflectors	54.22 / 1735
49	Ballast CMU Block	13.4 / 656.6
36	North Support	19.44 / 699.8
11	South Support	12.75 / 140.3
0	Middle Support	0 / 0.0
	% of Mechanical Attachments to Supports Ratio	4%
area, SQFT		879
total weight, LBS		3232
total load, PSF		3.7
total mech attach		2

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short period	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	Table 11.4-1
Site coefficient, 1 second	Fv	1.500	Table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	S0s	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor		D, unknown
13.1.4 Exemptions		1p 1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

## General Design Requirements

General Design Requirements			
13.2	Description	Symbol	Value/Comment
13.2.1	Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2	Special Certification Requirements		N/A
13.2.3	Consequential Damage		cannot cause failure of other essential architectural, electrical for mechanical components
13.2.4	Flexibility		Flexibility as well as strength must be considered
13.2.5	Testing Alternative		components tested to ICC-ES AC 156 are acceptable
13.2.6	Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7	Construction Documents		

## 13.3 Seismic Demands on Nonstructural Components

13.3.1 Seismic Design Force			
		F <sub>p</sub>	F <sub>p</sub> =[(0.4* <i>a<sub>p</sub>*SDS**W<sub>p</sub>)/(R<sub>p</sub>/I<sub>p</sub>)<sup>2</sup>](1+22/h)]/1.4</i>
	[lbs]	F <sub>p</sub> h	1120
		F <sub>pmax</sub>	5226
		F <sub>pmin</sub>	980
		SDS	1.011
	spectral acceleration, short period [g]		
	component amplification factor (table 13.6-1)		
	Component Importance Factor	I <sub>p</sub>	1.00
	Operating Weight (total load of array) [lbs]	W <sub>p</sub>	3232
	Response modification Factor (table 13.5-1 or 13.6-1)	R <sub>p</sub>	2.50
	point of component attachment [ft]	z	25
	average roof height [ft]	h	25
	concurrent vertical load [lb]	F <sub>v</sub>	=(2*SDS**W <sub>p</sub> )/1.4
			167
	vertical resisting load	9*I <sub>p</sub> L	0.9*I <sub>p</sub> W <sub>p</sub>
			2909
13.3.2 Seismic Relative Displacements			

Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to F <sub>p</sub> and Rp due to anchorage conditions need not be considered			
13.4	Nonstructural Component Anchorage		The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
13.4.1	Design Forces		
	roof attach lateral strength	628 [lbs]	
	roof attach vertical strength	808 [lbs]	
	Seismic Lateral Design Force, F <sub>p</sub>	1120 [lbs]	
	Seismic Vertical Design Force, F <sub>v</sub>	467 [lbs]	
	total roof attachments req for lateral	2	60% of the vertical resisting load (0.6*W <sub>p</sub> ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.
	total roof attachments req for vertical	4	

Array Informations			
qty	item	weight	total
14	Modules + Deflectors	54.22	759
30	Ballast CMU Block	13.4	402.0
18	North Support	19.44	349.9
5	South Support	12.75	63.8
0	Middle Support	0	0.0
	% of Mechanical Attachments to Supports Ratio	4%	
	area, SQFT	398	
	total weight, LBS	1575	
	total load, PSF	4.0	
	total mech attach	1	

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	Table 11.4-1
Site coefficient, 1 second	Fv	1.500	Table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters	Output Values		
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	I	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
13.2	Description	Symbol/Value/Comment	
13.2.1 Applicable Requirements for Architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections 13.2, 13.3, 13.4, 13.5	
13.2.2 Special Certification Requirements		N/A	
13.2.3 Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components	
13.2.4 Flexibility		Flexibility as well as strength must be considered	
13.2.5 Testing Alternative		components tested to ICC-ES AC 156 are acceptable	
13.2.6 Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by table 13.2-1	
13.2.7 Construction Documents			
Seismic Demands on Nonstructural Components			
13.3			
13.3.1 Seismic Design Force		$F_p = (0.4 * a_p * SDS^{**}W_p) / (R_p / I_p)^{*} [1 + 2z/h] / h / 1.4$	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	[lbs]	$F_p = 546$	
		$F_p = 2546$	
		$F_p = 477$	
		$F_p = 1.011$	
		$a_p = 1.00$	
		$SDS = 1.011$	
		$R_p = 1.00$	
		$I_p = 1.00$	
		$W_p = 1575$	
		$z = 2.50$	Only ratio $z/h$ is used, which is 1.0
		$h = 2.5$	Only ratio $z/h$ is used, which is 1.0
		$F_v = (2 * SDS^{**}W_p) / 1.4$	$F_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		$F_v = 227$	
		$S_d = 0.9 * W_p$	
		$S_d = 1417$	
13.3.2 Seismic Relative Displacements			
13.4	Nonstructural Component Anchorage		Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to $F_p$ and $R_p$ due to anchorage conditions need not be considered
13.4.1 Design Forces			The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
	roof attach lateral strength	628 [lbs]	
	roof attach vertical strength	808 [lbs]	
	Seismic Lateral Design Force, $F_p$	546 [lbs]	
	Seismic Vertical Design Force, $F_v$	227 [lbs]	
	total roof attachments req for lateral	1	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.
	total roof attachments req for vertical	4	

Array Informations		
qty	item	weight
7	Modules + Deflectors	54.22
22	Ballast CMU Block	380 13.4 294.8
10	North Support	19.44 194.4
4	South Support	12.75 51.0
0	Middle Support	0 0.0
	% of Mechanical Attachments to Supports Ratio	7%
	area, SQFT	210
	total weight, LBS	920
	total load, PSF	4.4
	total mech attach	1

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4 .=Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.533	Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters	Output Values		
Short Periods	Sps	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any/ exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

## General Design Requirements

13.2	Description	Symbol	Value/Comment
13.2.1	Applicable Requirements for Architectural, Mechanical and Electrical Components and Supports		Table 13-2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.5
13.2.2	Special Certification Requirements		N/A
13.2.3	Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4	Flexibility		Flexibility as well as strength must be considered
13.2.5	Testing Alternative		components tested to ICC-ES AC 156 are acceptable
13.2.6	Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13-2-1
13.2.7	Construction Documents		

## 13.3 Seismic Demands on Nonstructural Components

13.3.1	Seismic Design Force		
		$F_p = (0.4 * a_p * SDS * W_p) / (R_p / p) * (1 + 2z/h) / 1.4$	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		Fph 319 [lbs]	
		Fpmx 1487	
		Fpmin 279	
	spectral acceleration, short period [g]	SDS 1.011	
	component amplification factor: (table 13-6-1)	ap 1.00	
	Component Importance Factor	Ip 1.00	
	Operating Weight (total load of array) [lbs]	Wp 920	
	Response modification Factor (table 13-5-1 or 13-6-1)	Rp 2.50	1
	point of component attachment [ft]	z 25	Only ratio z/h is used, which is 1.0
	average roof height [ft]	h 25	Only ratio z/h is used, which is 1.0
	concurrent vertical load [lb]	$F_v = (2 * SDS * W_p) / 1.4$	$F_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		133	
	vertical resisting load	950	0.9**Wp
		38	
13.3.2	Seismic Relative Displacements		

13.4	Nonstructural Component Anchorage		Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to Fp and Rp due to anchorage conditions need not be considered
13.4.1	Design Forces		The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
	roof attach lateral strength	628 [lbs]	
	roof attach vertical strength	808 [lbs]	
	Seismic Lateral Design Force, Fq	319 [lbs]	
	Seismic Vertical Design Force, Fv	133 [lbs]	
	total roof attachments req for lateral	1	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.
	total roof attachments req for vertical	1	

Array Informations		
qty	Item	weight
7	Modules + Deflectors	54.22
22	Ballast CMU Block	380 13.4 294.8
10	North Support	19.44 194.4
4	South Support	12.75 51.0
0	Middle Support	0 0.0
	% of Mechanical Attachments to Supports Ratio	7%
	area, SQFT	209
	total weight, LBS	920
	total load, PSF	4.4
	total mech attach	1

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

11.4 Seismic Ground Motion Values		
Description	Symbol/Input Values	Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA
11.4.1 Mapped acceleration parameters		If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
mapped MCE spectral response, short periods	Ss 1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1 0.555	Figures 22-1 to 22-14
11.4.2 Site Class	D	A, B, C, D, E or F. D is default if site soil properties unknown - See table table 20.3.1
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters		
Site coefficient, short period	Fa 1.000	table 11.4-1
Site coefficient, 1 second	Fv 1.500	table 11.4-2
mapped MCE spectral response at short period	Sms 1.516	Sec 11.4 , =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1 0.833	Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters	Output Values	
Short Periods	Sds 1.011	11.4.3, 2/3*Sms
1 second period	SD1 0.555	11.4.4, 2/3*Sm1
13.1 Seismic Design Requirements for Nonstructural components	Symbol	Value/Comment
Description		Same as parent structure is site soil conditions
13.1.2 Seismic Design Category	D	Unknown
13.1.3 Component Importance Factor	Ip 1.00	13.1.3 Does not meet conditions requiring a 1.5 importance factor
13.1.4 Exemptions	do not meet any exemptions	
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight W
13.1.6 Reference Documents		
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
13.2	Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports			Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements			N/A
13.2.3 Consequential Damage			cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4 Flexibility			Flexibility as well as strength must be considered
13.2.5 Testing Alternative			components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data			An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7 Construction Documents			
13.3 Seismic Demands on Nonstructural Components			
13.3.1 Seismic Design Force		$F_p = (0.4 * a_p * SDS^5 * W_p) / (R_p / I_p) * (1 + 2z/h) / 7.4$	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	[lbs]	F <sub>oh</sub> 319	
		F <sub>pmax</sub> 1487	
		F <sub>min</sub> 279	
spectral acceleration, short period [g]		SDS 1.011	
component amplification factor (Table 13.6-1)		ap 1.00	
Component Importance Factor		I <sub>p</sub> 1.00	
Operating Weight (total load of array) [lbs]		W <sub>p</sub> 920	
Response modification Factor (Table 13.5-1 or 13.6-1)		R <sub>p</sub> 2.50	Only ratio z/h is used, which is 1.0
point of component attachment [ft]		z 25	Only ratio z/h is used, which is 1.0
average roof height [ft]		h 25	
concurrent vertical load [lb]		$F_v = (2 * SDS^5 * W_p) / 14$	$F_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		133	
vertical resisting load		9*D <sub>L</sub>	0.9*W <sub>p</sub>
		888	
13.3.2 Seismic Relative Displacements			
13.4 Nonstructural Component Anchorage			Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to F <sub>p</sub> and R <sub>p</sub> due to anchorage conditions need not be considered
13.4.1 Design Forces			The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
	roof attach lateral strength	628 [lbs]	
	roof attach vertical strength	808 [lbs]	
	Seismic Lateral Design Force, F <sub>p</sub>	319 [lbs]	
	Seismic Vertical Design Force, F <sub>v</sub>	133 [lbs]	
	total roof attachments req for lateral	1	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof
	total roof attachments req for vertical	4	attachments are required for the vertical forces.

Array Informations		
qty	item	weight
15	Modules + Deflectors	54.22
34	Ballast CMU Block	13.4
20	North Support	19.44
5	South Support	12.75
0	Middle Support	0.00
	% of Mechanical Attachments to Supports Ratio	4%
	area, SQFT	429
	total weight, LBS	1721
	total load, PSF	4.0
	total mech attach	1

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Comments
Zip Code	93405	1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDS	1.031	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a <i>nonbuilding structure</i> as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements					
13.2	Description	Symbol	Value/Comment		
13.2.1	Applicable Requirements for Architectural, Mechanical and Electrical Components and Supports			Table 13-2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.5	
13.2.2	Special Certification Requirements		N/A		
13.2.3	Consequential Damage			cannot cause failure of other essential architectural, electrical or mechanical components	
13.2.4	Flexibility			Flexibility as well as strength must be considered	
13.2.5	Testing Alternative			components tested to ICC-ES AC 156 are acceptable	
13.2.6	Use of Experience Data			An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13-2-1	
13.2.7	Construction Documents				
13.3 Seismic Demands on Nonstructural Components					
13.3.1	Seismic Design Force			$F_p = (0.4 * a_p * SDS * W_p) / (R_p / p) * (1 + z/h) / 1.4$	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		[lbs]	$F_{ph}$	597	
			$F_{pmax}$	2784	
			$F_{pmin}$	522	
			$SDS$	1.011	
			$a_p$	1.00	
			$p$	1.00	
			$R_p$	1721	
			$W_p$		
			$R_p$	2.50	
			$z/h$	2.25	Only ratio $z/h$ is used, which is 1.0
			$h$	25	Only ratio $z/h$ is used, which is 1.0
			$F_v$	$(2 * SDS * W_p) / 1.4$	$F_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
				329	
				9.91	0.9 * $W_p$
				5.49	
13.3.2	Seismic Relative Displacements				
13.4	Nonstructural Component Anchorage			Components shall be bolted, welded or otherwise fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to $F_p$ and $R_p$ due to anchorage conditions need not be considered	
13.4.1	Design Forces			The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2	
		roof attach lateral strength	628 [lbs]		
		roof attach vertical strength	808 [lbs]		
		Seismic Lateral Design Force, $F_p$	597 [lbs]		
		Seismic Vertical Design Force, $F_v$	249 [lbs]		
		total roof attachments req for lateral	1	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof	
		total roof attachments req for vertical	‡	‡ attachments are required for the vertical forces.	

Array Informations			
try	item	weight	total
15	Modules + Deflectors	54.22	813
34	Ballast CMU Block	13.4	455.6
20	North Support	19.44	383.8
5	South Support	12.75	63.8
0	Middle Support	0.0	0.0
	% of Mechanical Attachments to Supports Ratio	4%	
	area, SQFT	429	
	total weight, LBS	1721	
	total load, PSF	4.0	
	total mech attach	1	

**ASCE 7-05 Seismic Worksheet for Non-Structural Members****11.4 Seismic Ground Motion Values**

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A Only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1 D
11.4.2 Site Class			
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.333	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	Sds	1.001	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

**13.1 Seismic Design Requirements for Nonstructural components**

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	I0,100	do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a <i>nonbuilding structure</i> as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		



Array Informations		
qty	item	weight
13	Modules + Deflectors	54.22
26	Ballast CMU Block	13.4
16	North Support	19.44
6	South Support	12.75
0	Middle Support	0.0
	% of Mechanical Attachments to Supports Ratio	5%
	area, SQFT	370
	total weight, LBS	1441
	total load, PSF	3.9
	total mech attach	1

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405   1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short period	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4 , =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.555	Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	0.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements		
13.2	Description	Symbol/Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements	N/A	
13.2.3 Consequential Damage		cannot cause failure of other essential architectural/ electrical for mechanical components
13.2.4 Flexibility		Flexibility as well as strength must be considered
13.2.5 Testing Alternative		components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data		- An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7 Construction Documents		
13.3 Seismic Demands on Nonstructural Components		
13.3.1 Seismic Design Force		$F_p = [(0.4 * a_p * SDS * W_p) / (R_p / I_p)] * (1 + 2z/h) / 1.4$ Fp values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC [lbs] Fph 499
		Fpmax 2330
		Fpmin 437
		SDS 1.011
		a_p 1.00
		I_p 1.00
		Wp 1441
		Rp 2.50
		Only ratio z/h is used, which is 1.0
		Only ratio z/h is used, which is 1.0
		f_v = (2 * SDS * W_p) / 1.4 f_v values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC 203
		0.9 * W_p
		vertical resisting load 0.9 * DL 1297
13.3.2 Seismic Relative Displacements		
13.4 Nonstructural Component Anchorage		Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to Fp and Rp due to anchorage conditions need not be considered
13.4.1 Design Forces		The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
		rooftop lateral strength 628 [lbs]
		rooftop vertical strength 808 [lbs]
		Seismic Lateral Design Force, F_p 499 [lbs]
		Seismic Vertical Design Force, F_v 208 [lbs]
		total rooftop attachments req for lateral 1
		60% of the vertical resisting load (0.6 * W_p) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces. 4

Array Informations		
qry	item	weight
17 Modules + Deflectors		54.22
30 Ballast CMU Block		922
21 North Support		13.4
19.44	408.2	
6 South Support		12.75
76.5		
0 Middle Support		0.0
% of Mechanical Attachments to Supports Ratio		4%
area, SQFT		478
tora weight, LBS		1868
tora load, PSF		3.8
tora mech attach		1

**ASCE 7-05 Seismic Worksheet for Non-Structural Members****11.4 Seismic Ground Motion Values**

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405-1150 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4 , =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sml

**13.1 Seismic Design Requirements for Nonstructural components**

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00
		do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
Description	Symbol	Value/Comment	
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6	
13.2.2 Special Certification Requirements		N/A	
13.2.3 Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components	
13.2.4 Flexibility		Flexibility as well as strength must be considered	
13.2.5 Testing Alternative		components tested to ICC-ES AC 156 are acceptable	
13.2.6 Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by table 13.2-1.	
13.2.7 Construction Documents			
13.3 Seismic Demands on Nonstructural Components			
13.3.1 Seismic Design Force		$F_p = (0.4 * a_p * SDS * W_p) / (F_p / p) * (1 + z/h) / 1.4$	F <sub>p</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	[lbs]	F <sub>p</sub> ph 627	
		F <sub>pmax</sub> 2324	
		F <sub>pmin</sub> 548	
spectral acceleration, short period [g]	SDS	1.011	
component amplification factor (table 13.6-1)	a <sub>p</sub>	1.00	
Component Importance Factor	I <sub>p</sub>	1.00	
Operating Weight (total load of array) [lbs]	W <sub>p</sub>	1808	
Response modification Factor (table 13.5-1 or 13.6-1)	R <sub>p</sub>	2.50	
point of component attachment [ft]	z	25	Only ratio z/h is used, which is 1.0
average roof height [ft]	h	25	Only ratio z/h is used, which is 1.0
concurrent vertical load [lb]	F <sub>v</sub>	(2 * SDS * W <sub>p</sub> ) / 1.4	F <sub>v</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		261	
vertical resisting load	G <sub>D</sub>	0.9 * W <sub>p</sub>	
		1628	
13.3.2 Seismic Relative Displacements			
Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3-1 except that modifications to F <sub>p</sub> and R <sub>p</sub> due to anchorage conditions need not be considered			
13.4 Nonstructural Component Anchorage		The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2	
13.4.1 Design Forces			
roof attach lateral strength	F <sub>p</sub>	628 [lbs]	
roof attach vertical strength	F <sub>v</sub>	808 [lbs]	
Seismic Lateral Design Force, F <sub>p</sub>	F <sub>p</sub>	627 [lbs]	
Seismic Vertical Design Force, F <sub>v</sub>	F <sub>v</sub>	261 [lbs]	
total roof attachments req for lateral		1	60% of the vertical resisting load (0.6 * W <sub>p</sub> ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.
total roof attachments req for vertical		4	

Array Informations			
qty	item	weight	total
12	Modules + Deflectors	54.22	631
29	Balast CMU Block	13.4	388.6
16	North Support	19.44	311.0
5	South Support	12.75	63.8
0	Middle Support	0.00	
	% of Mechanical Attachments to Supports Ratio	5%	
area, SQFT		348	
total weight, LBS		1414	
total load, PSF		4.1	
total mech attach		1	

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

##### 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters	Output Values		
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

##### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
13.2 .	Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for Architectural, Mechanical and Electrical Components and Supports			Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements			N/A
13.2.3 Consequential Damage			cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4 Flexibility			Flexibility as well as strength must be considered
13.2.5 Testing Alternative			components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data			An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by table 13.2-1.
13.2.7 Construction Documents			
13.3 Seismic Demands on Nonstructural Components			
13.3.1 Seismic Design Force			$F_p = (0.4 * a_p * SDS * W_p) / (R_p / p) * (1 + 2z/h) / 1.4$ Fp values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		Fph [lbs]	Fph 390
		Fpmx [lbs]	Fpmx 12287
		Fpmin [lbs]	Fpmin 429
	spectral acceleration, short period [g]	SDS	1.011
	component amplification factor (table 13.6-1)	aP	1.00
	Component Importance Factor	I	1.00
	Operating Weight (total load of array) [lbs]	Wp	1414
	Response modification Factor (table 13.5-1 or 13.6-1)	Rp	2.50
	point of component attachment [ft]	z	2.5
	average roof height [ft]	h	25
	concurrent vertical load [lb]	Fv	$N = (1.2 * SDS * W_p) / 1.4$ Fv values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		204	
	vertical resisting load	Sv DL	$0.9 * W_p$
		273	
13.3.2 Seismic Relative Displacements			1
Components shall be bolted, welded or otherwise fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to Fp and Rp due to anchorage conditions need not be considered			
13.4 Nonstructural Component Anchorage			The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
13.4.1 Design Forces			
	roof attach lateral strength	628 [lbs]	
	roof attach vertical strength	808 [lbs]	
	Seismic Lateral Design Force, Fp	490 [lbs]	
	Seismic Vertical Design Force, Fv	204 [lbs]	
	total roof attachments req for lateral	1	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.
	total roof attachments req for vertical	1	

Array Informations		
qty	item	weight
14	Modules + Deflectors	54.22
30	Ballast CMU Block	75.9
18	North Support	13.4
		402.0
5	South Support	19.44
		349.9
5	Middle Support	12.75
		63.8
0	Middle Support	0
	% of Mechanical Attachments to Supports Ratio	0.0
	area, SQFT	3.98
	total weight, LBS	1575
	total load, PSF	4.0
	total mech attach	1

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
		Ss 1.516	Figures 22-1 to 22-14
		S1 0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
		Fa 1.000	table 11.4-1
		Fv 1.500	table 11.4-2
		Sms 1.516	Sec 11.4 , =Fa*Ss
		Sm1 0.833	Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters		Output Values	
		SDs 1.011	11.4.3, 2/3*Sms
		SD1 0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor		Unknown
13.1.4 Exemptions		1p 1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
	Description	Symbol	Value/Comment
13.2.1	Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.5
13.2.2	Special Certification Requirements		N/A
13.2.3	Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4	Flexibility		Flexibility as well as strength must be considered
13.2.5	Testing Alternative		components tested to ICC-ES AC 156 are acceptable
13.2.6	Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by table 13.2-1
13.2.7	Construction Documents		
Seismic Demands on Nonstructural Components			
13.3.1	Seismic Design Force		$F_p = (0.4 * a_p * SDS * W_p) / (R_p / I_p) * (1 + z/h) / 1.4$ F <sub>p</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		[lbs]	F <sub>p</sub> 546
			F <sub>ph</sub> 2346
			F <sub>pmax</sub> 2346
			F <sub>pmin</sub> 477
	spectral acceleration, short period [g]	SDS	1.011
	component amplification factor (table 13.6-1)	a <sub>p</sub>	1.00
	Component Importance Factor	I <sub>p</sub>	1.00
	Operating Weight (total load of array) [lbs]	W <sub>p</sub>	1575
	Response modification Factor (table 13.5-1 or 13.6-1)	R <sub>p</sub>	2.50
	Point of component attachment [ft]	z	2.25
	average roof height [ft]	h	25
	concurrent vertical load [lb]	F <sub>v</sub>	$(2 * SDS * W_p) / 1.4$
			227
	vertical resisting load	G * D <sub>L</sub>	$0.9 * W_p$
			147
13.3.2	Seismic Relative Displacements		
13.4	Nonstructural Component Anchorage		Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to F <sub>p</sub> and R <sub>p</sub> due to anchorage conditions need not be considered
13.4.1	Design Forces		The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
	roof attach lateral strength	628	[lbs]
	roof attach vertical strength	808	[lbs]
	Seismic Lateral Design Force, F <sub>p</sub>	546	[lbs]
	Seismic Vertical Design Force, F <sub>v</sub>	227	[lbs]
	total roof attachments req for lateral	1	
			60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical forces. Therefore, no roof attachments are required for the vertical forces.
			#

Array Informations			
city	item	weight	total
11 Modules + Deflectors		54.22	596
32 Ballast CMU Block		13.4	423.8
15 North Support		19.44	291.6
5 South Support		12.75	63.8
0 Middle Support		0.0	0.0
% of Mechanical Attachments to Supports Ratio		5%	
area, SQFT		321	
total weight, LBS		1381	
total load, PSF		4.3	
total mech attach		1	

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Comments
Zip Code	93405	1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1 D
11.4.2 Site Class			
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.883	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a <i>nonbuilding structure</i> as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
13.2	Description	Symbol	Value/Comment
13.2.1	Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2	Special Certification Requirements		N/A
13.2.3	Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4	Flexibility		Flexibility as well as strength must be considered
13.2.5	Testing Alternative		components tested to ICC-ES AC 156 are acceptable
13.2.6	Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7	Construction Documents		
13.3 Seismic Demands on Nonstructural Components			
13.3.1	Seismic Design Force		$F_p = [(0.4 * \rho * SDS * W_p) / (R_p / I_p)]^{(1+z/h)} / 1.4$
		[lbs]	$F_p = [478 / 1.4]^{(1+z/h)} / 1.4$
			Fph 478
			Fpmax 2232
			Fpmin 41.9
	spectral acceleration, short period [g]	SDS	1.011
	component amplification factor (table 13.6-1)	ap	1.00
	Component Importance Factor	Ip	1.00
	Operating Weight (total load of array) [lbs]	Wp	1181
	Response modification Factor (table 13.5-1 or 13.6-1)	Rp	2.50
	point of component attachment [ft]	z	25
	average roof height [ft]	h	25
	concurrent vertical load [lb]	Fv	$=(2 * SDS * W_p) / 1.4$
			199
	vertical resisting load	S*DL	0.9 * Wp
			1243
13.3.2	Seismic Relative Displacements		
Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to Fp and Rp due to anchorage conditions need not be considered			
13.4	Nonstructural Component Anchorage		The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
13.4.1	Design Forces		
	roof attach lateral strength	628 [lbs]	
	roof attach vertical strength	808 [lbs]	
	Seismic Lateral Design Force, Fp	478 [lbs]	
	Seismic Vertical Design Force, Fv	199 [lbs]	
	total roof attachments req for lateral	1	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.
	total roof attachments req for vertical	#	

Array Informations		
city	item	weight
31	Modules + Deflectors	54.22
69	Ballast CMU Block	13.4
43	North Support	19.44
7	South Support	12.75
0	Middle Support	0.0
	% of Mechanical Attachments to Supports Ratio	4%
area SQFT		887
total weight, LBS		3331
total load, PSF		4.0
total mech attach		2

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405	1550 MADONNA RD, SAN LUIS OBISPO, CA If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			table 11.4-1
Site coefficient, short period	Fa	1.000	table 11.4-2
Site coefficient, 1 second	Fv	1.500	Sec 11.4, =Fa*Ss
mapped MCE spectral response at short period	Sms	1.516	
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters	Output Values		
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	13.1.3 Does not meet conditions requiring a 1.5 importance factor
13.1.4 Exemptions	Ip,1.00	do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight W
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

## General Design Requirements

13.2	Description	Symbol	Value/Comment
13.2.1	Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2	Special Certification Requirements		N/A
13.2.3	Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4	Flexibility		Flexibility as well as strength must be considered components tested to ICC-ES AC 156 are acceptable
13.2.5	Testing Alternative		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by table 13.2-1
13.2.6	Use of Experience Data		
13.2.7	Construction Documents		

## 13.3 Seismic Demands on Nonstructural Components

13.3.1	Seismic Design Force		$F_p = [(0.4 * a_p * SDS^*W_p) / (F_p / p)] * (1 + z/h) / 1.4$
		[lbs]	$F_p = 3223$
			$F_p = 5709$
			$F_p = 1070$
			$SDS = 1.011$
			spectral acceleration, short period [g]
			$a_p = 1.00$
			component amplification factor (table 13.6-1)
	Component Importance Factor	10	1.00
	Operating Weight (total load of array) [lbs]	W_p	3531
	Response modification Factor (table 13.5-1 or 13.6-1)	R_p	2.50
	point of component attachment [ft]	z	25
	average roof height [ft]	h	25
	concurrent vertical load [lb]	F_v	$F_v = (2 * SDS^*W_p) / 1.4$
			$F_v = 500$
			$0.9 * W_p$
			$0.9 * 3531$
			$3178$
	13.3.2 Seismic Relative Displacements		

13.4	Nonstructural Component Anchorage		Components shall be bolted, welded or otherwise fastened without consideration for frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to F_p and R_p due to anchorage conditions need not be considered
			The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
13.4.1	Design Forces		
	roof attach lateral strength	628	[lbs]
	roof attach vertical strength	808	[lbs]
	Seismic Lateral Design Force, F_p	1223	[lbs]
	Seismic Vertical Design Force, F_v	510	[lbs]
	total roof attachments req for lateral	2	
	total roof attachments req for vertical	4	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.

Array Informations			
Qty	Item	Weight	Total
14	Modules + Deflectors	54.22	759
33	Ballast CMU Block	13.4	442.2
19	North Support	19.44	359.4
5	South Support	12.75	63.8
0	Middle Support	0.00	0.00
% of Mechanical Attachments to Supports Ratio		4%	
area, SQFT		404	
total weight, LBS		1634	
total load, PSF		4.0	
total mech attach		1	

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

##### 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
Zip Code	93405	1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A, only applies
Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4 .=Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4 . Fv*S1
11.4.4 Design Spectral Acceleration Parameters	Output Values		
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

##### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category	D	Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	Ip	1.00
13.1.4 Exemptions		do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
13.2	Description	Symbol /Value/Comment	
13.2.1	Applicable Requirements for architectural, Mechanical and Electrical Components and Supports	Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6	
13.2.2	Special Certification Requirements	N/A	
13.2.3	Consequential Damage	cannot cause failure of other essential architectural, electrical for mechanical components	
13.2.4	Flexibility	Flexibility as well as strength must be considered	
13.2.5	Testing Alternative	components tested to ICC-ES AC156 are acceptable	
13.2.6	Use of Experience Data	An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1	
13.2.7	Construction Documents		
13.3 Seismic Demands on Nonstructural Components			
13.3.1	Seismic Design Force	$F_p = [(0.4 * \alpha_p * SDS * W_p) / (F_p / D)] * [1 + z/h] / 1.4$	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		[lbs]	
		$F_p = 566$	
		$F_{pmax} = 2643$	
		$F_{pmin} = 486$	
		$SDS = 1.011$	
		$\alpha_p = 1.00$	
		$Spectral acceleration, short period [g]$	
		$Component amplification factor (table 13.6-1)$	
		$\alpha_p = 1.00$	
		$Component Importance Factor$	
		$I_p = 1.00$	
		$Operating Weight (total load of array) [lbs]$	
		$W_p = 1534$	
		$Response modification Factor (table 13.5-1 or 13.6-1)$	
		$R_p = 2.50$	
		$Point of component attachment [ft]$	
		$z = 25$	Only ratio $z/h$ is used, which is 1.0
		$average roof height [ft]$	Only ratio $z/h$ is used, which is 1.0
		$h = 25$	
		$concurrent vertical load [lb]$	$F_v = (2 * SDS * W_p) / 1.4$ $F_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		$W_p = 266$	
		$Vertical resisting load$	$0.9 * W_p$
		$9.1 CL$	
		$1471$	
		$13.3.2 Seismic Relative Displacements$	
13.4	Nonstructural Component Anchorage		Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to $F_p$ and $R_p$ due to anchorage conditions need not be considered
			The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
13.4.1	Design Forces		
		roof attach lateral strength	628 [lbs]
		roof attach vertical strength	808 [lbs]
		Seismic Lateral Design Force, $F_p$	566 [lbs]
		Seismic Vertical Design Force, $F_v$	236 [lbs]
		total roof attachments req for lateral	1
		total roof attachments req for vertical	‡ 60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.

Array Informations		
qty	item	weight
7	Modules + Deflectors	54.22
22	Ballast CMU Block	380
		13.4
11	North Support	294.8
		19.44
3	South Support	213.8
		12.75
0	Middle Support	38.3
		0.0
	% of Mechanical Attachments to Supports Ratio	0.0
	area, SQFT	7%
	total weight, LBS	212
	total load, PSF	926
	total mech attach	4.4
		1

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

##### 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Comments
	Zip Code	93405	1550 MADONNA RD, SAN LUIS OBISPO, CA
11.4.1 Mapped acceleration parameters			If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
			Figures 22-1 to 22-14
			Figures 22-1 to 22-14
			A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4. =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	1.031	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

##### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor		D unknown
13.1.4 Exemptions		do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a <i>nonbuilding structure</i> as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
13.2	Description	Symbol/Value/Comment	
13.2.1 Applicable Requirements for Architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6	
13.2.2 Special Certification Requirements	N/A		
13.2.3 Consequential Damage		cannot cause failure of other essential architectural, electrical for mechanical components	
13.2.4 Flexibility		Flexibility as well as strength must be considered	
13.2.5 Testing Alternative		components tested to ICC-ES AC 156 are acceptable	
13.2.6 Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by table 13.2-1	
13.2.7 Construction Documents			
Seismic Demands on Nonstructural Components			
13.3.1 Seismic Design Force		$F_p = (0.4 * \alpha * SDS * W_p) / (R_p / p) * (1 + z/h) / 1.4$	Fp values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	[lbs]	Fph 321	
		Fpmx 1498	
		Fpmin 231	
spectra acceleration, short period [g]	SDS	1.011	
component amplification factor (table 13.6-1)	ap	1.00	
Component Importance Factor	Ip	1.00	
Operating Weight (total load of array) [lbs]	Wp	926	
Response modification Factor (table 13.5-1 or 13.6-1)	Rp	2.50	Only ratio z/h is used, which is 1.0
point of component attachment [ft]	z	2.25	Only ratio z/h is used, which is 1.0
average roof height [ft]	h	2.5	
concurrent vertical load [lb]	Fv	$(2 * SDS * W_p) / 1.4$	Fv values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		134	
		3*D1	0.9*Wp
		334	
13.3.2 Seismic Relative Displacements			
13.4 Nonstructural Component Anchorage		Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to Fp and Rp due to anchorage conditions need not be considered	The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
13.4.1 Design Forces			
	roof attach lateral strength	628 [lbs]	
	roof attach vertical strength	808 [lbs]	
	Seismic Lateral Design Force, Fp	321 [lbs]	
	Seismic Vertical Design Force, Fv	134 [lbs]	
	total roof attachments req for lateral	1	60% of the vertical resisting load (0.6*Wp) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.
	total roof attachments req for vertical	4	

Array Informations		
qty	item	weight
13	Modules + Deflectors	54.22
30	Ballast CMU Block	13.4
17	North Support	19.44
5	South Support	12.75
0	Middle Support	0.0
	% of Mechanical Attachments to Supports Ratio	5%
	area, SQFT	372
	total weight, LBS	1501
	total load, PSF	4.0
	total mech attach	1

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F. D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.533	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Design Requirements for Nonstructural Components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
13.2	Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports			Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3,13.4,13.6
13.2.2 Special Certification Requirements			N/A
13.2.3 Consequential Damage			cannot cause failure of other essential architectural, electrical for mechanical components
13.2.4 Flexibility			Flexibility as well as strength must be considered
13.2.5 Testing Alternative			Components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data			An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7 Construction Documents			
13.3 Seismic Demands on Nonstructural Components			
13.3.1 Seismic Design Force		F <sub>p</sub>	$F_p = [(0.4 * a_p * SDS * W_p) / (R_p / I_p)] * [1 + 2z/h] / 1.4$ F <sub>p</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	[lbs]	F <sub>p</sub> 520	
		F <sub>pmax</sub> 2427	
		F <sub>pmin</sub> 455	
		SDS 1.011	spectral acceleration, short period [g]
		a <sub>p</sub> 1.00	component amplification factor (table 13.6-1)
		I <sub>p</sub> 1.00	Component Importance Factor
		W <sub>0</sub> 1501	Operating Weight (total load of array) [lbs]
		R <sub>p</sub> 2.50	Response modification Factor (table 13.5-1 or 13.6-1)
		z 25	point of component attachment [ft]
		h 25	average roof height [ft]
		F <sub>V</sub> = (2 * SDS * W <sub>p</sub> ) / 1.4	concurrent vertical load [lb]
		217	
		9*D <sub>L</sub>	vertical resisting load
		1351	
13.3.2 Seismic Relative Displacements			
Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to F <sub>p</sub> and R <sub>p</sub> due to anchorage conditions need not be considered			
13.4 Nonstructural Component Anchorage		T	The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
13.4.1 Design Forces			
	roof attach lateral strength	628 [lbs]	
	roof attach vertical strength	808 [lbs]	
	Seismic Lateral Design Force, F <sub>p</sub>	520 [lbs]	
	Seismic Vertical Design Force, F <sub>V</sub>	217 [lbs]	
	total roof attachments req for lateral	1	
	total roof attachments req for vertical	‡	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.

Array Informations			
qty	item	weight	total
13	Modules + Deflectors	54.22	705
30	Ballast CMU Block	13.4	402.0
17	North Support	19.44	330.5
5	South Support	12.75	63.8
0	Middle Support	0.0	
	% of Mechanical Attachments to Supports Ratio	5%	
	area, SQFT	372	
	total weight, LBS	1501	
	total load, PSF	4.0	
	total mech attach	1	

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

##### 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters	Ss	1.5156	Figures 22-1 to 22-14
	mapped MCE spectral response, short periods	S1 0.555	Figures 22-1 to 22-14
	mapped MCE spectral response, 1 second	D	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class			
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
	Fa	1.000	Table 11.4-1
	Fv	1.500	Table 11.4-2
	Sms	1.5156	Sec 11.4, =Fa*Ss
	Sm1	0.5553	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters	Output Values		
	SDS	1.051	11.4.3, 2/3*Sms
	SD1	0.5555	11.4.4, 2/3*Sm1

##### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a <i>nonbuilding structure</i> as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
13.2	Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports			Table 13.2-1 states that mechanical and electrical supports must meet sections 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements			N/A
13.2.3 Consequential Damage			cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4 Flexibility			Flexibility as well as strength must be considered
13.2.5 Testing Alternative			Components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data			An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7 Construction Documents			
13.3 Seismic Demands on Nonstructural Components			
13.3.1 Seismic Design Force		$F_p = [(0.4 * a_0 * SDS * W_p) / (R_p / I_p)] * [1 + 2z/h] / 1.4$	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	[lbs]	$F_{ph} = 520$	
		$F_{pmax} = 2427$	
		$F_{pmin} = 455$	
spectral acceleration, short period [g]		SDS 1.011	
component amplification factor (table 13.6-1)		ap 1.00	
Component Importance Factor		$I_p = 1.00$	
Operating Weight (total load of array) [lbs]		$W_p = 1501$	
Response modification Factor (table 13.5-1 or 13.6-1)		$R_p = 2.50$	Only ratio $z/h$ is used, which is 1.0
point of component attachment [ft]		$z = 25$	Only ratio $z/h$ is used, which is 1.0
average roof height [ft]		$h = 25$	
concurrent vertical load [lb]		$F_v = 1.2 * SDS * W_p / 1.4$	$F_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		217	
vertical resisting load		$2.9 * DL$	
		351	
0.9%Wp			
13.3.2 Seismic Relative Displacements			
13.4 Nonstructural Component Anchorage			Components shall be bolted, welded or otherwise positively fastened without consideration for frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to $F_p$ and $R_p$ due to anchorage conditions need not be considered
13.4.1 Design Forces			The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
	roof attach lateral strength	628 [lbs]	
	roof attach vertical strength	808 [lbs]	
	Seismic Lateral Design Force, $F_p$	520 [lbs]	
	Seismic Vertical Design Force, $F_v$	217 [lbs]	
	total roof attachments req for lateral	1	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof
	total roof attachments req for vertical	‡	attachments are required for the vertical forces.

Array Informations			
qty	item	weight	total
13	Modules + Deflectors	54.22	705
30	Ballast CMU Block	13.4	402.0
17	North Support	19.44	330.5
5	South Support	12.75	63.8
0	Middle Support	0.00	
	% of Mechanical Attachments to Supports Ratio	5%	
	area, SQFT	372	
	total weight, LBS	1501	
	total load, PSF	4.0	
	total mech attach	1	

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code:	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fg	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fg*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	10.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor		D unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a <i>nonbuilding structure</i> as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
13.2	Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for Architectural, Mechanical and Electrical Components and Supports			Table 13-2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements		N/A	
13.2.3 Consequential Damage			cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4 Flexibility			Flexibility as well as strength must be considered
13.2.5 Testing Alternative			components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data			An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13-2-1
13.2.7 Construction Documents			
13.3 Seismic Demands on Nonstructural Components			
13.3.1 Seismic Design Force		F <sub>p</sub>	F <sub>p</sub> = [(0.4 * F <sub>p</sub> * SDS * W <sub>p</sub> ) / (R <sub>p</sub> /  F <sub>v</sub>  )] * (1 + z <sub>z</sub> / h) / 1.4 F <sub>p</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	[lbs]	F <sub>p</sub> 520	
		F <sub>pmax</sub> 2427	
		F <sub>pmin</sub> 455	
		SDS 1.011	
		ap 1.00	
	Component Importance Factor	P  1.00	
	Operating Weight (total load of array) [lbs]	W <sub>p</sub> 1501	
	Response modification Factor (table 13-5-1 or 13-6-1)	R <sub>p</sub> 2.50	
	point of component attachment [ft]	z 25	Only ratio z/h is used, which is 1.0
	average roof height [ft]	h 25	Only ratio z/h is used, which is 1.0
	concurrent vertical load [lb]	F <sub>v</sub> F <sub>v</sub> = [(2 * SDS * W <sub>p</sub> ) / 1.4]	F <sub>v</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		217	
	vertical resisting load	F <sub>v</sub>   217	
		0.9 * W <sub>p</sub>	
		1351	
13.3.2 Seismic Relative Displacements			
Components shall be bolted, welded or otherwise fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to F <sub>p</sub> and R <sub>p</sub> due to anchorage conditions need not be considered			
13.4 Nonstructural Component Anchorage			The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
13.4.1 Design Forces			
	roof attach lateral strength	628 [lbs]	
	roof attach vertical strength	808 [lbs]	
	Seismic Lateral Design Force, F <sub>p</sub>	520 [lbs]	
	Seismic Vertical Design Force, F <sub>v</sub>	217 [lbs]	
	total roof attachments req for lateral	1	60% of the vertical resisting load (0.6 * W <sub>p</sub> ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.
	total roof attachments req for vertical	‡	

Array Informations		
qty	item	weight
13	Modules + Deflectors	54.22
30	Ballast CMU Block	70.5 13.4 40.0
17	North Support	19.44
5	South Support	330.5 12.75 63.8
0	Middle Support	0.0
	% of Mechanical Attachments to Supports Ratio	5%
	area, SQFT	372
	total weight, LBS	1501
	total load, PSF	4.0
	total mech attach	1

**ASCE 7-05 Seismic Worksheet for Non-Structural Members****11.4 Seismic Ground Motion Values**

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 150 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11-4-1
Site coefficient, 1 second	Fv	1.500	table 11-4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4 , =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.533	Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters	Output Values		
Short Periods	SDs	1.011	11.4.3 , 2/3*Sms
1 second period	SD1	0.555	11.4.4 , 2/3*Sm1

**13.1 Seismic Design Requirements for Nonstructural components**

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	I	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

## General Design Requirements

<b>General Design Requirements</b>			
13.2	Description	Symbol	Value/Comment
13.2.1	Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2	Special Certification Requirements		N/A
13.2.3	Consequential Damage		cannot cause failure of other essential architectural, electrical for mechanical components
13.2.4	Flexibility		Flexibility as well as strength must be considered
13.2.5	Testing Alternative		components tested to ICC-ES AC 156 are acceptable
13.2.6	Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7	Construction Documents		

## 13.3 Seismic Demands on Nonstructural Components

13.3.1 Seismic Design Force			
		F <sub>P</sub>	F <sub>P</sub> =((0.4*F <sub>P</sub> *SDS*W <sub>P</sub> )/(R <sub>P</sub> /I <sub>P</sub> ))^(1+2z/h)/1.4 F <sub>P</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	I <sub>P</sub> [lbs]	F <sub>P</sub> 500	
		F <sub>Pmax</sub> 2427	
		F <sub>Pmin</sub> 455	
	spectral acceleration, short period [g]	SDS 1.011	
	component amplification factor (table 13.6-1)	ap 1.00	
	Component Importance Factor	Ip 1.00	
	Operating Weight (total load of array) [lbs]	W <sub>P</sub> 1501	
	Response modification Factor (table 13.5-1 or 13.6-1)	R <sub>P</sub> 2.50	Only ratio z/h is used, which is 1.0
	point of component attachment [ft]	z 25	Only ratio z/h is used, which is 1.0
	average roof height [ft]	h 25	Only ratio z/h is used, which is 1.0
	concurrent vertical load [lb]	F <sub>V</sub> = ((2*SDS*W <sub>P</sub> )/1.4) 217	F <sub>V</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	vertical resisting load	0.9*D <sub>L</sub> 1331	0.9*W <sub>P</sub>
13.3.2 Seismic Relative Displacements			
13.4 Nonstructural Component Anchorage			
13.4.1	Design Forces		The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
	roof attach lateral strength	628 [lbs]	
	roof attach vertical strength	808 [lbs]	
	Seismic Lateral Design Force, F <sub>P</sub>	520 [lbs]	
	Seismic Vertical Design Force, F <sub>V</sub>	217 [lbs]	
	total roof attachments req for lateral	1	60% of the vertical resisting load (0.6*W <sub>P</sub> ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.
	total roof attachments req for vertical	1	2 attachments are required for the vertical forces.

Array Informations			
qty	item	weight	total
17	Modules + Deflectors	54.22	54.22
37	Ballast CMU Block	13.4	495.8
22	North Support	19.44	427.7
7	South Support	12.75	89.3
0	Middle Support	0	0.0
	% of Mechanical Attachments to Supports Ratio	7%	
	area, SQFT	488	
	total weight, LBS	1934	
	total load, PSF	4.0	
	total mech attach	2	

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

##### 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
Zip Code	93405	1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to .015 Then Seismic Design category A only applies
Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
D			
11.4.2 Site Class			
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.5016	Sec 11.4 , =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.8333	Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.5555	11.4.4, 2/3*Sm1

##### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
Description	Symbol	Value/Comment	
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports Special Certification Requirements		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6 N/A	
13.2.3 Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components	
13.2.4 Flexibility		Flexibility as well as strength must be considered Components tested to ICC-ES AC 156 are acceptable	
13.2.5 Testing Alternative		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by table 13.2-1	
13.2.6 Use of Experience Data			
13.2.7 Construction Documents			
13.3 Seismic Demands on Nonstructural Components			
13.3.1 Seismic Design Force		$F_p = (0.4 * 30 * SDS * W_p) / (R_p / (I_p)) * (1 + 2z/h) / 1.4$	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	[lbs]	$F_{ph} = 670$	
		$F_{pmax} = 3128$	
		$F_{pmin} = 587$	
spectral acceleration, short period [g]	SDS	1.011	
component amplification factor (table 13.6-1)	ap	1.00	
Component Importance Factor	I_p	1.00	
Operating Weight (total load of array) [lbs]	W_p	1934	
Response modification Factor (table 13.5-1 or 13.6-1)	R_p	2.50	1 Only ratio $z/h$ is used, which is 1.0
point of component attachment [ft]	z	2.25	Only ratio $z/h$ is used, which is 1.0
average roof height [ft]	h	2.25	
concurrent vertical load [lb]	F_v	$= 1.2 * SDS * W_p / 1.4$	$F_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		279	
		0.9 * W_p	
		254.1	
13.3.2 Seismic Relative Displacements			
Components shall be bolted, welded or otherwise positively fastened without consideration for frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to $F_p$ and $R_p$ due to anchorage conditions need not be considered			
13.4 Nonstructural Component Anchorage		The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2	
13.4.1 Design Forces			
	roof attach lateral strength	628 [lbs]	
	roof attach vertical strength	808 [lbs]	
	Seismic Lateral Design Force, F_p	670 [lbs]	
	Seismic Vertical Design Force, F_v	279 [lbs]	
	total roof attachments req for lateral	2	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof
	total roof attachments req for vertical	4	# attachments are required for the vertical forces.

Array Informations		
qty	Item	weight
17	Modules + Deflectors	54.22
36	Ballast CMU Block	922 13.4 482.4
22	North Support	19.44
6	South Support	427.7
6	Middle Support	12.75
0	% of Mechanical Attachments to Supports Ratio	7.0
	area, SQFT	484
	total weight, LBS	1908
	total load, PSF	3.9
	total mech attach	2

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
Zip Code	93405	1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
Site Class	D		
Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sns	1.516	Sec 11.4. =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.8333	Sec 11.4. , Fv*S1
Design Spectral Acceleration Parameters	Output Values		
Short Periods	SDs	1.011	11.4.3. 2/3*Sms
1 second period	SD1	0.555	11.4.4. 2/3*Sml

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor		D unknown
13.1.4 Exemptions		1p1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a <i>nonbuilding structure</i> as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

## General Design Requirements

13.2	Description	Symbol	Value/Comment
13.2.1	Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2	Special Certification Requirements		N/A
13.2.3	Consequential Damage		cannot cause failure of other essential architectural, electrical, or mechanical components
13.2.4	Flexibility		Flexibility as well as strength must be considered
13.2.5	Testing Alternative		components tested to ICC-ES AC 156 are acceptable
13.2.6	Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7	Construction Documents		

## 13.3 Seismic Demands on Nonstructural Components

13.3.1	Seismic Design Force		$F_p = [(0.4 * a_p * S_D * "W_p) / (R_p / b)]^{(z+2z/h)/1.4}$	F <sub>p</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		$F_{bh}$	861 [lbs]	
		$F_{pmax}$	3086	
		$F_{pmin}$	579	
	spectral acceleration, short period [g]	$S_D$	1.011	
	component amplification factor (Table 13.6-1)	$a_p$	1.00	
	Component Importance Factor	$I_p$	1.00	
	Operating Weight (total load of array) [lbs]	$W_p$	1908	
	Response modification Factor (table 13.3.1 or 13.6-1)	$R_p$	2.50	
	point of component attachment [ft]	$z$	25	Only ratio z/h is used, which is 1.0
	average roof height [ft]	$h$	25	Only ratio z/h is used, which is 1.0
	concurrent vertical load [lb]	$F_V$	$(2 * S_D * "W_p) / 1.4$	F <sub>V</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
			276	
			$9 * R_p$	
	vertical resisting load	$9 * R_p$	9 * R <sub>p</sub>	
			117	
	13.3.2 Seismic Relative Displacements			

13.4	Nonstructural Component Anchorage		Components shall be bolted, welded or otherwise positively fastened without consideration for frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to F <sub>p</sub> and R <sub>p</sub> due to anchorage conditions need not be considered
13.4.1	Design Forces		The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
	roof attach lateral strength		628 [lbs]
	roof attach vertical strength		808 [lbs]
	Seismic Lateral Design Force, F <sub>p</sub>		661 [lbs]
	Seismic Vertical Design Force, F <sub>v</sub>		276 [lbs]
	total roof attachments req for lateral		2
	total roof attachments req for vertical		4
			60% of the vertical resisting load (0.6 * W <sub>p</sub> ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.

Array Informations		
qty	item	weight
14	Modules + Deflectors	54.22
30	Ballast CMU Block	759
		13.4
18	North Support	402.0
		19.44
5	South Support	349.9
		12.75
0	Middle Support	63.8
		0.0
	% of Mechanical Attachments to Supports Ratio	4%
	area, SQFT	398
	total weight, LBS	1575
	total load, PSF	4.0
	total mech attach	1

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405-1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4 , =Fa*Ss
mapped MCE spectral response at 1 second period	Sml	0.833	Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters	Output Values		
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sml

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a <i>nonbuilding structure</i> as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

13.2 General Design Requirements	
Description	Symbol Value/Comment
13.2.1 Applicable Requirements for Architectural, Mechanical and Electrical Components and Supports	Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6 N/A
13.2.2 Special Certification Requirements	
13.2.3 Consequential Damage	cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4 Flexibility	Flexibility as well as strength must be considered components tested to ICC-ES AC 156 are acceptable
13.2.5 Testing Alternative	
13.2.6 Use of Experience Data	An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7 Construction Documents	
13.3 Seismic Demands on Nonstructural Components	
13.3.1 Seismic Design Force	$F_p = (0.4 * a_p * SDS^{**}W_p) / (R_p/I_p) * [1 + 2z/h] / 1.4$ F <sub>p</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	F <sub>p</sub> [lbs]
	F <sub>pmax</sub> 546
	F <sub>pmin</sub> 2546
spectral acceleration, short period [g]	SDS 1.011
component amplification factor (table 13.6-1)	a <sub>p</sub> 1.00
Component Importance Factor	I <sub>p</sub> 1.00
Operating Weight (total load of array) [lbs]	W <sub>p</sub> 1575
Response modification Factor (table 13.5-1 or 13.6-1) point of component attachment [ft]	R <sub>p</sub> 2.50 z 25 average roof height [ft] h 25 concurrent vertical load [lb] F <sub>v</sub> = (2 * SDS^{**}W <sub>p</sub> ) / 1.4 227 vertical resisting load 0.9%W <sub>p</sub> 417
Only ratio z/h is used, which is 1.0 Only ratio z/h is used, which is 1.0 F <sub>v</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC	
13.3.2 Seismic Relative Displacements	
13.4 Nonstructural Component Anchorage	
13.4.1 Design Forces	The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
roof attach lateral strength	638 [lbs]
roof attach vertical strength	808 [lbs]
Seismic Lateral Design Force, F <sub>p</sub>	546 [lbs]
Seismic Vertical Design Force, F <sub>v</sub>	227 [lbs]
total roof attachments req for lateral	1
total roof attachments req for vertical	‡ 60% of the vertical resisting load (0.6%W <sub>p</sub> ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.

Array Informations			
qty	Item	weight	total
10	Modules + Deflectors	54.22	542
31	Ballast CMU Block	13.4	415.4
14	North Support	19.44	272.2
5	South Support	12.75	63.8
0	Middle Support	0.0	0.0
	% of Mechanical Attachments to Supports Ratio	5%	
	area, SQFT	296	
	total weight, LBS	1294	
	total load, PSF	4.4	
	total mech attach	1	

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

11.4 Seismic Ground Motion Values			
Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1250 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, short periods	S1	0.555	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	D		A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class			
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4. =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4. Fv*S1
11.4.4 Design Spectral Acceleration Parameters	Output Values		
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

13.1 Seismic Design Requirements for Nonstructural components			
Description	Symbol	Value/Comment	
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions	
13.1.3 Component Importance Factor	D	Unknown	13.1.3 Does not meet conditions requiring a 1.5 importance factor
13.1.4 Exemptions	I	1.00	do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements			the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents			12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design			

## General Design Requirements

13.2	Description	Symbol	Value/Comment
13.2.1	Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2	Special Certification Requirements		N/A
13.2.3	Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4	Flexibility		Flexibility as well as strength must be considered
13.2.5	Testing Alternative		components tested to ICC-ES AC 156 are acceptable
13.2.6	Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by table 13.2-1
13.2.7	Construction Documents		

## 13.3 Seismic Demands on Nonstructural Components

13.3.1	Seismic Design Force	F <sub>p</sub>	F <sub>p</sub> =[(0.4"ap*SDS*W <sub>p</sub> )/(R <sub>p</sub> /I <sub>p</sub> )][(1+2z/h)/1.4]	F <sub>p</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	[lbs]	F <sub>ph</sub> 428		
		F <sub>pmax</sub> 2092		
		F <sub>pmin</sub> 392		
	spectral acceleration, short period [g]	SDS 1.011		
	component amplification factor (table 13.6-1)	ap 1.00		
	Component Importance Factor	I <sub>p</sub> 1.00		
	Operating Weight (total load of array) [lbs]	W <sub>p</sub> 1294		
	Response modification Factor (table 13.5-1 or 13.6-1) point of component attachment [ft]	R <sub>p</sub> 2.50		
	average roof height [ft]	z 25		Only ratio z/h is used, which is 1.0
	concurrent vertical load [lb]	h 25		Only ratio z/h is used, which is 1.0
		F <sub>v</sub> = (2*SDS*W <sub>p</sub> )/1.4		F <sub>v</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		1387		
	vertical resisting load	9*D <sub>L</sub>		0.9*W <sub>p</sub>
		1154		
13.3.2	Seismic Relative Displacements			
13.4	Nonstructural Component Anchorage			Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3-1 except that modifications to F <sub>p</sub> and R <sub>p</sub> due to anchorage conditions need not be considered
13.4.1	Design Forces			The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
	root of attach lateral strength	628 [lbs]		
	root of attach vertical strength	808 [lbs]		
	Seismic Lateral Design Force, F <sub>p</sub>	448 [lbs]		
	Seismic Vertical Design Force, F <sub>v</sub>	187 [lbs]		
	total roof attachments req for lateral	1		60% of the vertical resisting load (0.6*W <sub>p</sub> ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.
	total roof attachments req for vertical	‡		

Array Informations		
qty	item	weight
7	Modules + Deflectors	54.22
23	Ballast CMU Block	380
		13.4
10	North Support	19.44
4	South Support	19.44
12.75	Middle Support	51.0
0		0.0
	% of Mechanical Attachments to Supports Ratio	7%
	area, SQFT	221
	total weight, LBS	933
	total load, PSF	4.2
	total mech attach	1

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LOUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3-1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	I <sub>p</sub>	Unknown
13.1.4 Exemptions		do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a <i>nonbuilding structure</i> as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

**General Design Requirements**

<b>13.2</b>	<b>Description</b>	<b>Symbol</b>	<b>Value/Comment</b>
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports			Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements			N/A
13.2.3 Consequential Damage			cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4 Flexibility			Flexibility as well as strength must be considered
13.2.5 Testing Alternative			components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data			An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7 Construction Documents			

**13.3 Seismic Demands on Nonstructural Components**

<b>13.3.1 Seismic Design Force</b>		$F_p = \frac{F_p}{[(0.4 * a_p * SDS * W_p) / (R_p / p)] * [(z + 2z/h) / 1.4]}$	Fp values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
$F_{ph}$	[lbs]	323	
$F_{pmax}$	[lbs]	1509	
$F_{pmin}$	[lbs]	283	
spectral acceleration, short period [g]		SDS 1.011	
component amplification factor (table 13.6-1)		30 1.00	
Component Importance Factor		Ip 1.00	
Operating Weight (total load of array) [lbs]		Wp 933	
Response modification Factor (table 13.5-1 or 13.6-1)		Rp 2.50	1
point of component attachment [ft]		z 25	Only ratio z/h is used, which is 1.0
average roof height [ft]		h 25	Only ratio z/h is used, which is 1.0
concurrent vertical load [lb]		$F_v = (2 * SDS * W_p) / 1.4$	$F_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		315	
vertical resisting load		$0.9 * W_p$	
		310	
<b>13.3.2 Seismic Relative Displacements</b>			
<b>13.4 Nonstructural Component Anchorage</b>			Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to Fp and Rp due to anchorage conditions need not be considered
<b>13.4.1 Design Forces</b>			The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
roof attach lateral strength	[lbs]	628	
roof attach vertical strength	[lbs]	808	
Seismic Lateral Design Force, $F_p$	[lbs]	323	
Seismic Vertical Design Force, $F_v$	[lbs]	135	
total roof attachments req for lateral		1	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.
total roof attachments req for vertical		4	

Array Informations		
city	item	weight
13 Modules + Deflectors		54.22
30 Ballast CMU Block		13.4
17 North Support		402.0
17 North Support		19.44
5 South Support		330.5
0 Middle Support		12.75
0 Middle Support		0.0
% of Mechanical Attachments to Supports Ratio		5%
area, SQFT		372
total weight, LBS		1501
total load, PSF		4.0
total mech attach		1

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

##### 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405, 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to .15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters	Output Values		
Short Periods	Sds	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

##### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor		D unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

**General Design Requirements**

<b>13.2</b>	<b>General Design Requirements</b>		
Description	Symbol	Value/Comment	
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13-2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.5	
13.2.2 Special Certification Requirements	N/A		
13.2.3 Consequential Damage		cannot cause failure of other essential architectural, electrical for mechanical components	
13.2.4 Flexibility		Flexibility as well as strength must be considered components tested to ICC-ES AC 156 are acceptable	
13.2.5 Testing Alternative			
13.2.6 Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13-2-1	
13.2.7 Construction Documents			

**13.3 Seismic Demands on Nonstructural Components**

13.3.1 Seismic Design Force	F <sub>p</sub>	F <sub>p</sub> = $(0.4 * \alpha_p * SDS * W_p) / (R_p / p) * [1 + z/h] / 1.4$	F <sub>p</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	F <sub>p</sub> [lbs]	F <sub>p</sub> F <sub>p0</sub>	
	F <sub>pmax</sub> 2427		
	F <sub>pmin</sub> 455		
spectral acceleration, short period [g]	SDS 1.011		
component amplification factor (table 13-6-1)	ap 1.00		
Component Importance Factor	Ip 1.00		
Operating Weight (total load of array) [lbs]	W <sub>p</sub> 1501		
Response modification Factor (table 13-5-1 or 13-6-1)	R <sub>p</sub> 2.50		
point of component attachment [ft]	z 25		Only ratio z/h is used, which is 1.0
average roof height [ft]	h 25		Only ratio z/h is used, which is 1.0
concurrent vertical load [lb]	f <sub>v</sub> f <sub>v</sub> = $(2 * SDS * W_p) / 1.4$		f <sub>v</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	247		
vertical resisting load	9 * D <sub>L</sub>		0.9 * W <sub>p</sub>
	1351		
13.3.2 Seismic Relative Displacements			

13.4 Nonstructural Component Anchorage		Components shall be bolted, welded or otherwise fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13-3-1 except that modifications to F <sub>p</sub> and R <sub>p</sub> due to anchorage conditions need not be considered
13.4.1 Design Forces		The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13-3-1 and 13-3-2
rof attach lateral strength	628 [lbs]	
rof attach vertical strength	808 [lbs]	
Seismic Lateral Design Force, F <sub>p</sub>	520 [lbs]	
Seismic Vertical Design Force, F <sub>v</sub>	217 [lbs]	
total roof attachments req for lateral	1	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.
total roof attachments req for vertical	‡	

Array Informations		
qty	item	weight
13	Modules + Deflectors	54.22
30	Ballast CMU Block	705
		13.4
17	North Support	402.0
		19.44
5	South Support	330.5
		12.75
0	Middle Support	65.8
		0.0
	% of Mechanical Attachments to Supports Ratio	5%
	area, SQFT	372
	total weight, LBS	1501
	total load, PSF	4.0
	total mech attach	1

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

##### 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectra response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	1.01	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

##### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	Ip	Unknown
13.1.4 Exemptions		Ip 1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
13.2	Description	Symbol	Value/Comment
13.2.1	Applicable Requirements for Architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2	Special Certification Requirements		N/A
13.2.3	Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4	Flexibility		Flexibility as well as strength must be considered
13.2.5	Testing Alternative		Components tested to ICC-ES AC 156 are acceptable
13.2.6	Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by table 13.2-1
13.2.7	Construction Documents		
13.3 Seismic Demands on Nonstructural Components			
13.3.1	Seismic Design Force		$F_p = [(0.4 * a_p * SDS * W_p) / (R_p / I_p)] * [1 + 2z/h] / h / 1.4$
		[lbs]	Fph 520
			Fpmax 2427
			Fpmin 455
	spectral acceleration, short period [g]		SDS 1.011
	component amplification factor (table 13.6-1)	a <sub>p</sub>	1.00
	Component Importance Factor	I <sub>p</sub>	1.00
	Operating Weight (total load of array) [lbs]	W <sub>p</sub>	1501
	Response modification Factor (table 13.5-1 or 13.6-1)	R <sub>p</sub>	2.50
	point of component attachment [ft]	z	25
	average roof height [ft]	h	25
	concurrent vertical load [lb]	F <sub>V</sub>	$(2 * SDS * W_p) / 1.4$
			217
	vertical resisting load	W <sub>DL</sub>	$0.9 * W_p$
			1351
13.3.2	Seismic Relative Displacements		
13.4 Nonstructural Component Anchorage			
13.4.1	Design Forces		Components shall be bolted, welded or otherwise positively fastened without consideration for frictional resistance. The component forces shall be those determined in section 13.3-1 except that modifications to F <sub>p</sub> and R <sub>p</sub> due to anchorage conditions need not be considered
	roof attach lateral strength		The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3-1 and 13.3-2
	roof attach vertical strength		
	Seismic Lateral Design Force, F <sub>p</sub>		
	Seismic Vertical Design Force, F <sub>V</sub>		
	total roof attachments req for lateral		
	total roof attachments req for vertical		
			1. 60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.

Array Informations			
qty	item	weight	total weight
16	Modules + Deflectors	54.22	865
30	Ballast CMU Block	13.4	402.0
20	North Support	19.44	388.8
5	South Support	12.75	63.8
0	Middle Support	0.00	0.0
% of Mechanical Attachments to Supports Ratio		4%	
area, SQFT		448	
total weight, LBS		1722	
total load, PSF		3.8	
total mech attach		1	

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
Zip Code	93405	1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
Mapped acceleration parameters	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, short periods	S1	0.555	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	D		A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
Site Class			
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4 , =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters	Output Values		
Short Periods	Sds	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
Seismic Design Category		Same as parent structure is site soil conditions
Component Importance Factor	I	Unknown
Exemptions	Ip	1.00 do not meet any exemptions
Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
Reference Documents		12.7.2 Definition of effective seismic weight W
Reference Documents using allowable Stress Design		

General Design Requirements			
Description	Symbol	Value/Comment	
13.2.1 Applicable Requirements for Architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6	
13.2.2 Special Certification Requirements		N/A	
13.2.3 Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components	
13.2.4 Flexibility		Flexibility as well as strength must be considered	
13.2.5 Testing Alternative		components tested to ICC-ES AC 156 are acceptable	
13.2.6 Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1	
13.2.7 Construction Documents			
13.3 Seismic Demands on Nonstructural Components			
13.3.1 Seismic Design Force		$F_p = [(0.4 * a_p * SDS^2 * W_p) / (R_p / h)] * [1 + 2z/h] / 1.4$	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	[lbs]	Fph 597	
		Fpmax 2785	
		Fpmin 522	
spectral acceleration, short period [g]	SDS	1.011	
component amplification factor (table 13.6-1)	a <sub>p</sub>	1.00	
Component Importance Factor	I <sub>p</sub>	1.00	
Operating Weight (total load of array) [lbs]	W <sub>p</sub>	1722	
Response modification Factor (table 13.5-1 or 13.6-1)	R <sub>p</sub>	2.50	
point of component attachment [ft]	z	25	Only ratio z/h is used, which is 1.0
average roof height [ft]	h	25	Only ratio z/h is used, which is 1.0
concurrent vertical load [lb]	f <sub>v</sub>	$(.2 * SDS^2 * W_p) / 1.4$	$f_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		249	
		0.97*W <sub>p</sub>	
		550	
13.3.2 Seismic Relative Displacements			
13.4 Nonstructural Component Anchorage		Components shall be bolted, welded or otherwise positively fastened without consideration for frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to F <sub>p</sub> and R <sub>p</sub> due to anchorage conditions need not be considered	
13.4.1 Design Forces		The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2	
	roof attach lateral strength	628 [lbs]	
	roof attach vertical strength	808 [lbs]	
	Seismic Lateral Design Force, F <sub>p</sub>	597 [lbs]	
	Seismic Vertical Design Force, F <sub>v</sub>	249 [lbs]	
	total roof attachments req for lateral	1	
	total roof attachments req for vertical	1	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.
		‡	

Array Informations		
Qty	Item	Weight
12	Modules + Deflectors	54.22
26	Ballast CMU Block	13.4
15	North Support	19.44
5	South Support	12.75
0	Middle Support	0.0
	% of Mechanical Attachments to Supports Ratio	5%
	area, SQFT	340
	total weight, LBS	1354
	total load, PSF	4.0
	total mech attach	1

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
Zip Code:		93405   1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
<b>Mapped acceleration parameters</b>			Figures 22-1 to 22-14
mapped MCE spectral response, short period	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F. D is default if site soil properties unknown - See table table 20.3.1
<b>Site Class</b>	D		
<b>Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters</b>			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4, Fv*S1
<b>Design Spectra Acceleration Parameters</b>			
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
<b>Seismic Design Category</b>		Same as parent structure is site soil conditions
<b>Component Importance Factor</b>		Unknown
<b>Exemptions</b>		Ip 1.00 do not meet any exemptions
<b>Applicability of Nonstructural Component Requirements</b>		the array is not considered a <i>nonbuilding structure</i> as it is not 25% of the building seismic weight
<b>Reference Documents</b>		12.7.2 Definition of effective seismic weight W
<b>Reference Documents using allowable Stress Design</b>		

## General Design Requirements

13.2	Description	Symbol /Value/Comment
13.2.1	Applicable Requirements for Architectural, Mechanical and Electrical Components and Supports	Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2	Special Certification Requirements	N/A
13.2.3	Consequential Damage	cannot cause failure of other essential architectural, electrical for mechanical components
13.2.4	Flexibility	Flexibility as well as strength must be considered
13.2.5	Testing Alternative	components tested to ICC-ES AC 156 are acceptable
13.2.6	Use of Experience Data	An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7	Construction Documents	

## 13.3 Seismic Demands on Nonstructural Components

13.3.1	Seismic Design Force	Equation	Comment
	$F_p = (0.4 * \alpha_p * SDS^2 * W_p) / (R_p / p) * (1 - 2z/h) / 1.4$	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC	
	$F_{ph}$ [lbs]	$F_{ph}$ [lbs]	
	$F_{pmax}$	$F_{pmax}$	
	$F_{pmin}$ 411	$F_{pmin}$ 411	
	$SDS$ 1, 011	$SDS$ 1, 011	
	$\alpha_p$ 1.00	$\alpha_p$ 1.00	
	$R_p$ 1.00	$R_p$ 1.00	
	$W_p$ 1554	$W_p$ 1554	
	$R_p$ 2.50	$R_p$ 2.50	
	$z/h$ 2.25	$z/h$ 2.25	Only ratio $z/h$ is used, which is 1.0
	$R_p$ 1.4	$R_p$ 1.4	Only ratio $z/h$ is used, which is 1.0
	$W_p$ 196	$W_p$ 196	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	vertical resisting load	0.9*Wp	
		1219	
13.3.2	Seismic Relative Displacements		

13.4	Nonstructural Component Anchorage	Comment
13.4.1	Design Forces	The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
	roof attach lateral strength	628 [lbs]
	roof attach vertical strength	808 [lbs]
	Seismic Lateral Design Force, $F_p$	469 [lbs]
	Seismic Vertical Design Force, $F_v$	196 [lbs]
	total roof attachments req for lateral	1
	total roof attachments req for vertical	# 60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.

Array Informations		
qty	item	weight
14	Modules + Deflectors	54.22
25	Ballast CMU Block	75.9
		13.4
18	North Support	335.0
		19.44
5	South Support	349.9
		12.75
0	Middle Support	63.8
		0.0
	% of Mechanical Attachments to Supports Ratio	0.0
	area, SQFT	4%
	total weight, LBS	398
	total load, PSF	1508
	total load, PSF	3.8
	total mech attach	1

## ASCE 7-05 Seismic Worksheet for Non-Structural Members

## 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
Zip Code	93405	1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4 , =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

## 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor		D unknown
13.1.4 Exemptions		Ip 1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
13.2	Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for Architectural, Mechanical and Electrical Components and Supports			Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements			N/A
13.2.3 Consequential Damage			cannot cause failure of other essential architectural, electrical for mechanical components
13.2.4 Flexibility			Flexibility as well as strength must be considered components tested to ICC-ES AC 156 are acceptable
13.2.5 Testing Alternative			
13.2.6 Use of Experience Data			An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13-2-1
13.2.7 Construction Documents			
13.3 Seismic Demands on Nonstructural Components			
13.3.1 Seismic Design Force		F <sub>0</sub>	$F_0 = (0.4 * ap * SDS^2 * W_p) / (R_p / h) * (1 + 2z/h) / 1.4$
	[lbs]	F <sub>ph</sub>	$F_{ph} = F_0 / 522$
		F <sub>pmax</sub>	2438
		F <sub>pmin</sub>	457
spectral acceleration, short period [g]		SDS	1.011
component amplification factor (table 13.6-1)		ap	1.00
Component Importance Factor		R <sub>p</sub>	1.00
Operating Weight (total load of array) [lbs]		W <sub>p</sub>	1508
Response modification Factor (table 13.5-1 or 13.6-1) point of component attachment [ft]		R <sub>p</sub>	2.50
average roof height [ft]		z	25
concurrent vertical load [lb]		h	25
vertical resisting load		F <sub>v</sub>	$F_v = (2 * SDS^2 * W_p) / 1.4$
			118
			0.9W <sub>p</sub>
			357
13.3.2 Seismic Relative Displacements			
Components shall be bolted, welded or otherwise positively fastened without consideration for frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to F <sub>p</sub> and R <sub>p</sub> due to anchorage conditions need not be considered			
The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2			
13.4 Nonstructural Component Anchorage			
13.4.1 Design Forces			
	roof attach lateral strength	628	[lbs]
	roof attach vertical strength	808	[lbs]
	Seismic Lateral Design Force, F <sub>0</sub>	522	[lbs]
	Seismic Vertical Design Force, F <sub>v</sub>	218	[lbs]
	total roof attachments req for lateral	1	
	total roof attachments req for vertical	1	
		#	60% of the vertical resisting load (0.6*W <sub>p</sub> ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.

Array Informations			
Qty	Item	Weight	Total
14	Modules + Deflectors	54.22	759
26	Ballast CMU Block	13.4	348.4
18	North Support	19.44	349.9
5	South Support	12.75	63.8
0	Middle Support	0.00	
% of Mechanical Attachments to Supports Ratio		4%	
area, SQFT		398	
total weight, LBS		1521	
total load, PSF		3.8	
total mech attach		1	

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

##### 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
Zip Code	93405	1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss is less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4. =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4. Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sml1

##### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
13.2	Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports			Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements			N/A
13.2.3 Consequential Damage			cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4 Flexibility			Flexibility as well as strength must be considered
13.2.5 Testing Alternative			Components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data			An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7 Construction Documents			
13.3 Seismic Demands on Nonstructural Components			
13.3.1 Seismic Design Force			
		F <sub>p</sub>	$F_p = [(0.4 * a_p * SDS^2 * W_p) / (R_p / p)]^{(1+2z/h)/1.4}$
	F <sub>ph</sub>	[lbs]	F <sub>ph</sub> shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	527		
	F <sub>pmx</sub>	[lbs]	
	2460		
	F <sub>pmin</sub>	[lbs]	
	1461		
	SDS	[g]	
	1.011		
	spectral acceleration, short period [g]		
	ap	[1.00]	
	component amplification factor (table 13.6-1)	[p]	
	Component Importance Factor	[p]	
	Operating Weight (total load of array) [lbs]	W <sub>p</sub>	
	Response modification Factor (table 13.5-1 or 13.6-1)	R <sub>p</sub>	2.50
	point of component attachment [ft]	z	25
	average roof height [ft]	h	25
	concurrent vertical load [lb]	F <sub>v</sub>	$(2 * SDS^2 * W_p) / 1.4$
			230
	vertical resisting load	D <sub>L</sub>	0.9 * W <sub>p</sub>
			1369
13.3.2 Seismic Relative Displacements			
			Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3-1 except that modifications to F <sub>p</sub> and R <sub>p</sub> due to anchorage conditions need not be considered
13.4	Nonstructural Component Anchorage		The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
13.4.1 Design Forces			
	roof attach lateral strength	[lbs]	628
	roof attach vertical strength	[lbs]	808
	Seismic Lateral Design Force, F <sub>p</sub>	[lbs]	527
	Seismic Vertical Design Force, F <sub>v</sub>	[lbs]	220
	total roof attachments req for lateral	1	60% of the vertical resisting load (0.6 * W <sub>p</sub> ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof total roof attachments req for vertical
		1	# attachments are required for the vertical forces.

Array Informations			
qty	item	weight	total
15	Modules + Deflectors	83.3	54.22
30	Ballast CMU Block	13.4	402.0
18	North Support	19.44	349.9
6	South Support	12.75	76.5
0	Middle Support	0.0	0.0
	% of Mechanical Attachments to Supports Ratio	4%	
	area, SQFT	421	
	total weight, LBS	1642	
	total load, PSF	3.9	
	total mech attach	1	

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

##### 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters	Output Values		
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

##### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a <i>nonbuilding structure</i> as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements			
13.2	Description	Symbol	Value/Comment
13.2.1	Applicable Requirements for Architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2	Special Certification Requirements	N/A	
13.2.3	Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4	Flexibility		Flexibility as well as strength must be considered
13.2.5	Testing Alternative		components tested to ICC-ES AC 156 are acceptable
13.2.6	Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required per table 13.2-1
13.2.7	Construction Documents		
13.3 Seismic Demands on Nonstructural Components			
13.3.1	Seismic Design Force		$F_p = (0.4 * F_p^{*} SDS^{*} W_p) / (R_p / p) * (1 + z/h) / 1.4$
		[lbs]	$F_p = 563$
			$F_p = 2655$
			$F_{p\max} = 498$
	spectral acceleration, short period [g]	SDS	1.011
	component amplification factor (table 13.6-1)	ap	1.00
	Component Importance Factor	ip	1.00
	Operating Weight (total load of array) [lbs]	Wp	1642
	Response modification Factor (table 13.5-1 or 13.6-1) point of component attachment [ft]	Rp	2.50
	average roof height [ft]	z	25
	concurrent vertical load [lb]	h	25
	vertical resisting load	f_v	$= (2 * SDS^{*} W_p) / 1.4$
			237
			$0.9 * W_p$
13.3.2	Seismic Relative Displacements		1478
13.4	Nonstructural Component Anchorage		Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3-1 except that modifications to $F_p$ and $R_p$ due to anchorage conditions need not be considered
13.4.1	Design Forces		The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
	roof attach lateral strength		628 [lbs]
	roof attach vertical strength		808 [lbs]
	Seismic Lateral Design Force, $F_p$		569 [lbs]
	Seismic Vertical Design Force, $F_v$		237 [lbs]
	total roof attachments req for lateral		1
	total roof attachments req for vertical		1
			60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.

Array Informations		
Qty	Item	weight
13	Modules + Deflectors	54.22
30	Ballast CMU Block	705
13.4		402.0
16	North Support	19.44
		31.10
6	South Support	12.75
		76.5
0	Middle Support	0.0
	% of Mechanical Attachments to Supports Ratio	5%
	area, SQFT	370
	total weight, LBS	14.94
	total load, PSF	4.0
	total mech attach	1

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

##### 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405-1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.2 Site Class	D		
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.555	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

##### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

## General Design Requirements

13.2	Description	Symbol	Value/Comment
13.2.1	Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections 13.2, 13.3, 13.4, 13.6
13.2.2	Special Certification Requirements		N/A
13.2.3	Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4	Flexibility		Flexibility as well as strength must be considered
13.2.5	Testing Alternative		Components tested to ICC-ES AC 156 are acceptable
13.2.6	Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7	Construction Documents		

## 13.3 Seismic Demands on Nonstructural Components

13.3.1	Seismic Design Force	$F_p = (0.4 * \alpha * SDS * W_p) / (R_p / h) * (1 + 2z/h) / 1.4$	
		$F_p = 518$	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		$F_{pmax} = 2417$	
		$F_{pmin} = 453$	
	spectral acceleration, short period [g]	SDS 1.011	
	component amplification factor (table 13.6-1)	$\alpha = 1.00$	
	Component Importance Factor	Ib 1.00	
	Operating Weight (total load of array) [lbs]	$W_p = 1494$	
	Response modification Factor (table 13.5-1 or 13.6-1)	$R_p = 2.50$	
	point of component attachment [ft]	$z = 25$	Only ratio $z/h$ is used, which is 1.0
	average roof height [ft]	$h = 25$	Only ratio $z/h$ is used, which is 1.0
	concurrent vertical load [lb]	$F_v = (2 * SDS * W_p) / 1.4$	$F_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
		216	
	vertical resisting load	$216 * DL$	
		1345	$0.9 * W_p$
13.3.2	Seismic Relative Displacements		

13.4	Nonstructural Component Anchorage		Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional resistance. The component forces shall be those determined in section 13.3.1 except that modifications to $F_p$ and $R_p$ due to anchorage conditions need not be considered
			The force shall be determined based on the prescribed forces and displacements for the component determined in sections 13.3.1 and 13.3.2
13.4.1	Design Forces		
	roof attach lateral strength	628 [lbs]	
	roof attach vertical strength	808 [lbs]	
	Seismic Lateral Design Force, $F_p$	518 [lbs]	
	Seismic Vertical Design Force, $F_v$	216 [lbs]	
	total roof attachments req for lateral	1	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof attachments are required for the vertical forces.
	total roof attachments req for vertical	1	

Array Informations			
Qty	Item	weight	total
14	Modules + Deflectors	54.22	759
30	Ballast CMU Block	13.4	402.0
18	North Support	19.44	349.9
5	South Support	12.75	63.8
0	Middle Support	0.00	0.0
% of Mechanical Attachments to Supports Ratio		4%	
area, SQFT		397	
total weight, LBS		1575	
total load, PSF		4.0	
total mech attach		1	

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

11.4 Seismic Ground Motion Values			
Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	
11.4.2 Site Class	D		A, B, C D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fy	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sect 11.4. =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sect 11.4. Fy*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	Output Values		
1 second period	SDs 1.011	11.4.3, 2/3*Sms	
	SD1 0.555	11.4.4, 2/3*Sml1	

#### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
Same as parent structure is site soil conditions		
13.1.2 Seismic Design Category	D	Unknown
13.1.3 Component Importance Factor	Ip	1.00
13.1.4 Exemptions		do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a <i>nonbuilding structure</i> as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

#### General Design Requirements

Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13-2-1 states that mechanical and electrical supports must meet sections 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements		N/A

13.2.3 Consequential Damage	cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4 Flexibility	Flexibility as well as strength must be considered components tested to ICC-ES AC 156 are acceptable
13.2.5 Testing Alternative	
13.2.6 Use of Experience Data	An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by table 13.2-1
13.2.7 Construction Documents	

### **13.3 Seismic Demands on Nonstructural Components**

13.3 Seismic Demands on Nonstructural Components			
13.3.1 Seismic Design Force			
F <sub>p</sub>	F <sub>p</sub> =[0.4*(3*SDS''*W <sub>p</sub> )/(R <sub>p</sub> /I <sub>b</sub> )][(1+2z/h)/1.4]		F <sub>p</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
[lbs]	F <sub>p1</sub>		
	F <sub>pmax</sub>		
	F <sub>pmin</sub>		
spectral acceleration, short period [g]	SDS 1.011		
component amplification factor (table 13.6-1)	ap 1.00		
Component Importance Factor	I <sub>p</sub> 1.00		
Operating Weight (total load of array) [lbs]	W <sub>p</sub> 4		
Response modification Factor (table 13.5-1 or 13.6-1)	R <sub>p</sub> 2.50		
point of component attachment [ft]	2.25		Only ratio z/h is used, which is 1.0
average roof height [ft]	h 25		Only ratio z/h is used, which is 1.0
concurrent vertical load [lb]	f <sub>v</sub> = 1.2*(SDS''*W <sub>p</sub> )/1.4		f <sub>v</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	1		
vertical resisting load	3 <sup>rd</sup> D <sub>1</sub>		
	4		0.9*W <sub>p</sub>
13.3.2 Seismic Relative Displacements			

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13.4 Nonstructural Component Anchorage		Components shall be bolted, welded or otherwise positively fastened without consideration for frictional and 13.3.2
13.4.1 Design Forces	roof attach lateral strength	628 [lbs]
	Roof attach vertical strength	808 [lbs]
	Seismic Lateral Design Force, $F_{pl}$	1 [lbs]
	Seismic Vertical Design Force, $F_v$	1 [lbs]
	total roof attachments req for lateral	1
	total roof attachments req for vertical	1
	‡ 60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof	

Array Informations		
Qty	Item	Weight
12	Modules + Deflectors	54.22
30	Ballast CMU Block	651
		13.4 402.0
16	North Support	19.44
		311.0
5	South Support	12.75
		63.8
0	Middle Support	0.0
	% of Mechanical Attachments to Supports Ratio	5%
area, SQFT		347
total weight, LBS		1427
total load, PSF		4.1
total mech attach		1

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

11.4 Seismic Ground Motion Values		
Description	Symbol	Input Values
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA
11.4.1 Mapped acceleration parameters		
mapped MCE spectral response, short periods	Ss	1.516
mapped MCE spectral response, 1 second	S1	0.555
11.4.2 Site Class	D	
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters		
Site coefficient, short period	Fa	1.000
Site coefficient, 1 second	Fv	1.500
mapped MCE spectral response at short period	Sms	1.516
mapped MCE spectral response at 1 second period	Sm1	0.833
11.4.4 Design Spectral Acceleration Parameters		
Short Periods	SDs	1.011
1 second period	SD1	0.555
		11.4.3, 2/3*Sm1
		11.4.4, 2/3*Sm1

#### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value\Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00
13.1.5 Applicability of Nonstructural Component Requirements		13.1.3 Does not meet conditions requiring a 1.5 importance factor
13.1.6 Reference Documents		do not meet any exemptions
13.1.7 Reference Documents using allowable Stress Design		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
		12.7.2 Definition of effective seismic weight W

#### 13.2 General Design Requirements

Description	Symbol	Value\Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements		N/A

13.2.3 Consequential Damage		cannot cause failure of other essential architectural, electrical for mechanical components
13.2.4 Flexibility		Flexibility as well as strength must be considered
13.2.5 Testing Alternative		components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13-2-1
13.2.7 Construction Documents		

13.3 Seismic Demands on Nonstructural Components		
13.3.1 Seismic Design Force		
	$F_p = (0.4 * a_p * SDS^2 * W_p) / (R_p / p) * (z + 22/h) / h / 1.4$	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
[lbs]	$F_{ph}$ 1	
	$F_{ph}$ 7	
	$F_{pmax}$ 7	
	$F_{pmin}$ 1	
spectral acceleration, short period [g]	SDS 1.011	
component amplification factor (table 13-6-1)	$a_p$ 1.00	
Component Importance Factor	$I_p$ 1.00	
Operating Weight (total load of array) [lbs]	$W_p$ 4	
Response modification Factor (table 13-5-1 or 13-6-1)	$R_p$ 2.50	1
point of component attachment [ft]	$z$ 25	Only ratio $z/h$ is used, which is 1.0
average roof height [ft]	$h$ 25	Only ratio $z/h$ is used, which is 1.0
concurrent vertical load [lb]	$F_v = (2 * SDS^2 * W_p) / 1.4$	$F_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	$S_{VDL}$	
vertical resisting load	4	$0.9 * W_p$
13.3.2 Seismic Relative Displacements		

13.4 Nonstructural Component Anchorage		
Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional and 13.3.2		
13.4.1 Design Forces		
	roof attach lateral strength	628 [lbs]
	roof attach vertical strength	808 [lbs]
	Seismic Lateral Design Force, $F_p$	1 [lbs]
	Seismic Vertical Design Force, $F_v$	1 [lbs]
	total roof attachments req for lateral	1
	total roof attachments req for vertical	1
	‡	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof

Array Informations		
Qty	Item	weight
7	Modules + Deflectors	54.22
22	Ballast CMU Block	380 13.4 294.8
10	North Support	19.44 194.4
4	South Support	12.75 51.0
0	Middle Support	0.0
	% of Mechanical Attachments to Supports Ratio	7%
area_sqft		210
total weight, LBS		920
total load, PSF		4.4
total mech attach		1

**ASCE 7-05 Seismic Worksheet for Non-Structural Members****11.4 Seismic Ground Motion Values**

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and S5 less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters	S1	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, short period	S5	0.555	Figures 22-1 to 22-14
11.4.2 Site Class	D		A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fg	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.8333	Sec 11.4, Fv*S1
11.4.4 Design Spectra Acceleration Parameters			
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

**13.1 Seismic Design Requirements for Nonstructural components**

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a <i>nonbuilding structure</i> as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

**General Design Requirements**

Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13-2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements		N/A

13.2.3 Consequential Damage		cannot cause failure of other essential architectural, electrical for mechanical components
13.2.4 Flexibility		Flexibility as well as strength must be considered
13.2.5 Testing Alternative		components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by table 13.2-1
13.2.7 Construction Documents		

13.3 Seismic Demands on Nonstructural Components		
13.3.1 Seismic Design Force		
	$F_p = [(0.4 * \alpha_p * SDS * W_p) / (R_p / I_p)] * (1+2Z/h) / 1.4$	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	$F_{ph}$ [lbs]	
	$F_{pmax}$ 7	
	$F_{pmin}$ 1	
spectral acceleration, short period [g]	SDS 1.011	
component amplification factor (table 13.6-1)	$\alpha_p$ 1.00	
Component Importance Factor	I_p 1.00	
Operating Weight (total load of array) [lbs]	$W_p$ 4	
Response modification Factor (table 13.5-1 or 13.6-1)	$R_p$ 2.50	
point of component attachment [ft]	$Z$ 25	Only ratio $Z/h$ is used, which is 1.0
average roof height [ft]	$h$ 25	Only ratio $Z/h$ is used, which is 1.0
concurrent vertical load [lb]	$F_v$ $= (2 * SDS * W_p) / 1.4$	$F_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
vertical resisting load	$9 * D_L$	$0.9 * W_p$
	4	
13.3.2 Seismic Relative Displacements		

13.4 Nonstructural Component Anchorage		
Components shall be bolted, welded or otherwise positively fastened without consideration for frictional		
and 13.3.2		
13.4.1 Design Forces	Roof attach lateral strength	628 [lbs]
	Roof attach vertical strength	808 [lbs]
	Seismic Lateral Design Force, $F_p$	2 [lbs]
	Seismic Vertical Design Force, $F_v$	1 [lbs]
	total roof attachments req for lateral	1
	total roof attachments req for vertical	4
		60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof

Array Informations			
qty	item	weight	total
7	Modules + Deflectors	54.22	380
22	Ballast CMU Block	13.4	294.8
10	North Support	19.44	194.4
4	South Support	12.75	51.0
0	Middle Support	0.0	0.0
% of Mechanical Attachments to Supports Ratio		7%	
area, SQFT		20.9	
total weight, LBS		920	
total load, PSF		4.4	
total mech attach		1	

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

##### 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Comments
	Zip Code	93405	150 MADONNA RD, SAN LUIS OBISPO, CA
11.4.1 Mapped acceleration parameters			If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	Figures 22-1 to 22-14
11.4.2 Site Class	D		A, B, C, D, E or F. D is default if site soil properties unknown - See table table 20.3.1
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.555	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	0.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

##### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		
13.1.7 Reference Documents using allowable Stress Design		

##### General Design Requirements

Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements		N/A

13.2.3 Consequential Damage		cannot cause failure of other essential architectural, electrical for mechanical components
13.2.4 Flexibility		Flexibility as well as strength must be considered
13.2.5 Testing Alternative		Components tested to ICC-ES AC 155 are acceptable
13.2.6 Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by table 13.2-2
13.2.7 Construction Documents		

### 13.3 Seismic Demands on Nonstructural Components

#### 13.3.1 Seismic Design Force

		$F_p = ((0.4 * \alpha * SDS * W_d) / (R_d *  p )) * (1 + 2z/h) / 1.4$
[lbs]	$F_{ph}$ [2]	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	$F_{pmax}$ [7]	
	$F_{pmin}$ [1]	
spectral acceleration, short period [g]	SDS 1.011	
component amplification factor (table 13.6-1)	$\alpha$ 1.00	
Component Importance Factor	$I_p$ 1.00	
Operating Weight (total load of array) [lbs]	$W_o$ 4	
Response modification Factor (table 13.5-1 or 13.6-1)	$R_p$ 2.50	
point of component attachment [ft]	z 25	Only ratio z/h is used, which is 1.0
average roof height [ft]	h 25	Only ratio z/h is used, which is 1.0
concurrent vertical load [lb]	$F_v = (1.2 * SDS * W_d) / 1.4$	$F_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
vertical resisting load	$0.9 * W_d$	
13.3.2 Seismic Relative Displacements	4	

#### 13.4 Nonstructural Component Anchorage

##### 13.4.1 Design Forces

roof attach lateral strength	628 [lbs]	Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional and 13.3.2
roof attach vertical strength	808 [lbs]	
Seismic Lateral Design Force, $F_p$	2 [lbs]	
Seismic Vertical Design Force, $F_v$	1 [lbs]	
total roof attachments req for lateral	1	
total roof attachments req for vertical	4	60% of the vertical resisting load ( $0.6 * W_d$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof

Array Informations		
Qty	Item	Weight
12	Modules + Deflectors	54.22
31	Ballast CMU Block	651 13.4/45.4
16	North Support	19.44 311.0
5	South Support	12.75 63.8
0	Middle Support	0.0
	% of Mechanical Attachments to Supports Ratio	5%
	area, SQFT	347
	total weight, LBS	1441
	total load, PSF	4.2
	total mech attach	1

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

##### 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.5555	Figures 22-1 to 22-14
11.4.2 Site Class	D		A, B, C, D, E or F. D is default if site soil properties unknown - See table table 20.3.1
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4 , =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.5555	11.4.4, 2/3*Sm1

##### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00
13.1.5 Applicability of Nonstructural Component Requirements		do not meet any exemptions
13.1.6 Reference Documents		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.7 Reference Documents Using allowable Stress Design		12.7.2 Definition of effective seismic weight W

##### 13.2 General Design Requirements

Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements		N/A

13.2.3 Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4 Flexibility		Flexibility as well as strength must be considered
13.2.5 Testing Alternative		components tested to ICC-ES AC 155 are acceptable
13.2.6 Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7 Construction Documents		

### 13.3 Seismic Demands on Nonstructural Components

#### 13.3.1 Seismic Design Force

		$F_p = [(0.4^2 * \alpha_p * SDS * W_0) / (R_p / \rho)] * (1 + z/h) / 1.4$	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	$F_{ph}$ [lbs]	$F_{ph} 1$	
	$F_{pmax}$	$F_{pmax} 7$	
	$F_{pmin}$	$F_{pmin} 1$	
spectral acceleration, short period [g]	SDS 1.011		
component amplification factor (table 13.6-1)	ap. 1.00		
Component Importance Factor	Ip 1.00		
Operating Weight (total load of array) [lbs]	$W_p 4$		
Response modification Factor (table 13.5-1 or 13.6-1)	$R_p 2.50$		
point of component attachment [ft]	$z 25$	Only ratio $z/h$ is used, which is 1.0	
average roof height [ft]	$h 25$	Only ratio $z/h$ is used, which is 1.0	
concurrent vertical load [lb]	$f_v 1 = (2 * SDS * W_p) / 1.4$	$f_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC	
	$1$		
vertical resisting load	$2 * DL 4$	$0.9 * W_p$	
	$4$		

#### 13.3.2 Seismic Relative Displacements

#### 13.4 Nonstructural Component Anchorage

		Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional and 13.3.2
13.4.1 Design Forces	roof attach lateral strength	628 [lbs]
	roof attach vertical strength	808 [lbs]
	Seismic Lateral Design Force, $F_p$	1 [lbs]
	Seismic Vertical Design Force, $F_v$	1 [lbs]
total roof attachments req for lateral	1	total roof attachments req for vertical
	1	# 60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof

Array Informations		
qty	Item	weight
36	Modules + Deflectors	56.22
51	Ballast CMU Block	13.4
40	North Support	77.76
11	South Support	140.3
0	Middle Support	0.0
% of Mechanical Attachments to Supports Ratio		2%
area, SQFT		981
total weight, LBS		3553
total load, PSF		3.6
total mech attach		1

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

##### 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405	1550 MADONNA RD, SAN LUIS OBISPO, CA
11.4.1 Mapped acceleration parameters			If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	Figures 22-1 to 22-14

A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1

##### 11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters

Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4 , =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters	Output Values		
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

##### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	I	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

##### General Design Requirements

Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections 13.2, 13.3, 13.4, 13.5
13.2.2 Special Certification Requirements		N/A

13.2.3 Consequential Damage		cannot cause failure of other essential architectural, electrical for mechanical components
13.2.4 Flexibility		Flexibility as well as strength must be considered
13.2.5 Testing Alternative		Components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by table 13.2.1
13.2.7 Construction Documents		

### 13.3 Seismic Demands on Nonstructural Components

13.3.1 Seismic Design Force		
	$F_p = (0.4 * \alpha_p * SDS * W_p) / (R_p / D_p) * (1 + 2z/h) / 1.4$	Fp values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
[lbs]	$F_{ph}$	
	$F_{pmax}$	
	$F_{pmin}$	
spectral acceleration, short period [g]	SDS 1.011	
component amplification factor (table 13.6-1)	ap 1.00	
Component Importance Factor	Ip 1.00	
Operating Weight (total load of array) [lbs]	Wp 4	
Response modification Factor (table 13.5-1 or 13.6-1)	Rp 2.50	
point of component attachment [ft]	2.25	Only ratio z/h is used, which is 1.0
average roof height [ft]	h 25	Only ratio z/h is used, which is 1.0
concurrent vertical load [lb]	$F_v = (2 * SDS * W_p) / 1.4$	$F_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	1	
vertical resisting load	$9 * D_L$	
	3	$0.9 * W_p$
13.3.2 Seismic Relative Displacements		

### 13.4 Nonstructural Component Anchorage

13.4.1 Design Forces	Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional and 13.3.2
roof attach lateral strength	628 [lbs]
roof attach vertical strength	808 [lbs]
Seismic Lateral Design Force, Fp	1 [lbs]
Seismic Vertical Design Force, Fv	1 [lbs]
total roof attachments req for lateral	1
total roof attachments req for vertical	‡ 60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof

Array Informations		
qty	item	weight
12	Modules + Deflectors	54.22
30	Ballast CMU Block	13.4
16	North Support	19.44
5	South Support	31.10
0	Middle Support	12.75
0	% of Mechanical Attachments to Supports Ratio	63.8
	area SQFT	0.0
	total weight, LBS	5%
	total load, PSF	370
	total mech attach	1427
		3.9
		1

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

##### 11.4 Seismic Ground Motion Values

Description	Symbol/Input Values	Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA
11.4.1 Mapped acceleration parameters		If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design Category A only applies
	mapped MCE spectral response, short periods	Figures 22-1 to 22-14
	mapped MCE spectral response, 1 second	Figures 22-1 to 22-14
11.4.2 Site Class	D	A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters		
	Site coefficient, short period	Fa 1.000 table 11.4-1
	Site coefficient, 1 second	Fv 1.500 table 11.4-2
	mapped MCE spectral response at short period	Sms 1.516 Sec 11.4 , =Fa*Ss
	mapped MCE spectral response at 1 second period	Sm1 0.833 Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters		
	Short Periods	Output Values SDs 1.011 11.4.3, 2/3*Sms
	1 second period	SD1 0.555 11.4.4, 2/3*Sm1

##### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 13.1.3 Does not meet conditions requiring a 1.5 importance factor do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

##### General Design Requirements

13.2	Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports			Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements		N/A	

		cannot cause failure of other essential architectural, electrical for mechanical components
13.2.3 Consequential Damage		
13.2.4 Flexibility		Flexibility as well as strength must be considered
13.2.5 Testing Alternative		components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7 Construction Documents		

13.3 Seismic Demands on Nonstructural Components		
13.3.1 Seismic Design Force		
	$F_p = (0.4 * a_p * S_{DS} * W_p) / (R_p / \beta_p) * (1 + 2z/h) / 1.4$	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
$F_p$ [lbs]	$F_{ph}$ 1	
	$F_{pmax}$ 6	
	$F_{pmin}$ 1	
spectral acceleration, short period [g]	$S_{DS}$ 1.01.1	
component amplification factor (table 13.6-1)	$a_p$ 1.00	
Component Importance Factor	$I_p$ 1.00	
Operating Weight (total load of array) [lbs]	$W_p$ 4	
Response modification Factor (table 13.5-1 or 13.6-1)	$R_p$ 2.50	1
point of component attachment [ft]	$z$ 25	Only ratio $z/h$ is used, which is 1.0
average roof height [ft]	$h$ 25	Only ratio $z/h$ is used, which is 1.0
concurrent vertical load [lb]	$F_v = (2 * S_{DS} * W_p) / 1.4$	$F_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	1	
	$g_{vR}$	
vertical resisting load	$0.9 * W_p$	
	3	
13.3.2 Seismic Relative Displacements		

13.4 Nonstructural Component Anchorage		
Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional and 13.3.2		
13.4.1 Design Forces	roof attach lateral strength	628 [lbs]
	roof attach vertical strength	808 [lbs]
	Seismic Lateral Design Force, $F_p$	1 [lbs]
	Seismic Vertical Design Force, $F_v$	1 [lbs]
	total roof attachments req for lateral	1
	total roof attachments req for vertical	1
	‡ 60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof	

**Array Informations**

Qty	Item	Weight	Total
12	Moulties + Deflectors	54.22	651
26	Ballast CMU Block	13.4	348.4
15	North Support	19.44	291.6
5	South Support	12.75	63.8
0	Middle Support	0.0	0.0
	% of Mechanical/Attachments to Supports Ratio	5%	
	area, SQFT	340	
	total weight, LBS	1354	
	total load, PSF	4.0	
	total mech attach	1	

**ASCE 7-05 Seismic Worksheet for Non-Structural Members****11.4 Seismic Ground Motion Values**

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	
11.4.1 Mapped acceleration parameters			If \$1 is less than or equal to .04 and \$5 less than or equal to 0.15 Then Seismic Design category A only applies
mapped MCE spectral response, short periods	\$5	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	\$1	0.555	Figures 22-1 to 22-14
11.4.2 Site Class	D		A, B, C, D, E or F is default if site soil properties unknown. See table table 20.3.1
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	15.16	Sec 11.4 , =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	1.011	11.4-3, 2/3*Sms
1 second period	SD1	0.555	11.4-4, 2/3*Sml1

**13.1 Seismic Design Requirements for Nonstructural components**

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00
		do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents Using allowable Stress Design		

**General Design Requirements**

Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements		N/A

13.2.3 Consequential Damage		cannot cause failure of other essential architectural, electrical for mechanical components
13.2.4 Flexibility		Flexibility as well as strength must be considered components tested to ICC-ES AC 156 are acceptable
13.2.5 Testing Alternative		
13.2.6 Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7 Construction Documents		

<b>13.3 Seismic Demands on Nonstructural Components</b>		
<b>13.3.1 Seismic Design Force</b>		
$F_b = ((0.4 * \alpha_p * SDS * W_p) / (R_p / \beta))^{(1-2z/h)/1.4}$		$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
$F_{ph}$ [lbs]	$F_{ph}$ 1	
$F_{pmax}$ 6	$F_{pmax}$ 6	
$F_{pmin}$ 1	$F_{pmin}$ 1	
SDS 1.011	SDS 1.011	
component amplification factor (table 13.6-1)	ap 1.00	Only ratio $z/h$ is used, which is 1.0
Component Importance Factor	Ip 1.00	Only ratio $z/h$ is used, which is 1.0
Operating Weight (total load of array) [lbs]	Wp 4	$F_V$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
Response modification Factor (table 13.5-1 or 13.6-1)	Rp 2.50	
point of component attachment [ft]	z 25	
average roof height [ft]	h 25	
concurrent vertical load [lb]	$F_V = (2 * SDS * W_p) / 1.4$	
	1	
vertical resisting load	$0.9 * W_p$	
	4	
<b>13.3.2 Seismic Relative Displacements</b>		

<b>13.4 Nonstructural Component Anchorage</b>		
<b>Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional and 13.3.2</b>		
13.4.1 Design Forces	rof attach lateral strength	628 [lbs]
	rof attach vertical strength	308 [lbs]
	Seismic Lateral Design Force, $F_p$	1 [lbs]
	Seismic Vertical Design Force, $F_V$	1 [lbs]
	total roof attachments req for lateral	1
	total roof attachments req for vertical	1
	‡	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof

Array Informations		
Qty	Item	Weight
12	Modules + Deflectors	54.22
26	Balast CMU Block	651
		13.4
15	North Support	348.4
		19.44
5	South Support	291.6
		12.75
0	Middle Support	63.8
		0.0
	% of Mechanical Attachments to Supports Ratio	5%
	area, SQFT	341
	total weight, LBS	1554
	total load, PSF	4.0
	total mech attach	1

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

##### 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design Category A only applies
11.4.1 Mapped acceleration parameters		Ss 1.516	Figures 22-1 to 22-14
		S1 0.555	Figures 22-1 to 22-14
11.4.2 Site Class	D		A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1

##### 11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters

Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4. =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4. , Fv*S1
11.4.4 Design Spectral Acceleration Parameters	Output Values		
Short Periods	SDs	1.011	11.4.3. 2/3*Sms
1 second period	SD1	0.555	11.4.4. 2/3*Sm1

##### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00
		do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

##### General Design Requirements

Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements		N/A

13.2.3 Consequential Damage		cannot cause failure of other essential architectural, electrical for mechanical components
13.2.4 Flexibility		Flexibility as well as strength must be considered
13.2.5 Testing Alternative		components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required be table 13.2-1
13.2.7 Construction Documents		

<b>13.3 Seismic Demands on Nonstructural Components</b>		
<b>13.3.1 Seismic Design Force</b>		
		$F_p = ((0.4 * \rho_p * SDS * W_p) / (R_d / \beta)) * (1 - 2z/h) / 1.4$
		F <sub>p</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
[lbs]	F <sub>ph</sub> 1	
	F <sub>pmax</sub> 6	
	F <sub>pmin</sub> 1	
spectral acceleration, short period [g]	SDS 1.011	
component amplification factor (table 13.6-1)	ap 1.00	
Component Importance Factor	I 1.00	
Operating Weight (total load of array) [lbs]	W <sub>p</sub> 4	
Response modification Factor (table 13.5-1 or 13.6-1)	R <sub>p</sub> 2.50	
point of component attachment [ft]	z 25	Only ratio z/h is used, which is 1.0
average roof height [ft]	h 25	Only ratio z/h is used, which is 1.0
concurrent vertical load [lb]	F <sub>v</sub> = (2 * SDS * W <sub>p</sub> ) / 1.4	F <sub>v</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
vertical resisting load	9 * DL 4	0.9 * W <sub>p</sub>
<b>13.3.2 Seismic Relative Displacements</b>		

<b>13.4 Nonstructural Component Anchorage</b>		
<b>Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional and 13.3.2</b>		
13.4.1 Design Forces		
roof attach lateral strength	628 [lbs]	
roof attach vertical strength	808 [lbs]	
Seismic Lateral Design Force, F <sub>p</sub>	1 [lbs]	
Seismic Vertical Design Force, F <sub>v</sub>	1 [lbs]	
total roof attachments req for lateral	1	
total roof attachments req for vertical	4	60% of the vertical resisting load (0.6 * W <sub>p</sub> ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof

Array Informations		
Qty	Item	Weight
12	Modules + Deflectors	54.22
26	Ballast CMU Block	651 13.4 348.4
15	North Support	19.44 291.6
5	South Support	12.75 63.8
0	Middle Support	0.0
% of Mechanical Attachments to Supports Ratio		5%
area, SQFT		341
total weight, LBS		1354
total load, PSF		4.0
total mech attach		1

#### 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	
11.4.2 Site Class	D		A, B, C, D, E or F. D is default if site soil properties unknown - See table table 20.3.1
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4 , =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	1.011	11.4.3 , 2/3*Sms
1 second period	SD1	0.555	11.4.4 , 2/3*Sm1

#### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents Using allowable Stress Design		

#### General Design Requirements

Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3,13.4,13.6
13.2.2 Special Certification Requirements		N/A

13.2.3 Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4 Flexibility		Flexibility as well as strength must be considered
13.2.5 Testing Alternative		Components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by table 13.2-1
13.2.7 Construction Documents		

### 13.3 Seismic Demands on Nonstructural Components

#### 13.3.1 Seismic Design Force

		$F_p = ((0.4 * \alpha * SDS * W_p) / (R_p *  p )) * (1 + 2z/h) / 1.4$	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
[lbs]	$F_{ph}$	1	
	$F_{pmax}$	6	
	$F_{pmin}$	1	
spectral acceleration, short period [g]	SDS	1.011	
component amplification factor (table 13.6-1)	$\alpha_p$	1.00	
Component Importance Factor	$I_p$	1.00	
Operating Weight (total load of array) [lbs]	$W_o$	4	
Response modification Factor (table 13.5-1 or 13.6-1)	$R_p$	2.50	1
point of component attachment [ft]	$z$	2.25	Only ratio $z/h$ is used, which is 1.0
average roof height [ft]	$h$	2.25	Only ratio $z/h$ is used, which is 1.0
concurrent vertical load [lb]	$F_v$	$(2 * SDS * W_o) / 1.4$	$F_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	$I_v$	1	
vertical resisting load	$g * D_L$	$0.9 * W_p$	
	4		
13.3.2 Seismic Relative Displacements			

#### 13.4 Nonstructural Component Anchorage

##### 13.4.1 Design Forces

roof attach lateral strength	628 [lbs]	
roof attach vertical strength	808 [lbs]	
Seismic Lateral Design Force, $F_p$	1 [lbs]	
Seismic Vertical Design Force, $F_v$	1 [lbs]	
total roof attachments req for lateral	1	
total roof attachments req for vertical	1	# 60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof

Array Informations			
Qty	Item	Weight	Total
10	Moudles + Deflectors	54.22	542
26	Ballast CMU Block	13.4	348.4
14	North Support	19.44	272.2
4	South Support	12.75	51.0
0	Middle Support	0.0	0.0
% of Mechanical Attachments to Supports Ratio		6%	
area, SQFT		292	
total weight, LBS		1214	
total load, PSF		4.2	
total mech attach		1	

#### 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	
11.4.1 Mapped acceleration parameters			If S1 is less than or equal to .04 and S5 less than or equal to 0.15 Then Seismic Design category A only applies
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	Figures 22-1 to 22-14
11.4.2 Site Class	D		A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4 , =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sm1

#### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00
13.1.5 Applicability of Nonstructural Component Requirements		do not meet any exemptions the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		13.1.3 Does not meet conditions requiring a 1.5 importance factor 12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		
13.2	General Design Requirements	
Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections:13.2, 13.3,13.4,13.6
13.2.2 Special Certification Requirements		N/A

13.2.3 Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4 Flexibility		Flexibility as well as strength must be considered
13.2.5 Testing Alternative		Components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by table 13.2-1
13.2.7 Construction Documents		

### 13.3 Seismic Demands on Nonstructural Components

#### 13.3.1 Seismic Design Force

	F <sub>p</sub>	F <sub>p</sub> = $(0.4^2 * \text{ap} * \text{SDS} * \text{W}_p) / (\text{R}_p / \text{I}_{\text{p}}) * [1 + z/h] / 1.4$	F <sub>p</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
F <sub>ph</sub> [lbs]	F <sub>ph</sub> 1		
F <sub>pmax</sub> 7			
F <sub>pmin</sub> 1			
spectral acceleration, short period [g]	SDS 1.011		
component amplification factor (table 13.6-1)	ap 1.00		
Component Importance Factor	I <sub>p</sub> 1.00		
Operating Weight (total load of array) [lbs]	W <sub>p</sub> 4		
Response modification Factor (table 13.5-1 or 13.6-1) point of component attachment [ft]	R <sub>p</sub> 2.50		
average roof height [ft]	z 25	Only ratio z/h is used, which is 1.0	
concurrent vertical load [lb]	h 25	Only ratio z/h is used, which is 1.0	
	F <sub>v</sub> = $(2 * \text{SDS} * \text{W}_p) / 1.4$	F <sub>v</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC	
	1		
vertical resisting load	9 * Q <sub>L</sub>	0.9 * W <sub>p</sub>	
	4		
13.3.2 Seismic Relative Displacements			

#### 13.4 Nonstructural Component Anchorage

##### 13.4.1 Design Forces

roof attach lateral strength	628 [lbs]	
roof attach vertical strength	808 [lbs]	
Seismic Lateral Design Force, F <sub>p</sub>	1 [lbs]	
Seismic Vertical Design Force, F <sub>v</sub>	1 [lbs]	
total roof attachments req for lateral	1	
total roof attachments req for vertical	1	# 60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof

Array Informations			
Qty	Item	Weight	Total
25	Modules + Deflectors	54.22	1355
42	Ballast CMU Block	13.4	562.8
29	North Support	19.44	563.8
8	South Support	12.75	102.0
0	Middle Support	0.0	0.0
	% of Mechanical Attachments to Supports Ratio	3%	
	area, SQFT	689	
	total weight, LBS	2584	
	total load, PSF	3.8	
	total mech attach	1	

**ASCE 7-05 Seismic Worksheet for Non-Structural Members****11.4 Seismic Ground Motion Values**

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	
11.4.2 Site Class	D		A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4. =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4. Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	1.011	11.4-3, 2/3*Sms
1 second period	SD1	0.555	11.4-4, 2/3*Sm1

**13.1 Seismic Design Requirements for Nonstructural components**

Description	Symbol	Value/Comment
		Same as parent structure is site soil conditions
13.1.2 Seismic Design Category	D	Unknown
13.1.3 Component Importance Factor	Ip	1.00
13.1.4 Exemptions		do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

**General Design Requirements**

Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements		N/A

13.2.3 Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4 Flexibility		Flexibility as well as strength must be considered
13.2.5 Testing Alternative		Components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by table 13.2-1
13.2.7 Construction Documents		

13.3 Seismic Demands on Nonstructural Components		
13.3.1 Seismic Design Force		
	$F_p = ((0.4 * \alpha * SDS * W_p) / (R_p / p)) * (1 + 2z/h) / 1.4$	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
[lbs]	$F_{ph}$ [1]	
	$F_{ph}$ [2]	
	$F_{ph}$ [6]	
	$F_{pmax}$ [6]	
	$F_{pmin}$ [1]	
spectral acceleration, short period [g]	SDS 1, 0.011	
component amplification factor (table 13.6-1)	$\alpha_p$ 1.00	
Component Importance Factor	$I_p$ 1.00	
Operating Weight (total load of array) [lbs]	$W_p$ 4	
	$R_p$ 2.50	1
Response modification Factor (table 13.5-1 or 13.6-1)	point of component attachment [ft]	Only ratio $z/h$ is used, which is 1.0
	2.25	Only ratio $z/h$ is used, which is 1.0
average roof height [ft]	$h$ 25	
concurrent vertical load [lb]	$F_v = (2 * SDS * W_p) / 1.4$	$F_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	1	
vertical resisting load	$9 * D_L$	$0.9 * W_p$
	3	
13.3.2 Seismic Relative Displacements		

13.4 Nonstructural Component Anchorage		
Components shall be bolted, welded or otherwise positively fastened without consideration for frictional and 13.3.2		
13.4.1 Design Forces		
	roof attach lateral strength	628 [lbs]
	roof attach vertical strength	803 [lbs]
	Seismic Lateral Design Force, $F_p$	1 [lbs]
	Seismic Vertical Design Force, $F_v$	1 [lbs]
	total roof attachments req for lateral	1
	total roof attachments req for vertical	# 60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof

Array Informations		
qty	item	weight
25	Modules + Deflectors	54.22
42	Ballast Civil Block	13.4
29	North Support	19.44
8	South Support	12.75
0	Middle Support	0.0
	% of Mechanical Attachments to Supports Ratio	3%
	area, SQFT	639
	total weight, LBS	2584
	total load, PSF	3.8
	total mech attach	1

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

##### 11.4 Seismic Ground Motion Values

Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1550 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters		Ss 1.516 S1 0.555	Figures 22-1 to 22-14
mapped MCE spectral response, short periods		Sms 1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second		S1 0.555	
11.4.2 Site Class	D		A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4, =Fa*Ss
mapped MCE spectral response at 1 second period	S1	0.833	Sec 11.4, Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDs	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*S1

##### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

##### General Design Requirements

Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13.2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements		N/A

13.2.3 Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4 Flexibility		Flexibility as well as strength must be considered
13.2.5 Testing Alternative		Components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by Table 13-2-1
13.2.7 Construction Documents		

### 13.3 Seismic Demands on Nonstructural Components

#### 13.3.1 Seismic Design Force

		$F_p = (0.4^*F_p^{*}SDS^{*}W_D)/(R_D^{*}I_D) * (1+2z/h)/1.4$	F <sub>p</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	[lbs]	$F_{ph}$ [1]	
		$F_{pmax}$ 6	
		$F_{pmin}$ 1	
spectral acceleration, short period [g]	SDS 1.0; 1		
component amplification factor (Table 13-6-1)	ap 1.00		
Component Importance Factor	Iq 1.00		
Operating Weight (total load of array) [lbs]	$W_p$ 4		
Response modification Factor (Table 13-5-1 or 13-6-1)	$R_p$ 2.50	1	Only ratio z/h is used, which is 1.0
point of component attachment [ft]	z 25		Only ratio z/h is used, which is 1.0
average roof height [ft]	h 25		
concurrent vertical load [lb]	$F_V = (2^*SDS^{*}W_D)/14$		
	1		F <sub>V</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
vertical resisting load	$9^*DL$	2	
	3		

#### 13.3.2 Seismic Relative Displacements

		Components shall be bolted, welded or otherwise positively fastened without consideration for frictional and 13.3.2
13.4 Nonstructural Component Anchorage		
13.4.1 Design Forces		
	roof attach lateral strength	623 [lbs]
	roof attach vertical strength	803 [lbs]
	Seismic Lateral Design Force, $F_p$	1 [lbs]
	Seismic Vertical Design Force, $F_V$	1 [lbs]
	total roof attachments req for lateral	1
	total roof attachments req for vertical	‡ 60% of the vertical resisting load ( $0.6^*W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof

Array Informations			
city	item	weight	total
14 Modules + Deflectors		54.22	759
30 Ballast CMU Block		13.4	402.0
18 North Support		19.44	349.9
5 South Support		12.75	63.8
0 Middle Support		0.0	0.0
% of Mechanical Attachments to Supports Ratio		4%	
area, SQFT		397	
total weight, LBS		1575	
total load, PSF		4.0	
total mech attach		1	

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

Description	Symbol	Input Values	Sections/Figures / Comments
Zip Code	93405	1550 MADONINA RD, SAN LUIS OBISPO, CA,	If S1 is less than or equal to .04 and Ss less than or equal to 0.15 Then Seismic Design category A only applies

11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	
mapped MCE spectral response, 1 second	S1	0.555	

11.4.2 Site Class	D		A, B, C D, E or F, D is default if site soil properties unknown - See table table 20-3.1
Site coefficient, short period	Fa	1.000	table 11-4-1
Site coefficient, 1 second	Fv	1.500	table 11-4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4. =Fa*Ss

11.4.4 Design Spectral Acceleration Parameters			Sec 11.4. Fv*S1
Short Periods	Sm1	0.833	
1 second period	SD1	0.555	

Description	Symbol	Value/Comment
Same as parent structure is site soil conditions	D	Same as parent structure is site soil conditions

13.1.2 Seismic Design Category	D	Unknown
13.1.3 Component Importance Factor	Ip	1.00
13.1.4 Exemptions		do not meet any exemptions

13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		
13.1.7 Reference Documents using allowable Stress Design		

Description	Symbol	Value/Comment
Table 13-2-1 states that mechanical and electrical supports must meet sections : 13-2, 13-3, 13-4, 13-6		
N/A		

13.2.3 Consequential Damage		cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4 Flexibility		Flexibility as well as strength must be considered
13.2.5 Testing Alternative		Components tested to ICC-ES AC 156 are acceptable
13.2.6 Use of Experience Data		An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by table 13.2-1
13.2.7 Construction Documents		

<b>13.3 Seismic Demands on Nonstructural Components</b>		
<b>13.3.1 Seismic Design Force</b>		
	$F_p = [(0.4 * \beta_p * SDS^{**}W_p) / (R_p / h)] * [1 + 2z/h] / 1.4$	$F_p$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
[lbs]	$F_{ph}$	
	$F_{pmax}$	
	$F_{pmin}$	
spectral acceleration, short period [g]	SDS 1.011	
component amplification factor (table 13.6-1)	ap 1.00	
Component Importance Factor	Ip 1.00	
Operating Weight (total load of array) [lbs]	Wp 4	
Response modification Factor (table 13.5-1 or 13.6-1) point of component attachment [ft]	Rp 2.50	Only ratio z/h is used, which is 1.0
average roof height [ft]	z 25	Only ratio z/h is used, which is 1.0
concurrent vertical load [lb]	h 25	
vertical resisting load	$f_v = (2 * SDS^{**}W_p) / 1.4$	$f_v$ values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	2*DL	
	0.9*Wp	
13.3.2 Seismic Relative Displacements		

<b>13.4 Nonstructural Component Anchorage</b>		
<b>Components shall be bolted, welded or otherwise positively fastened without consideration for frictional forces.</b>		
<b>and 13.3.2</b>		
13.4.1 Design Forces		
roof attach lateral strength	628 [lbs]	
roof attach vertical strength	808 [lbs]	
Seismic Lateral Design Force, $F_p$	1 [lbs]	
Seismic Vertical Design Force, $F_v$	1 [lbs]	
total roof attachments req for lateral	1	
total roof attachments req for vertical	1	60% of the vertical resisting load ( $0.6 * W_p$ ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof

Array Informations			
qty	item	weight	total
72	Modules + Deflectors	54.22	3904
62	Ballast CMU Block	13.4	830.8
80	North Support	19.44	1555.2
10	South Support	12.75	127.5
0	Middle Support	0.0	0.0
	% of Mechanical Attachments to Supports Ratio	15%	
	area, SQFT	1917	
	total weight, LBS	6417	
	total load, PSF	3.3	
	total mech attach	1	

#### ASCE 7-05 Seismic Worksheet for Non-Structural Members

11.4 Seismic Ground Motion Values			
Description	Symbol	Input Values	Sections/Figures / Comments
	Zip Code	93405 1250 MADONNA RD, SAN LUIS OBISPO, CA	If S1 is less than or equal to .04 and S5 less than or equal to 0.15 Then Seismic Design category A only applies
11.4.1 Mapped acceleration parameters			Figures 22-1 to 22-14
mapped MCE spectral response, short periods	Ss	1.516	Figures 22-1 to 22-14
mapped MCE spectral response, 1 second	S1	0.555	
11.4.2 Site Class	D		A, B, C, D, E or F, D is default if site soil properties unknown - See table table 20.3.1
11.4.3 Site Coefficients and Adjusted "Maximum Considered Earthquake" MCE Spectral Response Acceleration Parameters			
Site coefficient, short period	Fa	1.000	table 11.4-1
Site coefficient, 1 second	Fv	1.500	table 11.4-2
mapped MCE spectral response at short period	Sms	1.516	Sec 11.4 , =Fa*Ss
mapped MCE spectral response at 1 second period	Sm1	0.833	Sec 11.4 , Fv*S1
11.4.4 Design Spectral Acceleration Parameters			
Short Periods	SDS	1.011	11.4.3, 2/3*Sms
1 second period	SD1	0.555	11.4.4, 2/3*Sml1

#### 13.1 Seismic Design Requirements for Nonstructural components

Description	Symbol	Value/Comment
13.1.2 Seismic Design Category		Same as parent structure is site soil conditions
13.1.3 Component Importance Factor	D	Unknown
13.1.4 Exemptions	Ip	1.00 do not meet any exemptions
13.1.5 Applicability of Nonstructural Component Requirements		the array is not considered a nonbuilding structure as it is not 25% of the building seismic weight
13.1.6 Reference Documents		12.7.2 Definition of effective seismic weight W
13.1.7 Reference Documents using allowable Stress Design		

General Design Requirements		
Description	Symbol	Value/Comment
13.2.1 Applicable Requirements for architectural, Mechanical and Electrical Components and Supports		Table 13-2-1 states that mechanical and electrical supports must meet sections: 13.2, 13.3, 13.4, 13.6
13.2.2 Special Certification Requirements	N/A	

13.2.3	Consequential Damage	cannot cause failure of other essential architectural, electrical or mechanical components
13.2.4	Flexibility	Flexibility as well as strength must be considered
13.2.5	Testing Alternative	Components tested to ICC-ES AC 156 are acceptable
13.2.6	Use of Experience Data	An alternative to analytical seismic capacity is data construction documents are to be prepared by a registered design professional where required by table 13.2-1
13.2.7	Construction Documents	

13.3 Seismic Demands on Nonstructural Components		
13.3.1 Seismic Design Force	F <sub>p</sub> [F <sub>p</sub> =(0.4*ap*SDS*W <sub>b</sub> )/(R <sub>f</sub> (l <sub>e</sub> ))^(1+2z/h))/1.4 [lbs]	F <sub>p</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
	F <sub>ph</sub> 5	
	F <sub>pmax</sub> 5	
	F <sub>pmin</sub> 1	
spectral acceleration short period [g]	SDS 1.011	
component amplification factor (table 13.6-1)	ap 1.00	
Component Importance Factor	Ip 1.00	
Operating Weight (total load of array) [lbs]	W <sub>p</sub> 3	
Response modification Factor (table 13.5-1 or 13.6-1)	R <sub>p</sub> 2.50	
point of component attachment [ft]	z 25	Only ratio z/h is used, which is 1.0
average roof height [ft]	h 25	Only ratio z/h is used, which is 1.0
concurrent vertical load [lb]	f <sub>v</sub> f <sub>v</sub> =(2*SDS*W <sub>b</sub> )/1.4 0	f <sub>v</sub> values shall be divided by a factor of 1.4 per Equation 16A-21 of 2007 CBC
vertical resisting load	3*D <sub>L</sub> 3	0.9*W <sub>p</sub>
13.3.2 Seismic Relative Displacements		

13.4 Nonstructural Component Anchorage		
Components shall be bolted, welded or otherwise positively fastened without consideration for of frictional and 13.3.2		
13.4.1 Design Forces	roof attach lateral strength 808 [lbs]	
	roof attach vertical strength 1 [lbs]	
Seismic Lateral Design Force, F <sub>p</sub>	0 [lbs]	
Seismic Vertical Design Force, F <sub>v</sub>	1 [lbs]	
total roof attachments req for lateral	1	
total roof attachments req for vertical	1	‡ 60% of the vertical resisting load (0.6*W <sub>p</sub> ) is greater than the concurrent vertical load from the seismic forces. Therefore, no roof



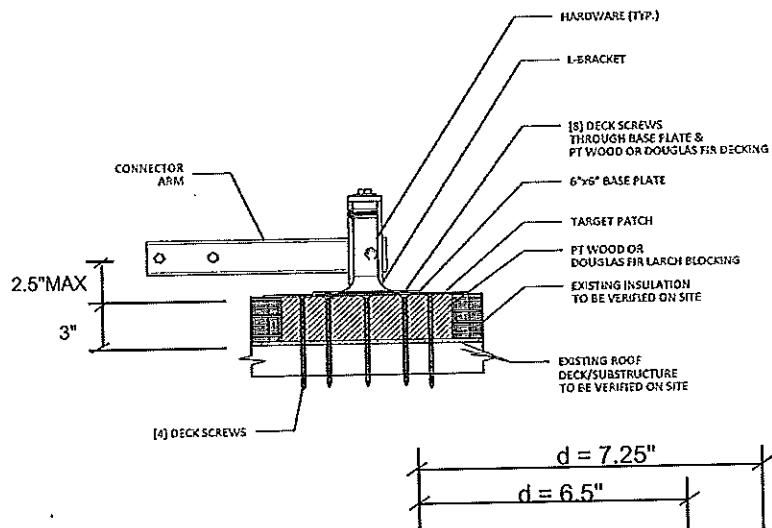
**CARUSO TURLEY SCOTT INC**

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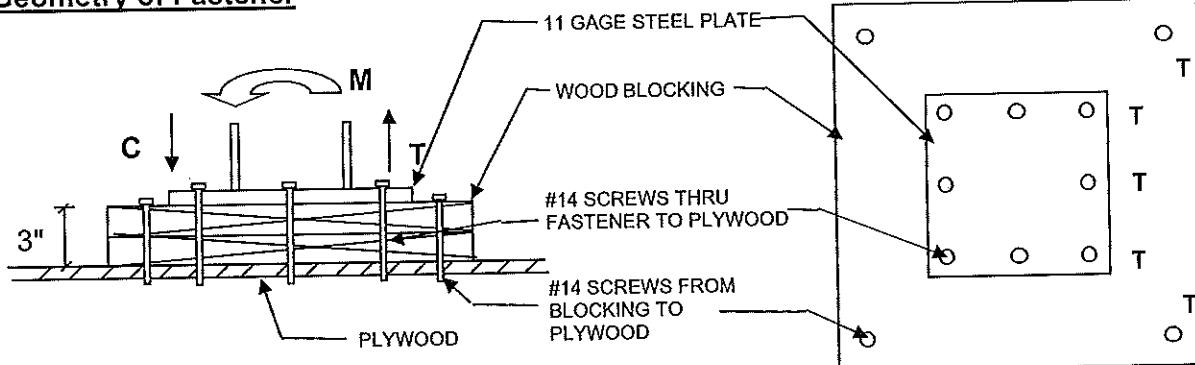
## Capacity of Eco Fasten Attachment To Wood

### Maximum of 3" Insulation with a Max 2.5" Connection

The Ecofasten Fastener plate is attached to plywood/OSB with 8#14 screws. The wood blocking is attached to the plywood/OSB with 4#14 screws. Therefore there is a total of 12 #14 screws attaching the fastener to the roof deck.



### Geometry of Fastener



5 Screws in Tension  
7 Screws in Shear

### Allowable Screw Values

Allowable Screw Shear Values =

Ultimate Shear ( $C_D$ )(Factor for Group)  
5

{Reference APA Fastener Loads  
for Plywood-Screws}

Allowable Screw Tension Values = Screw Capacity( $C_D$ )

{Reference APA Screw in  
Withdrawl - APA TT-051}

Note: The screw tension capacity is dependant on the specific gravity. Therefore, a SG=0.43 was assumed to obtain values from NDS Table 11.2B. The screw capacity is also dependant on the penetration of the screw.


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**Check Lateral Strength**
**Check Shear Loads:**

$$V_{\text{allowable}} = (7 \text{ Screws})(\text{Allowable Screw Shear Value})$$

**Check Pryout Loads:**

$$T_{\text{allowable (fastener)}} = (3 \text{ screws})(\text{Allowable Screw Tension Value})$$

$$T_{\text{allowable (wood)}} = (2 \text{ screws})(\text{Allowable Screw Tension Value})$$

$$\text{Allowable Moment} = T_{\text{allowable (fastener)}} \times 6.5" + T_{\text{allowable (wood)}} \times 7.25"$$

$$\text{Allowable Lateral Load for Pryout} = \frac{\text{Allowable Moment}}{5.5"}$$

**Table 1: Allowable Lateral Strength**

Roof Material	Shear (lbs)	*Pryout (lbs)
1/2" Plywood/OSB	1169	628
5/8" Plywood/OSB	1232	785
3/4" Plywood/OSB	1246	942

Note: Pryout values will govern for lateral strength values. Therefore, lateral strength of the attachment is limited to the pryout values for each sheathing type.

**Check Vertical Strength**

$$T_{\text{allowable}} = (8 \text{ screws})(\text{Allowable Screw Tension Value})$$

**Table 2: Allowable Vertical Strength**

Roof Material	Uplift (lbs)
1/2" Plywood/OSB	813
5/8" Plywood/OSB	1016
3/4" Plywood/OSB	1219

# FASTENER LOADS FOR PLYWOOD - SCREWS

Number E830C  
December 1995

## Introduction

The integrity of a structure is frequently dependent upon the connections between its component elements. For maximum strength and stability, each joint requires design which is adapted to the fastener type and to the strength properties of the individual structural members. Included in the following tables are ultimate withdrawal and lateral loads for plywood joints fastened with wood and sheet metal screws. These load values are based upon tests conducted by APA - The Engineered Wood Association.

## Test Results

**Plywood-and-Metal Connections**  
Self-drilling, self-tapping screws are commonly used to attach plywood up to 1-1/8 in. thick to steel flanges up to 3/16 in. thick. However, since threads are usually provided on only a portion of the fastener shank, it is important to specify the appropriate fastener length for a given plywood thickness. This precaution ensures that the threaded

portion of the shank will engage in the steel framing. Several lengths and styles are available. Additional details for these types of screws may be obtained from specific fastener manufacturers. The following data apply to wood screws and sheet metal screws.

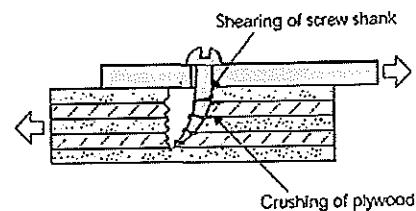
### Lateral Resistance:

Performance of plywood-and-metal connections is dependent upon the strength properties of all three elements.

a) Plywood-critical joints are characterized by a shearing of the plywood veneers oriented parallel to the direction of the applied force. Veneer plugs, whose width equals the diameter of the screw shank, may shear loose and protrude at the loaded end.

b) Fastener-critical joints are characterized by a shear failure of the screw shank. As shown in Figure 1, once localized crushing of the wood has occurred, resistance to fastener-head embedment into the metal causes the screw to become a shear specimen and joint behavior is dependent upon the shear strength of the fastener. Shear failure of the screw shank occurs at the wood-metal interface.

**FIGURE 1.**  
*Failure of Laterally  
Loaded, Single-Shear  
Metal-to-Plywood Connection*



c) The metal-critical joint may fail in one of two ways. Failure occurs when the resistance of the screw head to embedment is greater than the resistance of the metal to lateral and/or withdrawal load, and the screw tears away from the metal framing. Failure also occurs when thin metal in a metal-to-plywood joint crushes or tears away from the screw.

Tables 1 and 2 present ultimate lateral loads for wood- and sheet-metal-screw connections in plywood-and-metal joints. Loaded end distance in these tests was one inch. Plywood face grain was parallel to the load since this direction yields the lowest lateral loads when the joint is plywood-critical. All wood-screw specimens were tested with a 3/16-in.-thick steel side plate, and values should be modified if thinner steel is used.

**A P A**

*The Engineered Wood Association*

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TABLE 1.  
Screws: Metal-to-Plywood Connections<sup>(a)</sup>

Depth of Threaded Penetration (in.)	Ultimate Lateral Load (lb) <sup>(b)</sup>					
	Wood Screws			Sheet Metal Screws		
	#8	#10	#12	#8	#10	#12
1/2	415	(500)	590	465	(565)	670
5/8	-	-	-	500	(600)	705
3/4	-	-	-	590	(655)	715

(a) Plywood was C-D grade with exterior glue (all plies Group 1), face grain parallel to load. Side plate was 3/16"-thick steel.

(b) Values in parentheses are estimates based on other tests.

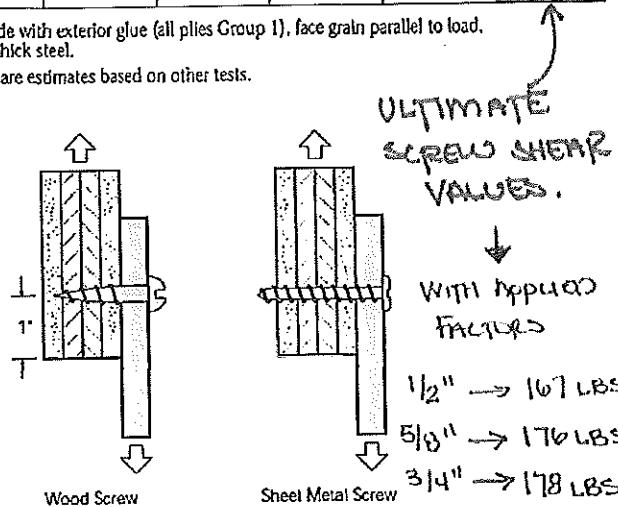
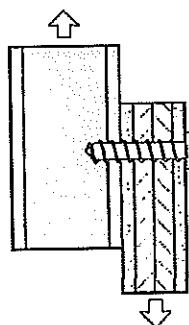


TABLE 2.  
Sheet Metal Screws: Plywood-to-Metal Connections<sup>(a)</sup>

Framing	Plywood Thickness (in.)	Ultimate Lateral Load (lb) <sup>(b)</sup>					
		Screw Size				1/4"-20 Self Tapping Screw	
		#8	#10	#12	#14		
0.080" Aluminum	1/4	330	360	390	410	590	
	1/2	630	850*	860	920	970	
	3/4	910*	930*	1260	1330	1440	
0.078" Galvanized Steel (14 gage)	1/4	360	380	400	410	650	
	1/2	700*	890*	900	920	970	
	3/4	700*	950*	1300*	1390*	1500	

(a) Plywood was A-C EXT (all plies Group 1), face grain parallel to load.

(b) Loads denoted by an asterisk(\*) were limited by screw-to-framing strength; others were limited by plywood strength.



#### Withdrawal:

Tables 3 and 4 present average ultimate withdrawal loads for wood and sheet metal screws in plywood-and-metal joints, based on analysis of test results. Wood screws have a tapered shank and are threaded for only 2/3 of their length. Sheet metal screws typically have higher ultimate load than wood screws in the smaller gages, because of their uniform shank diameter and full-length thread. The difference is not as apparent in the larger gages and lengths because the taper is not as significant.

Values shown in Table 3 for wood screws are based on 1/4-in. protrusion of the wood screw from the back of the panel. This was to assure measurable length of thread embedment in the wood, since the tip of the tapered wood screw may be smaller than the pilot hole. This was not a factor for sheet metal screws due to their uniform shanks.

#### Adjustment for Species Other Than Group 1:

All the ultimate loads presented in Tables 1 through 4 are based on plywood panels of all-Group 1 construction. For plywood panels of other species groups, the ultimate loads in these tables must be adjusted by

correction factors presented in Table 5. Correction factors apply for both lateral and withdrawal loading. The adjustment factor for the highest numbered species group present in any veneer should be used.

**Fastening Into Plywood Panel Edges**  
Fastening into plywood panel edges is not normally recommended. For some purposes, however, edge fastening may be necessary. Table 6 presents ultimate lateral and withdrawal loads for various sizes of wood screws in this application.

### Estimating Allowable Design Loads

It is the responsibility of the designer to select a working load suitable for the particular application. A high degree of variability is inherent in individual fastener test results.

Therefore, for screws in withdrawal, a working load of about one-sixth of the ultimate load has traditionally been used for long-duration loads. For normal load duration, the long-term working load may be increased by 10 percent. Normal load duration contemplates fully stressing the connection for approximately ten years, either continuously or cumulatively.

TABLE 3.  
Wood and Sheet Metal Screws: Metal-to-Plywood Connections(a)

Depth of Threaded Penetration (in.)	Average Ultimate Withdrawal Load (lb)					
	Screw Size					
	#6	#8	#10	#12	#14	#16
3/8	150	180	205	-	-	-
1/2	200	240	275	315	350	-
5/8	250	295	345	390	440	-
3/4	300	355	415	470	525	-
1	-	-	-	625	700	775
1-1/8	-	-	-	705	790	875
2-1/4	-	-	-	-	1580	-

(a) Plywood was C-D grade with exterior glue (all plies Group 1).

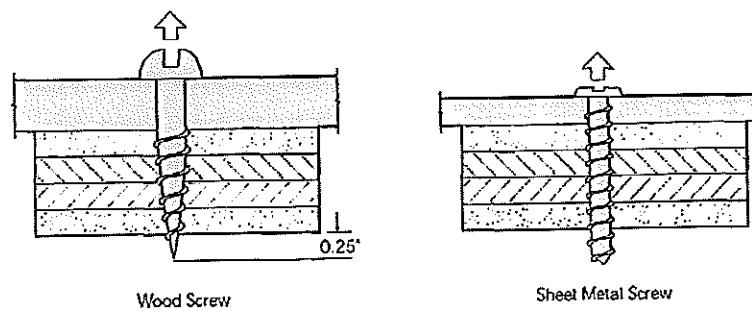
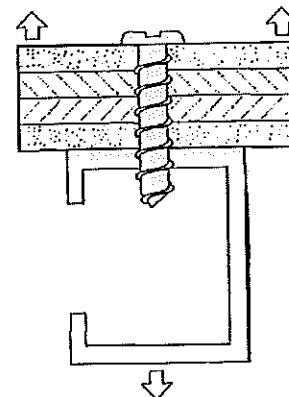


TABLE 4.  
Sheet Metal Screws: Plywood-to-Metal Connections(a)

Framing	Plywood Thickness (in.)	Ultimate Lateral Load (lb)(b)				
		Screw Size				1/4"-20 Self Tapping Screw
		#8	#10	#12	#14	
0.080"	1/4	130	150	170	180	220
	1/2	350	470	500	520	500
	3/4	660	680	790	850*	790*
0.078"	1/4	130	150	170	180	220
	1/2	350	470	500	520	500
	3/4	660	680	800	900	850

(a) Plywood was A-C EXT (all plies Group 1).

(b) Loads denoted by an asterisk(\*) were limited by screw-to-framing strength; others were limited by plywood strength.



For laterally loaded screws, a working load of normal duration may be approximated by dividing the tabulated ultimate load by 5 or 6. For practically all laterally loaded screw connections shown, the normal-duration working load will correspond to a joint slip of less than 0.01 inch.

Adjustments for shorter or longer duration of load apply to design values for mechanical fasteners where the strength of the wood (i.e., not the strength of the metal fastener) determines the load capacity. Adjustments of design values for varying durations of load and combinations of load should be in accordance with the current AF&PA National Design Specification for Wood Construction.

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TABLE 5.  
Load Adjustment for Screws into  
Plywood for Species Groups Noted<sup>(a)</sup>(b)

Types of Loading	All-Group 1	All-Group 2	All-Group 3, 4, 5
Lateral	100%	78%	78%
Withdrawal	100%	60%	47%

(a) Adjustments based on the species groups for plywood shown in Voluntary Product Standard PS 1 and the equations in U.S. Agricultural Handbook No. 72.

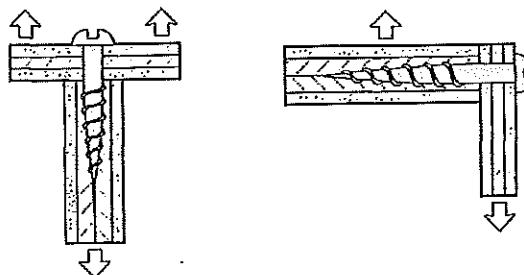
(b) Face, back, and core veneer must be of the same species group. When species group is unknown, assume all-Group 4.

TABLE 6.  
Wood Screws: Plywood-to-Plywood Edge Connections<sup>(a)</sup>

Depth of Threaded Penetration (in.)	Ultimate Lateral Load (lb) <sup>(b)</sup>			Ultimate Withdrawal Load (lb) <sup>(b)</sup>		
	#8	#10	#12	#8	#10	#12
1	180	(185)	195	360	(405)	450
1-1/2	180	(185)	195	410	(455)	500

(a) Plywood receiving screw thread was 3/4"-thick C-D grade with exterior glue (Group 2 inner plies).

(b) Values in parentheses are estimates based on other tests.



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Form No. E830C  
Revised December 1995/0100





# Technical Topics

TT-051C

JUNE 2011

## Screw Withdrawal from the Face of APA-Trademarked Structural Panels

### **BACKGROUND**

Withdrawal capacities of screws from wood products are dependent upon a number of variables including the type and diameter of the screw, the specific gravity of the wood component, the effective penetration of the *threaded portion* (approximately 2/3 of total screw length) of the screw, and moisture conditions. These variables are briefly discussed below:

- Various screw types have different combinations of thread pitch and profile, diameter, and material type. The capacity of the fastener is dependent on the combination of each of these factors. Of the various types available, recommendations in this Technical Topic are based on the result of testing No. 10, Type A sheet metal screws. The results given in the following table are applicable to only this type of screw.
- The capacity of a screw in solid lumber depends on the specific gravity<sup>a)</sup> of the wood component into which it is driven. The equivalent specific gravity of engineered wood products, like plywood and OSB, for use with screws is based on test results.
- Fastener withdrawal capacities for wood products are usually provided on a "per inch of penetration of the threaded portion" basis. Tabulated values that are provided on such a basis must therefore be adjusted to reflect the depth of penetration of the thread portion of the screw in the wood component anchoring the screw.
- The values tabulated in this publication are based on the use of screws driven into dry panels (moisture content < 16%) and used under circumstances where the connection will remain dry in service. For any wet-use conditions (moisture content ≥ 16%), before, during or after installation, the capacity of the fastener must be multiplied by a 0.7 factor<sup>b)</sup>.

Another important consideration is the relative ease in over-torquing or overdriving the screws when using power tools. If the screw continues to turn (spin) after the head has contacted the panel surface, the threads will essentially drill a hole in the panel which may reduce the withdrawal capacity of the fastener significantly.

This Technical Topic addresses screw withdrawal in two ways. It first looks at the results of withdrawal testing of No. 10, Type A sheet metal screws in various wood structural panels, as shown in Table 1. Note that the values given are ultimate values. Traditionally, single-fastener design values are determined by dividing the average ultimate values by a factor of 5.0. *APA Technical Note, Fastener Loads for Plywood – Screws*, Form E830, contains information for screw withdrawal and lateral load on plywood-to-metal connections ([www.apawood.org](http://www.apawood.org)).

a. 2005 National Design Specification (NDS) for Wood Construction, Table 11.3.2A.

b. 2005 National Design Specification (NDS) for Wood Construction, Table 10.3.3.

## TESTS RESULTS

A series of tests were conducted using 1-1/2-inch-long No. 10, Type A sheet metal screws (12 threads per inch, flat head, pointed tip, 0.190-inch nominal diameter) primarily on 23/32-inch-thick wood structural panels in compliance with ASTM D 1761. The withdrawal rate was 0.6 inch per minute. The tabulated average withdrawal values provide a basis for comparison among various panel types and wood species. Data shown in Table 1 cannot be generalized to determine the withdrawal capacity of screws from edges or their lateral load capacities.

TABLE 1. WITHDRAWAL VALUES OF NO. 10 TYPE A 1-1/2-INCH SHEET METAL SCREWS (12 THREADS PER INCH)  
FROM PANEL FACES NORMALIZED TO POUNDS PER INCH OF THREAD PENETRATION<sup>(a)</sup>

	Type of Panel			Wood Species in OSB	
	Wood Species in Plywood			Southern Pine	Southern Pine
	Southern Pine	Douglas-fir	Mixed Species	Aspen	Aspen
Number of Tests	529	145	119	146	131
Average Ultimate Load (lbf/in.)	835	730	641	550	648
Design Load (lbf/in.) <sup>(b)</sup>	167	146	128	110	130
Equivalent Specific Gravity, G for Withdrawal	0.55	0.52	0.49	0.45	0.49
Recommended Equivalent Specific Gravity, G, for Withdrawal				0.45	

a. Ultimate values listed are based primarily of tests of 23/32-inch-thick wood structural panels.

b. Design values are based on average ultimate load divided by 5.0.

## CALCULATED DESIGN CAPACITIES

The second method for determining design values is to use the mechanics-based method provided in the 2005 National Design Specification (NDS) for Wood Construction based on the equivalent specific gravity listed in Table 1. Adjustments for moisture content or duration of load shall be permitted to be applied as appropriate.

When calculating the design withdrawal capacity for screws, NDS Equation 11.2.2 was adapted to take into account penetration into the panel as follows:

$$W = 2,850 \times G^2 \times D \times L \rightarrow \text{TABLE 11.2B OF NDS.}$$

where:

W = reference withdrawal design value (lbf)

G = the equivalent specific gravity of the wood receiving member. (See Table 1)

D = nominal screw diameter (in.)

L = length of thread penetration into the panel (in.)

Common adjustment values for screw withdrawal are:

$C_D$ – Duration of load (NDS 10.3.2)		
Permanent duration		0.90
Normal duration		1.00
Two month duration		1.15
Seven days duration		1.25
Ten minutes duration		1.60 ← C <sub>D</sub>

$C_M$  – Wet Service Factor (NDS 10.3.3)

Wood Structural Panel moisture content before, during or after construction  $\geq 16\%$  (note<sup>(10)</sup>, page 1) 0.70

The following design example is for calculating the allowable withdrawal design value of screws from the face of OSB panels.

**Example:**

Calculate the withdrawal capacity of a 1-inch-long No. 12 wood screw (0.216 inch in diameter) through a 1/8-inch-thick steel bracket into 23/32-inch-thick OSB. The screws will be driven into dry panels and will be used in dry service conditions. The application is for normal duration of load.

The threaded portion of the screw is  $2/3 \times 1 = 0.67$  inch. The unthreaded portion is  $1 - 0.67 = 0.33$  inch. The length of unthreaded screw imbedded in the panel is  $0.33 - 0.125 = 0.205$  inch. The screw fully penetrates the 23/32-inch panel. The threaded portion in the panel is  $0.7188 - 0.205 = 0.51$  inch.  $G = 0.45$ . The design withdrawal capacity is:

$$W = 2,850 \times 0.45^2 \times 0.216 \times 0.51 = 64 \text{ pounds per screw}$$

Adjustment for duration of load and moisture conditions:

$$64 \times 1.00 \times 1.00 = 64 \text{ pounds per screw}$$

Designers are cautioned about over-torquing screws in wood products. Good construction practice should minimize the potential for over-torquing. Over-torquing will reduce screw withdrawal capacity, regardless of the construction materials involved.

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## 11.2.2 Wood Screws

11.2.2.1 The reference withdrawal design value, in lb/in. of penetration, for a single wood screw (cut thread or rolled thread) inserted in side grain, with the wood screw axis perpendicular to the wood fibers, shall be determined from Table 11.2B or Equation 11.2-2, within the range of specific gravities and screw diameters given in Table 11.2B. Reference withdrawal design values,  $W$ , shall be multiplied by all applicable adjustment factors (see Table 10.3.1) to obtain adjusted withdrawal design values,  $W'$ .

$$W = 2850 G^2 D \quad (11.2-2)$$

11.2.2.2 Wood screws shall not be loaded in withdrawal from end grain of wood.

11.2.2.3 When wood screws are loaded in withdrawal, the adjusted tensile strength of the wood screw at net (root) section shall not be exceeded (see 10.2.3).

## 11.2.3 Nails and Spikes

11.2.3.1 The reference withdrawal design value, in lb/in. of penetration, for a single nail or spike driven in the side grain of the main member, with the nail or spike axis perpendicular to the wood fibers, shall be determined from Table 11.2C or Equation 11.2-3, within the range of specific gravities and nail or spike diameters given in Table 11.2C. Reference withdrawal design values,  $W$ , shall be multiplied by all applicable adjustment factors (see Table 10.3.1) to obtain adjusted withdrawal design values,  $W'$ .

$$W = 1380 G^{5/2} D \quad (11.2-3)$$

11.2.3.2 Nails and spikes shall not be loaded in withdrawal from end grain of wood.

## 11.2.4 Drift Bolts and Drift Pins

Drift bolt and drift pin connections loaded in withdrawal shall be designed in accordance with principles of engineering mechanics.

**Table 11.2B Cut Thread or Rolled Thread Wood Screw Reference Withdrawal Design Values ( $W$ )<sup>1</sup>**

Tabulated withdrawal design values ( $W$ ) are in pounds per inch of thread penetration into side grain of main member. Thread length is approximately 2/3 the total wood screw length (see Appendix L).

Specific Gravity, $G$	Wood Screw Number										
	6	7	8	9	10	12	14	16	18	20	24
0.73	209	229	249	268	288	327	367	406	446	485	564
0.71	198	216	235	254	272	310	347	384	421	459	533
0.68	181	199	216	233	250	284	318	352	387	421	489
0.67	176	193	209	226	243	276	309	342	375	409	475
0.58	132	144	157	169	182	207	232	256	281	306	356
0.55	119	130	141	152	163	186	208	231	253	275	320
0.51	102	112	121	131	141	160	179	198	217	237	275
0.50	98	107	117	126	135	154	172	191	209	228	264
0.49	94	103	112	121	130	147	165	183	201	219	254
0.47	87	95	103	111	119	136	152	168	185	201	234
0.46	83	91	99	107	114	130	146	161	177	193	224
0.44	76	83	90	97	105	119	133	148	162	176	205
0.43	73	79	86	93	100	114	127	141	155	168	196
0.42	69	76	82	89	95	108	121	134	147	161	187
0.41	66	72	78	85	91	103	116	128	141	153	178
0.40	63	69	75	81	86	98	110	122	134	146	169
0.39	60	65	71	77	82	93	105	116	127	138	161
0.38	57	62	67	73	78	89	99	110	121	131	153
0.37	54	59	64	69	74	84	94	104	114	125	145
0.36	51	56	60	65	70	80	89	99	108	118	137
0.35	48	53	57	62	66	75	84	93	102	111	130
0.31	38	41	45	48	52	59	66	73	80	87	102

<sup>1</sup> Tabulated withdrawal design values ( $W$ ) for wood screw connections shall be multiplied by all applicable adjustment factors (see Table 10.3.1).